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**Plastics piping systems for the supply  
of gaseous fuels for maximum  
operating pressures up to and including  
2 MPa (20 bar) — Polyamide (PA) —**

**Part 5:  
Fitness for purpose of the system**

*Systèmes de canalisations en matières plastiques pour la distribution  
de combustibles gazeux pour des pressions maximales de service  
inférieures ou égales à 2 MPa (20 bar) — Polyamide (PA) —*

*Partie 5: Aptitude à l'emploi du système*



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# Contents

Page

<b>Foreword</b> .....	<b>iv</b>
<b>Introduction</b> .....	<b>v</b>
<b>1 Scope</b> .....	<b>1</b>
<b>2 Normative references</b> .....	<b>1</b>
<b>3 Terms, definitions, symbols and abbreviated terms</b> .....	<b>2</b>
<b>3.1 Terms and definitions — General</b> .....	<b>2</b>
<b>3.2 Terms and definitions for preparation of test assemblies by electrofusion</b> .....	<b>3</b>
<b>3.3 Symbols</b> .....	<b>3</b>
<b>4 Fitness for purpose</b> .....	<b>5</b>
<b>4.1 Method of preparation of assemblies for testing</b> .....	<b>5</b>
<b>4.2 Requirements for fitness for purpose</b> .....	<b>6</b>
<b>5 Overall service (design) coefficient</b> .....	<b>9</b>
<b>Annex A (normative) Preparation of test assemblies by butt fusion</b> .....	<b>10</b>
<b>Annex B (normative) Preparation of test assemblies by electrofusion</b> .....	<b>13</b>
<b>Annex C (normative) Test methods for the assessment of fitness for purpose of transition fittings</b> .....	<b>19</b>
<b>Annex D (normative) Derating coefficients for operating temperatures</b> .....	<b>21</b>

## Foreword

ISO (the International Organization for Standardization) is a worldwide federation of national standards bodies (ISO member bodies). The work of preparing International Standards is normally carried out through ISO technical committees. Each member body interested in a subject for which a technical committee has been established has the right to be represented on that committee. International organizations, governmental and non-governmental, in liaison with ISO, also take part in the work. ISO collaborates closely with the International Electrotechnical Commission (IEC) on all matters of electrotechnical standardization.

International Standards are drafted in accordance with the rules given in the ISO/IEC Directives, Part 2.

The main task of technical committees is to prepare International Standards. Draft International Standards adopted by the technical committees are circulated to the member bodies for voting. Publication as an International Standard requires approval by at least 75 % of the member bodies casting a vote.

Attention is drawn to the possibility that some of the elements of this document may be the subject of patent rights. ISO shall not be held responsible for identifying any or all such patent rights.

ISO 22621-5 was prepared by Technical Committee ISO/TC 138, *Plastics pipes, fittings and valves for the transport of fluids*, Subcommittee SC 4, *Plastics pipes and fittings for the supply of gaseous fuels*.

ISO 22621 consists of the following parts, under the general title *Plastics piping systems for the supply of gaseous fuels for maximum operating pressures up to and including 2 MPa (20 bar) — Polyamide (PA)*:

- *Part 1: General*
- *Part 2: Pipes*
- *Part 3: Fittings*
- *Part 5: Fitness for purpose of the system*
- *Part 6: Code of practice for design, handling and installation*

## Introduction

As polyamide material is used for piping systems for the supply of gaseous fuels both at low and high pressure, ISO/TC 138/SC 4 experts decided to split the standardization programme into two series of International Standards, with one series [ISO 15439 (all parts)] covering low pressures up to 0,4 MPa (4 bar), and the other (ISO 22621) high pressures up to 2 MPa (20 bar).

Thin wall thickness pipes and solvent cement joints are used typically for pressures up to 0,4 MPa (4 bar), while thicker wall thickness pipes and butt fusion, electrofusion and mechanical joints are typically used for pressures up to 2 MPa (20 bar). For technical and safety reasons, it is not possible to mix the components of the two types of piping system (thin wall thickness pipes cannot be jointed by butt fusion or mechanical joints and vice versa). In particular, solvent cement joints must not be used for jointing for high-pressure piping systems.

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# Plastics piping systems for the supply of gaseous fuels for maximum operating pressures up to and including 2 MPa (20 bar) — Polyamide (PA) —

## Part 5: Fitness for purpose of the system

### 1 Scope

This part of ISO 22621 specifies the requirements of fitness for purpose of the polyamide (PA) piping system, intended to be buried and used for the supply of gaseous fuels at maximum operating pressures (MOP) up to and including 2 MPa (20 bar<sup>1</sup>).

It specifies the definitions of electrofusion and butt fusion joints.

It also specifies the method of preparation of test piece joints and the tests to be carried out on these joints for assessing the fitness for purpose of the system under normal and extreme conditions.

In addition, it specifies the test parameters for the test methods to which it refers.

In conjunction with the other parts of ISO 22621, it is applicable to PA fittings, their joints and joints with components of PA.

### 2 Normative references

The following referenced documents are indispensable for the application of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

ISO 291, *Plastics — Standard atmospheres for conditioning and testing*

ISO 1167-1, *Thermoplastics pipes, fittings and assemblies for the conveyance of fluids — Determination of the resistance to internal pressure — Part 1: General method*

ISO 1167-4, *Thermoplastics pipes, fittings and assemblies for the conveyance of fluids — Determination of the resistance to internal pressure — Part 4: Preparation of assemblies*

ISO 6259-1, *Thermoplastics pipes — Determination of tensile properties — Part 1: General test method*

ISO 13953, *Polyethylene (PE) pipes and fittings — Determination of the tensile strength and failure mode of test pieces from a butt-fused joint*

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1) 1 bar = 0,1 MPa = 10<sup>5</sup> Pa; 1 MPa = 1 N/mm<sup>2</sup>.

## ISO 22621-5:2010(E)

ISO 13954, *Plastics pipes and fittings — Peel decohesion test for polyethylene (PE) electrofusion assemblies of nominal outside diameter greater than or equal to 90 mm*

ISO 13955, *Plastics pipes and fittings — Crushing decohesion test for polyethylene (PE) electrofusion assemblies*

ISO 22621-1, *Plastics piping systems for the supply of gaseous fuels for maximum operating pressures up to and including 2 MPa (20 bar) — Polyamide (PA) — Part 1: General*

ISO 22621-2, *Plastics piping systems for the supply of gaseous fuels for maximum operating pressures up to and including 2 MPa (20 bar) — Polyamide (PA) — Part 2: Pipes*

ISO 22621-3, *Plastics piping systems for the supply of gaseous fuels for maximum operating pressures up to and including 2 MPa (20 bar) — Polyamide (PA) — Part 3: Fittings*

### 3 Terms, definitions, symbols and abbreviated terms

For the purposes of this document, the terms, definitions, symbols and abbreviated terms given in ISO 22621-1 and the following apply.

#### 3.1 Terms and definitions — General

##### 3.1.1

##### **electrofusion joint**

joint between a PA electrofusion socket or saddle fitting and a pipe or a spigot end fitting

NOTE The electrofusion fittings are heated by the Joule effect of the heating element incorporated at their jointing surfaces, causing the material adjacent to them to melt and the pipe and fitting surfaces to fuse.

##### 3.1.2

##### **butt fusion joint (using heated tool)**

joint made by heating the planed ends the surfaces of which match by holding them against a flat heating plate until the PA material reaches fusion temperature, removing the heating plate quickly and pushing the two softened ends against one another

##### 3.1.3

##### **fusion compatibility**

ability of two similar or dissimilar polyamide materials to be fused together to form a joint which conforms to the performance requirements of this standard

##### 3.1.4

##### **transition fitting**

fitting that makes a transition joint between a polyamide (PA) piping and a metallic pipe

##### 3.1.5

##### **transition joint**

joint at which two different piping materials (the PA and metal piping) are connected

##### 3.1.6

##### **anodeless riser**

type of transition fitting which is designed to transport gas from an underground polyamide (PA) service line to above-ground steel piping

NOTE In an anodeless riser, the PA pipe is always the gas carrier, at least, in the below ground section.



## 3.2 Terms and definitions for preparation of test assemblies by electrofusion

### 3.2.1

#### reference time

 $t_R$ 

theoretical fusion time indicated by the fitting manufacturer for the reference ambient temperature

See Annex B.

### 3.2.2

#### fusion energy

electrical energy supplied during the fusion-jointing cycle as measured at the terminals of the fitting at a given ambient temperature,  $T_a$ , and for electrical parameters whose values lie within the tolerance ranges declared by the manufacturer

NOTE 1 The fitting manufacturer is generally required to state in the technical file any variations in fusion energy input required as a function of the ambient temperature in the range  $T_{min}$  to  $T_{max}$ .

NOTE 2 Where applicable, energy measurement should exclude the effect of terminal contact resistance.

### 3.2.3

#### reference energy

energy supplied to a fitting having a nominal electrical resistance and using the nominal fusion parameters defined by the manufacturer at the reference ambient temperature,  $T_R$

See Annex B.

### 3.2.4

#### maximum energy

maximum value of the fusion energy supplied for jointing at a given ambient temperature,  $T_a$

See Annex B.

### 3.2.5

#### minimum energy

minimum value of the fusion energy supplied for jointing at a given ambient temperature,  $T_a$

See Annex B.

### 3.2.6

#### nominal energy

nominal energy supplied for jointing at a given ambient temperature,  $T_a$

See Annex B.

## 3.3 Symbols

Application	Symbol	Description	Unit
Symbols used in more than one phase of the fusion-jointing cycle <sup>a</sup>	$e_n$	nominal pipe wall thickness	mm
	$d_n$	nominal external diameter of the pipe	
	$p$	pressure applied to the butt fusion joint interface	
	$t$	duration of each phase in the fusion cycle	
	$T_{nom}$	nominal temperature (23 ± 2) °C	°C
	$T_{max}$	maximum permissible ambient temperature	°C
	$T_{min}$	minimum permissible ambient temperature	°C

Application	Symbol	Description	Unit
<b>Symbols for joint geometry<sup>a</sup></b>	$\Delta a$	misalignment between the pipes or fittings to be butt-fused, expressed in terms of the difference between the external diameters	mm
	$\Delta w$	clearance between the fusion faces, expressed in terms of the gap between the prepared faces	mm
<b>Symbols for ambient temperature<sup>ab</sup></b>	$T_a$	ambient temperature at which the joint is made	°C
<b>Symbols for butt fusion cycle parameters<sup>a</sup>:</b>	$T$	heater-plate temperature, measured in the zone of the heater-plate surface in contact with the pipe or spigot ends to be butt-fused	°C
— <b>General</b>			
— <b>Phase 1: heating</b>	$p_1$	interface pressure during the heating phase, i.e. the pressure applied in the contact zone	MPa
	$B_1$	initial bead width taken as the bead width at the end of the heating phase	mm
	$t_1$	heating time, taken as the time necessary to obtain a bead of width $B_1$ in the joint region during the heating phase	s
— <b>Phase 2: heat soak</b>	$p_2$	pressure between the heater plate and the pipe or spigot ends during the heat soak phase	MPa
	$t_2$	duration of internal heating during the heat soak phase	s
— <b>Phase 3: withdrawal of heater plate</b>	$t_3$	time between the moment when the heater plate is removed from the pipe and/or spigot ends and the moment when the pipe and/or spigot ends are placed in contact with each other	s
— <b>Phase 4: pressure increase</b>	$t_4$	time required to establish the butt fusion pressure	s
— <b>Phase 5: butt fusion</b>	$p_5$	pressure applied to the contact zone during the butt fusion phase	MPa
	$t_5$	time during which the assembly remains under the butt fusion pressure in the machine	min
— <b>Phase 6: cooling</b>	$t_6$	cooling time during which the butt-fused assembly is not subjected to any rough handling; this cooling can take place outside the machine	min
	$B_2$	bead width obtained at the end of the cooling phase	mm
<b>Symbols for the preparation of test assemblies by electrofusion<sup>c</sup></b>	$D_{im}$	mean inside diameter of the fusion zone of a fitting in the radial plane located a distance $L_3 + 0,5L_2$ from the face of the fitting socket	
	$D_{im,max}$	maximum theoretical value of $D_{im}$ as declared by the fitting manufacturer	
	$D_{i,max}$	maximum inside diameter of the fusion zone of the fitting	
	$D_{i,min}$	minimum inside diameter of the fusion zone of the fitting	
	$d_e$	outside diameter of a pipe or fitting spigot	
	$d_{em}$	mean outside diameter of a pipe or fitting spigot in conformance with ISO 22621-2 and ISO 22621-3, as applicable, and calculated from the measured circumference	

Application	Symbol	Description	Unit
	$d_{emp}$	mean outside diameter of a pipe or fitting spigot after preparation for assembly with the outer layer, removed by scraping or peeling and calculated from the circumference measured in a radial plane coincident with the centre of the fusion zone at a distance $L_3 + 0,5L_2$ from the face of the fitting socket after assembly	
	$e_n$	nominal wall thickness of the pipe	mm
	$e_s$	depth of scraping or the thickness of material removed from the pipe surface by peeling	mm
	$L_2$	nominal length of the fusion zone as indicated by the fitting manufacturer	
	$L_3$	nominal distance from the face of the fitting socket to the leading edge of the fusion zone	
<p>a See Annex A.</p> <p>b The ambient temperature may vary from the minimum temperature, <math>T_{min}</math>, to the maximum temperature, <math>T_{max}</math>, defined by agreement between the manufacturer and purchaser.</p> <p>c See Figure B.1; see Annex B.</p>			

## 4 Fitness for purpose

### 4.1 Method of preparation of assemblies for testing

#### 4.1.1 General

The joints shall be made by using pipes conforming to ISO 22621-2 or fittings conforming to ISO 22621-3.

Test pieces for pressure test shall be closed with pressure-tight, end-load-bearing end caps, plugs or flanges, which shall be provided with connections for the entry of water and release of air.

#### 4.1.2 Butt fusion joints

PA pipes and spigot end fittings intended to be used for jointing by butt fusion shall be prepared and assembled in accordance with Annex A.

#### 4.1.3 Electrofusion jointing

PA pipes and fittings intended to be used for jointing by electrofusion shall be prepared and assembled in accordance with Annex B.

For joints with electrofusion socket fittings and joints with electrofusion saddle fittings, test joints shall be prepared to check the fitness for purpose of the fittings under extreme jointing conditions.

For joints with electrofusion saddle fittings, the electrofusion saddle fitting shall be fused to the pipe, while it is pneumatically pressurized to the allowable maximum operating pressure. The pipe shall be cut immediately after the manufacturer-prescribed cooling time has elapsed.

These joints with electrofusion saddle fitting should be prepared taking national safety regulations into consideration.

For straight equal electrofusion socket fittings (couplers), test joints on selected diameters out of the product range shall be prepared with a gap of  $0,05d_n$  between the pipe end and the maximum theoretical depth of

penetration of the fitting, where for diameters greater than 225 mm, the adjoining pipes shall be arranged to provide the maximum angular deflection possible for the fitting, limited to 1,5°.

## 4.2 Requirements for fitness for purpose

### 4.2.1 Fitness for purpose for butt fusion joints

#### 4.2.1.1 Under normal conditions — Ambient temperature 23 °C

For the assessment of fitness for purpose under normal conditions, butt fusion joints shall have the characteristic of tensile strength conforming to the requirement given in Table 5, using the parameters as specified in Annex A, Table A.2 and Table A.3, at an ambient temperature of  $(23 \pm 2)$  °C and the scheme listed in Table 1.

**Table 1 — Scheme for butt fusion joints**

Pipe/spigot end fitting	Pipe			
	PA 11 160	PA 11 180	PA 12 160	PA 12 180
PA 11 160	X	X <sup>a</sup>	Jointing not allowed	Jointing not allowed
PA 11 180	X <sup>a</sup>	X	Jointing not allowed	Jointing not allowed
PA 12 160	Jointing not allowed	Jointing not allowed	X	X <sup>a</sup>
PA 12 180	Jointing not allowed	Jointing not allowed	X <sup>a</sup>	X

This table should be interpreted as follows: as an example, for a pipe or a spigot end fitting made from a PA 11 160 compound, a joint should be tested with a pipe made from PA 11 160 compound. When requested by the purchaser or end user, for mixed compound joints, test pieces should be used incorporating PA 11 160 and PA 11 180 compounds.

<sup>a</sup> Only when requested by the purchaser or end user.

The pipe manufacturer shall declare, according to 4.2.1.1, which pipes from his own product range conforming to ISO 22621-2 are compatible with each other for butt fusion.

The fitting manufacturer shall declare, according to 4.2.1.1, the SDR range and MRS values of pipes conforming to ISO 22621-2, to which his fittings conforming to ISO 22621-3 can be fused by using the same procedures (e.g. times, temperatures, fusion pressures) to conform to this part of ISO 22621. If there is a need for deviation in fusion procedures, the fitting manufacturer shall state this clearly.

#### 4.2.1.2 Under extreme conditions

For butt fusion joints, the characteristics to be examined for fitness for purpose under extreme conditions shall conform to Table 2.

**Table 2 — Relationship between the joints and fitness for purpose characteristics**

Butt fusion joint	Associated characteristic
Both components of the joint: same MRS and same SDR Joint: minimum and maximum condition <sup>a</sup>	Hydrostatic strength (80 °C, 165 h)
Both components of the joint: same MRS and same SDR Joint: minimum and maximum condition	Tensile strength for butt fusion joint

<sup>a</sup> As specified in Annex A concerning misalignment [A.5 a)] and the limit values of fusion parameters (Table A.4).

When tested in accordance with the test methods as specified in Table 5 using the indicated parameters, the joints shall have characteristics conforming to the requirements given in Table 5.

The fitting manufacturer shall declare, according to Table 2, as applicable, the fitness for purpose under extreme conditions of his fittings.

The pipe manufacturer shall declare, according to Table 2, the fitness for purpose under extreme conditions of his pipes.

**4.2.2 Fitness for purpose for electrofusion joints**

**4.2.2.1 Under normal conditions — Ambient temperature 23 °C**

For the assessment of fitness for purpose under normal conditions, electrofusion joints shall have the characteristic of decohesive resistance or cohesive strength, as applicable, conforming to the requirement given in Table 5, using assembly condition 1 as specified in Annex B, Table B.3, at an ambient temperature of (23 ± 2) °C and the scheme listed in Table 3.

**Table 3 — Scheme for electrofusion joints**

Electrofusion fitting with electrofusion socket	Pipe			
	PA 11 160 SDR maximum	PA 11 180 SDR minimum	PA 12 160 SDR maximum	PA 12 180 SDR minimum
PA 11 160	X	X <sup>a</sup>	Jointing not allowed	Jointing not allowed
PA 11 180	X <sup>a</sup>	X	Jointing not allowed	Jointing not allowed
PA 12 160	Jointing not allowed	Jointing not allowed	X	X <sup>a</sup>
PA 12 180	Jointing not allowed	Jointing not allowed	X <sup>a</sup>	X

This table should be interpreted as follows: as an example, for an electrofusion fitting made from a PA 11 160 compound, a joint should be tested with a pipe made from PA 11 160 compound and an SDR maximum and another joint should be tested with a pipe made from PA 11 160 compound and an SDR minimum.

<sup>a</sup> Only when requested by the purchaser.

The fitting manufacturer shall declare, according to 4.2.2.1, the SDR range and MRS values of pipes conforming to ISO 22621-2, to which his fittings conforming to ISO 22621-3 can be fused by using the same procedures (e.g. times, temperatures, fusion pressures) to conform to this part of ISO 22621. If there is a need for deviation in fusion procedures, the fitting or valve manufacturer shall state this clearly.

**4.2.2.2 Under extreme conditions**

For electrofusion joints, the characteristics to be examined for fitness for purpose under extreme conditions shall conform to Table 4.

When tested in accordance with the test methods as specified in Table 5 using the indicated parameters, the joints shall have characteristics conforming to the requirements given in Table 5.

**Table 4 — Relationship between the joints and fitness for purpose characteristics**

Electrofusion joint, including socket fitting <sup>a</sup>	Electrofusion joint, including saddle fitting <sup>a</sup>	Associated characteristic
Pipe: MRS maximum <sup>b</sup> SDR minimum <sup>b</sup> Joint: conditions 2.2 and 3.2 of Table B.3 <sup>c</sup>		Decohesive resistance
	Pipe: MRS maximum <sup>b</sup> SDR minimum <sup>b</sup> Joint: conditions 2.2 and 3.2 of Table B.3 <sup>c</sup>	Cohesive strength

<sup>a</sup> If accepted by the purchaser, the minimum and maximum energy conditions 2.2 and 3.2 may be replaced by a nominal energy at a given ambient temperature,  $T_a$ , defined by the fitting manufacturer (see 3.2.6).

<sup>b</sup> As declared by the fitting manufacturer according to 4.2.2.1.

<sup>c</sup> As specified in Table B.3 with  $T_{min}$  and  $T_{max}$  as stated in the fitting manufacturer's technical specification.

The fitting manufacturer shall declare according to Table 4, as applicable, the fitness for purpose under extreme conditions of his fittings.

**Table 5 — Characteristics for fitness for purpose of the system**

Characteristic	Requirement	Test parameters		Test method
		Parameter	Value	
Hydrostatic strength (80 °C, 165 h)	No failure during the test period of any test piece	End caps	Type A	ISO 1167-1
		Orientation	Free	ISO 1167-4
		Conditioning time	6 h	
		Type of test	Water-in-water	
		Circumferential (hoop) stress		
		PA 11 160 and PA 12 160	10,0 MPa	
		PA 11 180 and PA 12 180	11,5 MPa	
		Test period	165 h	
		Test temperature	80 °C	
Cohesive resistance for electrofusion socket fittings	Length of initiation rupture $\leq L_2/3$ in brittle failure	Test temperature	23 °C	ISO 13954 or ISO 13955
Cohesive resistance for electrofusion saddle fittings	Surface rupture: $\leq 25\%$ , brittle failure	Test temperature	23 °C	ISO 22621-3 Annex D
Tensile strength for — butt fusion fittings — spigot end fittings	Test to failure: — ductile: pass — brittle: fail	Test temperature	23 °C	ISO 13953

### 4.2.3 Fitness for purpose for transition fittings

#### 4.2.3.1 Leaktightness test

The transition joint shall be leak-free when leak tested at 0,5 bar and at a minimum of 1,5 MOP at both  $(23 \pm 2) ^\circ\text{C}$  and  $(-29 \pm 2) ^\circ\text{C}$  in accordance with C.3.

#### 4.2.3.2 Leaktightness with temperature cycling

The transition joint shall be leak-free after 10 temperature cycles as tested at 0,5 bar and a minimum of 1,5 MOP in accordance with C.5.

#### 4.2.3.3 Leaktightness after tensile pull test

**4.2.3.3.1** Transition joints in transition fittings and anodeless risers in PA sizes less than 110 mm shall be qualified under this requirement if the pipe is pulled to a minimum of 25 % elongation, as indicated by when the length of the unrestrained PA piping has been elongated to 125 % of its original length, when tested in accordance with C.4, and is bubble tight in accordance with 4.2.3.3.3. No leakage or pullout is permitted.

**4.2.3.3.2** For PA sizes 110 mm and greater, the joint shall be qualified by pull testing to tensile stress equal to, or greater than, the maximum tensile stress that would be produced by a temperature change of  $38 ^\circ\text{C}$  when tested in accordance with C.4. No leakage or pullout is permitted in accordance with 4.2.3.3.3. Failure of one sample constitutes failure of this test.

**4.2.3.3.3** The transition joint shall be leak tested at 0,5 bar and a minimum of 1,5 MOP, prior to and at the end of the test, while still under tensile load and immediately following the tensile test. No leakage shall be permitted when tested in accordance with C.4.

**4.2.3.3.4** Each nominal size transition design, in PA, shall be tested, except testing of the heaviest wall PA piping shall qualify all thinner wall PA pipe joints of the same outside diameter.

#### 4.2.3.4 Leaktightness after constant tensile load joint test

The transition joint shall be leak tested at 0,5 bar and a minimum of 1,5 MOP, prior to, at the end of the test while still under tensile load, and immediately following the constant tensile load (CTL) joint test according to C.6. No leakage shall be permitted when tested in accordance with C.3.

## 5 Overall service (design) coefficient

The minimum value of the overall service (design) coefficient,  $C$ , for pipes and fittings for the supply of gaseous fuels shall be 2, or higher values according to national regulations.

To this value other coefficients may be applied, taking into account different aspects, such as:

- a) operating temperature range;
- b) specific material aspects;
- c) storage and laying conditions.

NOTE For information about derating coefficients for other operating temperatures, see Annex D.

## Annex A (normative)

### Preparation of test assemblies by butt fusion

#### A.1 General

This annex specifies a method for preparing butt fusion jointed test piece assemblies between PA pipes and spigot-ended fittings.

#### A.2 Pipes used for test assemblies

The pipes used for test assemblies shall be taken from straight lengths.

#### A.3 Conditioning

Condition the pipes used for test assemblies at temperature  $T_a$  (see Table A.3) for a period of time according to Table A.1.

**Table A.1 — Conditioning periods**

Thickness, $e_n$ mm	Minimum conditioning period h
$e_n < 3$	1
$3 \leq e_n < 8$	3
$8 \leq e_n < 16$	6
$16 \leq e_n < 32$	10
$32 \leq e_n$	16

#### A.4 Apparatus

The butt fusion machine used shall be fitted with an automatic fusion-pressure controller enabling the pressure to be kept constant during the whole of Phases 1, 2 and 5 of the fusion cycle.

#### A.5 Jointing procedure

Using straight pipes and fittings conforming to ISO 22621-2 and ISO 22621-3, as applicable, join the components as follows, deviations from the procedure being permitted to demonstrate improvements in joint performance (appearance or mechanical properties).

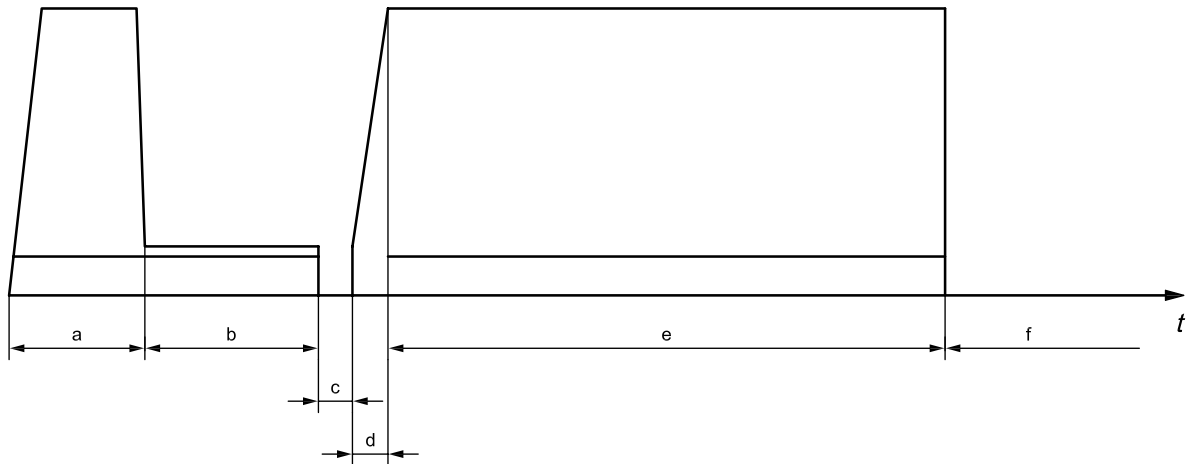
- a) Fix the pipes or fittings in the butt fusion machine in such a manner as to obtain a misalignment  $\Delta a$  of, at the most, 0,5 mm when  $d_n < 200$  mm or at the most 0,1 $e_n$  or 1 mm, whichever is the greater, when  $d_n \geq 200$  mm.
- b) Prepare and plane the butt fusion faces by means of a planing machine to obtain a maximum clearance  $\Delta w$  of 0,3 mm when  $d_n < 200$  mm or 0,5 mm when  $d_n \geq 200$  mm.



- c) Perform the butt fusion using the parameters specified in Table A.2, repeating the procedure on fresh test assemblies while varying the parameters within the limits given in Table A.4.
- d) Proceed to the tests as given in this part of ISO 22621.

## A.6 Butt fusion cycle and parameters

Figure A.1 illustrates the butt fusion cycle and Tables A.2 and A.3 give reference values for the parameters in each phase.



### Key

- $t$  time
- a Phase 1.
- b Phase 2.
- c Phase 3.
- d Phase 4.
- e Phase 5.
- f Phase 6.

Figure A.1 — Butt fusion cycle

**Table A.2 — Butt fusion cycle and parameters**

Parameter		Value	Unit
Heater-plate temperature, $T$		240 ± 20	°C
Phase 1	Pressure, $p_1^a$	0,3 ± 0,1	MPa
	Time, $t_1$	Measured as the time until $B_1$ is reached	s
	Bead width, $B_1$	$d_n \leq 110$ : $0,5 < B_1 \leq 1,5$ $110 < d_n \leq 180$ : $2 < B_1 \leq 4$	mm mm
Phase 2	Pressure, $p_2^a$	0,03 ± 0,02	MPa
	Time, $t_2$	$(30 + 0,5d_n) \pm 20$	s
Phase 3	Time, $t_3$	Maximum value: 3	s
Phase 4	Time, $t_4$	Maximum value: 3	s
Phase 5	Pressure, $p_5^a$	0,3 ± 0,1	MPa
	Time, $t_5$	12 ± 3	min
Phase 6	Time, $t_6$	Minimum value: $1,5e_n$	min
		Maximum value: 20	min
<sup>a</sup> This pressure is the interface pressure and is related to $d_n$ , $e_n$ and the butt fusion equipment used.			

**Table A.3 — Wall thickness dependent butt fusion parameters<sup>a</sup>**

Wall thickness, $e_n$ mm	$B_1$ mm	$t_2$ s	$t_3$ s	$t_4$ s	$t_5$ min
≤ 4,5	0,5	45	5	5	6
$4,5 < e_n \leq 7$	1,0	45 to 70	5 to 6	5 to 6	6 to 10
$7 < e_n \leq 12$	1,5	70 to 120	6 to 8	6 to 8	10 to 16
$12 < e_n \leq 19$	2,0	120 to 190	8 to 10	8 to 11	16 to 24
$19 < e_n \leq 26$	2,5	190 to 260	10 to 12	11 to 14	24 to 32
$26 < e_n \leq 37$	3,0	260 to 370	12 to 16	14 to 19	32 to 45
<sup>a</sup> If other parameters are considered, they are subject to agreement between the pipe/fitting manufacturer and the end-user.					

Table A.4 gives the limits placed on the values of the parameters used in evaluating the jointing procedure.

**Table A.4 — Limits on values of butt fusion parameters**

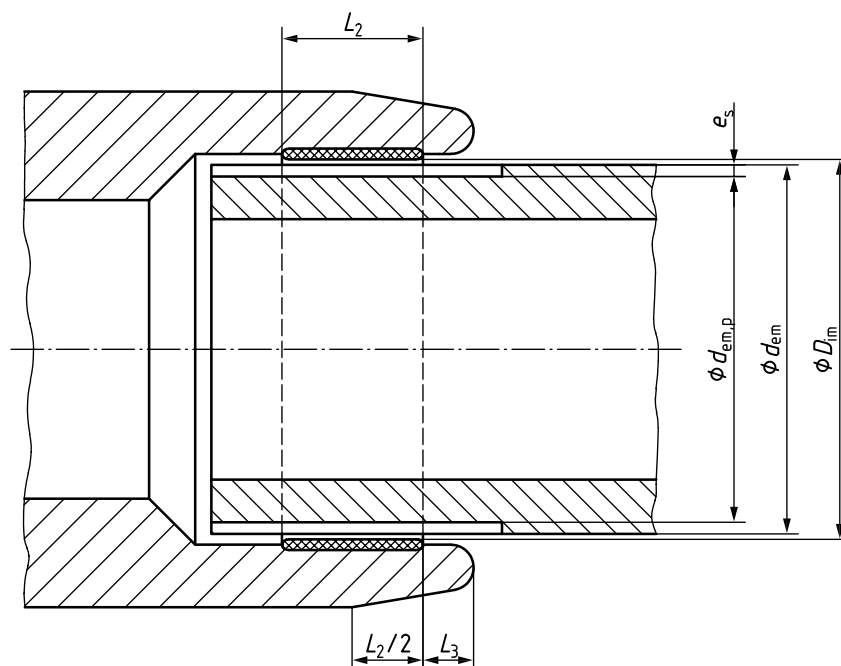
Set of conditions	Condition	Ambient temperature		Heater plate temperature, $T$ °C	Butt fusion pressure, $p$ N/mm <sup>2</sup>
		Symbol	Value, °C		
1	Nominal	$T_{nom}$	23 ± 2	260 ± 2	0,5 ± 0,02
2	Minimum	$T_{min}$	0 ± 2	265 ± 2	0,6 ± 0,02
3	Maximum	$T_{max}$	40 ± 2	255 ± 2	0,4 ± 0,02

## Annex B (normative)

### Preparation of test assemblies by electrofusion

#### B.1 General

This annex specifies a method for the preparation of test pieces assembled from PA pipes or spigot-ended fittings and electrofusion fittings.



#### Key

$$D_{im} = (D_{i,max} + D_{i,min})/2$$

$$d_{em} = C/\pi \text{ where } C \text{ is the circumference of the unscrapped pipe}$$

$$d_{emp} \text{ (by analogy)} = C_p/\pi \text{ where } C_p \text{ is the circumference of the pipe to be assembled with the fitting}$$

$$e_s = (d_{em} - d_{emp})/2$$

$L_2$  nominal length of the fusion zone

$L_3$  length of the unheated section of the socket

Figure B.1 — Dimensions of an electrofusion socket

#### B.2 Clearances

##### B.2.1 Socket fittings

$C_1$ , the clearance between fitting bore and outside diameter of unscrapped pipe, is given by Equation (B.1):

$$C_1 = D_{im} - d_{em} \quad (\text{B.1})$$

$C_2$ , the clearance between fitting bore and outside diameter of scraped pipe, is given by Equation (B.2):

$$C_2 = C_1 + 2 e_s \quad (\text{B.2})$$

NOTE 1  $C_2$  can be obtained by machining the unscraped pipe to bring its mean outside diameter,  $d_{em}$ , to the value  $d_{emp}$  calculated from Equation (B.3), see B.3.1, third paragraph.

$$d_{emp} = D_{im} - C_2 \quad (\text{B.3})$$

$C_3$ , the maximum theoretical clearance between fitting bore and outside diameter of unscraped pipe, is given by Equation (B.4):

$$C_3 = D_{im,max} - d_e \quad (\text{B.4})$$

$C_4$ , the maximum theoretical clearance between fitting bore and outside diameter of scraped pipe, is given by Equation (B.5):

$$C_4 = C_3 + 2 e_s \quad (\text{B.5})$$

NOTE 2  $C_4$  may be obtained by machining the unscraped pipe to bring its mean outside diameter,  $d_{em}$ , to the value  $d_{emp}$  calculated from Equation (B.6):

$$d_{emp} = D_{im} - C_4 \quad (\text{B.6})$$

## B.2.2 Saddles

The clearance between saddle fittings and pipes is assumed to be zero.

## B.2.3 Ambient temperature

—  $T_a$  ambient temperature at which a joint is made

The ambient temperature may vary from the minimum temperature,  $T_{min}$ , to the maximum temperature,  $T_{max}$ , as specified by agreement between the manufacturer and the purchaser.

- $T_R$  reference ambient temperature of  $(23 \pm 2) ^\circ\text{C}$ ;
- $T_{max}$  maximum permitted ambient temperature for joint assembly;
- $T_{min}$  minimum permitted ambient temperature for joint assembly.

## B.2.4 Determination of fusion-jointing electrical parameters

NOTE Using the voltage tolerances specified in ISO 12176-2<sup>[1]</sup>.

### B.2.4.1 Maximum energy input at ambient temperature, $T_a$

For control boxes using voltage control, the applied voltage is given by Equation (B.7):

$$V_{max} \sqrt{\frac{R}{R_{min}}} \quad (\text{B.7})$$

where

$V_{max}$  is the maximum control-box output voltage, in volts (nominal + tolerance);

$R_{\min}$  is the manufacturer's stated minimum fitting resistance, in ohms, at  $T_R$ ;

$R$  is the resistance, measured using a four-arm resistance bridge with the performance characteristics specified in Table B.1, of the fitting conditioned at the ambient temperature,  $T_a$ , specified for jointing.

**B.2.4.2 Minimum energy input at ambient temperature,  $T_a$**

For control boxes using voltage control, the applied voltage is given by Equation (B.8):

$$V_{\min} \sqrt{\frac{R}{R_{\max}}} \tag{B.8}$$

where

$V_{\min}$  is the minimum control-box output voltage, in volts (nominal – tolerance);

$R_{\max}$  is the manufacturer's stated maximum fitting resistance, in ohms, at  $T_R$ ;

$R$  is the resistance, measured using a four-arm resistance bridge with the performance characteristics specified in Table B.1, of the fitting conditioned at the ambient temperature,  $T_a$ , specified for jointing.

The procedure for measuring the coil resistance implies the use of measuring equipment at the reference ambient temperature of  $(23 \pm 2)^\circ\text{C}$ , conditioning of the fitting at  $T_{\max}$  or  $T_{\min}$  and measurement of the resistance of the coil of the fitting within 30 s of removal from the conditioning enclosure.

**Table B.1 — Resistance-bridge performance characteristics**

Range $\Omega$	Resolution $\text{m}\Omega$	Accuracy
0 to 1	0,1	0,25 % of reading
0 to 10	1	0,25 % of reading
0 to 100	10	0,25 % of reading

**B.3 Joint assembly**

**B.3.1 General**

The joints shall be made using pipes and/or spigot-ended fittings conforming to ISO 22621-2 and ISO 22621-3, as applicable, and electrofusion fittings for which the dimensions conform to ISO 22621-3. The preparation of the assembly for testing shall be carried out in accordance with the electrofusion fitting manufacturer's written procedures.

Unless a greater scraping depth is recommended by the manufacturer, the minimum scraping depth,  $e_s$ , shall be 0,2 mm.

In cases where the pipes do not need to be scraped, the minimum scraping depth,  $e_s$ , may be zero.

**B.3.2 Procedure**

Carry out the following procedure, where steps d) and f) shall be carried out in a temperature-controlled environment maintaining the temperature to within  $\pm 2$  °C and large enough to contain the fitting, the pipes and the holding apparatus. Fittings shall not be used within 170 h of manufacture.

- a) Measure, at the reference temperature,  $T_R$ , the parts to be joined to determine the dimensional characteristics defined in 3.3 (Symbols for the preparation of test assemblies by electrofusion) and illustrated in Figure B.1.
- b) Prepare the pipes to achieve the necessary clearance conditions, at the reference temperature,  $T_R$ , as given in B.2.
- c) Mount the fitting on the pipes in accordance with the manufacturer's instructions.
- d) Condition the assembly and the associated apparatus for a period conforming to Table B.2 at the applicable ambient temperature,  $T_a$ , specified in Table B.3.

**Table B.2 — Conditioning periods**

Nominal wall thickness, $e_n$ mm	Minimum conditioning period h
$e_n < 3$	1
$3 \leq e_n < 8$	3
$8 \leq e_n < 16$	6
$16 \leq e_n < 32$	10
$32 \leq e_n$	16

- e) After conditioning, measure the resistance of the heating coil and determine the values of the electrical parameters in accordance with Table B.3 and B.2.4. The procedure for measuring the coil resistance implies the use of measuring equipment at the reference ambient temperature,  $T_R$ , with the fitting at the conditioning temperature.
- f) With the assembly conditioned at ambient temperature,  $T_a$ , carry out the fusion jointing in accordance with the fitting manufacturer's instructions at the energy levels indicated in Table B.3.
- g) Leave the joint to cool until it reaches ambient temperature.
- h) Proceed to the tests as given in this part of ISO 22621.

**Table B.3 — Conditions for pipe and fitting preparation**

Set of conditions	Ambient temperature, $T_a$	Pipe configuration	Clearance <sup>a</sup>	Energy	Assembly load <sup>b</sup>
1	$T_R$	Coiled or straight pipe as supplied	$C_2$	reference	usual
2.1	$T_{min}$	Straight pipe	$C_4$	nominal	usual
2.2	$T_{min}$	Straight pipe	$C_4$	minimum	minimum
3.1	$T_{max}$	Straight pipe	$C_2$	nominal	usual
3.2	$T_{max}$	Straight pipe	$C_2$	maximum	maximum
4	$T_{max}$	Straight pipe	$C_4$	minimum	minimum
5	$T_{min}$	Coiled or straight pipe as supplied	$C_2$	maximum	maximum

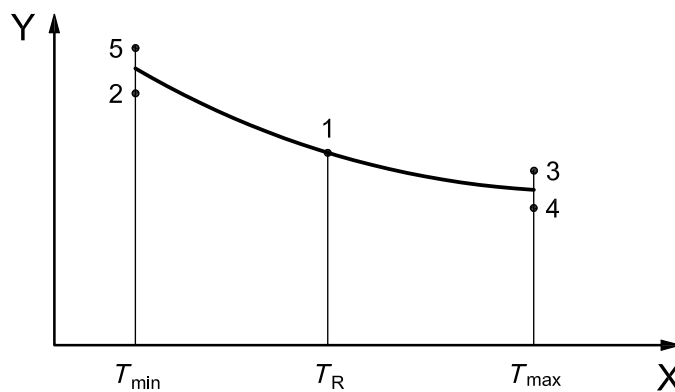
NOTE Sets of conditions 1 to 5 are applicable to the energy profiles illustrated in Figures B.2 and B.3.

<sup>a</sup> In the case of saddles, the clearance shall be considered to be zero.

<sup>b</sup> Applicable to joints with saddles, where the load can be controlled.

**B.4 Diagrammatic representation of variation in fusion energy with ambient temperature**

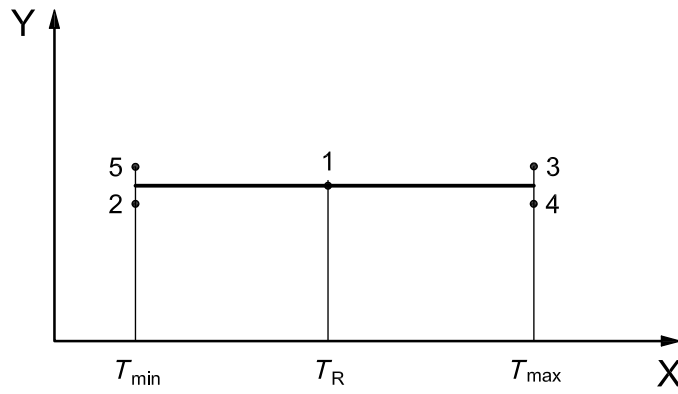
Figures B.2 and B.3 illustrate different forms of energy profile (see Table B.3).



**Key**

- X temperature
- Y fusion energy

**Figure B.2 — Profile with continuous adjustment of energy**



**Key**

X temperature

Y fusion energy

**Figure B.3 — Constant-energy profile**

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## Annex C (normative)

### Test methods for the assessment of fitness for purpose of transition fittings

#### C.1 Test pieces

Unless otherwise specified by the applicable test method, six test specimens shall be tested.

#### C.2 Conditioning and test conditions

Unless otherwise specified by the applicable test method, the test pieces shall be conditioned for at least 16 h at 23 °C and 50 % relative humidity in accordance with ISO 291 before testing.

Unless otherwise specified by the applicable test method, the test procedure shall be carried out at  $(23 \pm 2)$  °C.

#### C.3 Leaktightness testing

Pressurize the test specimen using air or other inert gas.

**WARNING — For large diameter test specimens, it is prudent to first fill the specimen with a coarse granular solid to reduce the pressurized volume of the sample. Plastic granules are frequently used for this purpose.**

Ensure that all end caps and test fittings are bubble tight.

Detect leakage of the transition joint in accordance with the applicable test method. Conduct leak testing for 2 min.

#### C.4 Tensile pull testing

Affix the transition joint area of the transition fitting or anodeless riser in a tensile apparatus in accordance with ISO 6259-1 capable of subjecting the joint to a constant pull rate of  $(5 \pm 25 \%)$  mm/min.

Tensile pull test the transition joint at a constant pull rate of  $(5 \pm 25 \%)$  mm/min.

Return the tensile machine crosshead to the original position; remove the transition.

#### C.5 Temperature cycling testing

**C.5.1** Conduct tests on six of the smallest and six of the largest nominal outlet pipe sizes of each transition design used in transition fittings or anodeless risers.

**C.5.2** Leak test specimens at ambient temperature at 0,5 bar and a minimum of 1,5 MOP in accordance with C.3.

**C.5.3** Condition test specimens to a temperature of  $(-29 \pm 2)$  °C and maintain for a minimum of 2,5 h.

**C.5.4** Condition specimens to a temperature of  $(60 \pm 2)$  °C and maintain for a minimum of 2,5 h.

**C.5.5** Repeat C.5.3 and C.5.4 for a total of ten cycles.

**C.5.6** After the tenth cycle is completed, pressurize 50 % of the test specimens of each size at 0,5 bar and the remaining 50 % of each size at 1,5 MOP of the piping material and SDR for which the transition fittings are designed to be used. Leak test first at  $(60 \pm 2)$  °C and then at  $(-29 \pm 2)$  °C. Condition the test specimen at leak test temperature for at least 4 h prior to testing.

## **C.6 Tensile testing under constant tensile load at 80 °C**

**C.6.1** For each transition joint, use PA pipe of length (not counting the transition fitting and the clamping jaws) equivalent to at least two times the nominal outside diameter of the pipe, but a maximum of 250 mm.

**C.6.2** Mount the transition fitting assembly in a fixture capable of applying a constant longitudinal tensile force to the pipe(s) and fitting. The fitting shall be held in such a way that no distortion or support of any of the fitting components can occur.

**C.6.3** Suspend the fitting assembly, subjected to a longitudinal force (end load) corresponding to a stress of 14,2 MPa at  $(80 \pm 5)$  °C applied gradually within a time period of  $(5 \pm 1)$  min and then maintained for 1 000 h.

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## Annex D (normative)

### Derating coefficients for operating temperatures

Derating factor (DF) is a coefficient used in the calculation of the maximum operating pressure (MOP), which takes into account the influence of operating temperature.

Table D.1 gives derating coefficients for various operating temperatures.

**Table D.1 — Temperature derating coefficients**

Temperature °C	Derating coefficient DF
20	1,0
30	1,1
40	1,25

For other temperatures between each step, linear interpolation is permitted.

The calculation of MOP for a given operating temperature is based on Equation (D.1):

$$MOP = \frac{20 \times MRS}{(SDR-1) \times C \times D_F} \quad (D.1)$$

in which the value of the overall service coefficient,  $C$ , should be not less than 2.

## Bibliography

- [1] ISO 12176-2, *Plastics pipes and fittings — Equipment for fusion jointing polyethylene systems — Part 2: Electrofusion*
- [2] ISO 15439-1, *Plastics piping systems for the supply of gaseous fuels for maximum operating pressure up to and including 0,4 MPa (4 bar) — Polyamide (PA) — Part 1: General*
- [3] ISO 15439-2, *Plastics piping systems for the supply of gaseous fuels for maximum operating pressure up to and including 0,4 MPa (4 bar) — Polyamide (PA) — Part 2: Pipes*
- [4] ISO 15439-3, *Plastics piping systems for the supply of gaseous fuels for maximum operating pressure up to and including 0,4 MPa (4 bar) — Polyamide (PA) — Part 3: Fittings*

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