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## Implants for surgery — Roentgen stereophotogrammetric analysis for the assessment of migration of orthopaedic implants

*Implants chirurgicaux — Analyse stéréophotogrammétrique Roentgen pour l'évaluation de la migration des implants orthopédiques*

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# Foreword

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The committee responsible for this document is ISO/TC 150, *Implants for surgery*, Subcommittee SC 4, *Bone and joint replacement*.

# Introduction

Since its introduction in 1974,[1] roentgen stereophotogrammetric analysis (RSA) has been widely used to assess migration of orthopaedic implants. It is a highly accurate method of quantifying three-dimensional migration between an implant and the bone it is fixed in. RSA is also used in other applications such as measuring migration between bone fragments in e.g. bone fracture studies, and measuring wear of implants. These applications are not within the scope of this International Standard.

Several studies have found implant migration to be predictive of long-term implant survival and, for most devices, measurement over two years might therefore provide a surrogate outcome measure with relatively low numbers of subjects, e.g. less than 50 patients in each group in randomized studies.[2][3] [4] A smaller number of subjects can be used in these studies as a consequence of the high accuracy of the measurement technique. Because of this, RSA is an important technique in early clinical trials for screening new joint replacement prostheses.

However, results from these early clinical trials are difficult to compare as different studies report their results in different formats. To facilitate comparison of outcome reported from different research groups and because the results are obtained using different methodological procedures, there is a need for standardization of RSA investigations.

The RSA method described in this International Standard requires the use of X-rays and exposes the patient to a greater X-ray exposure dose with its associated health risk. For this reason, it is neither the intention of this International Standard to recommend the routine use of RSA nor to add to existing regulatory requirements. Rather it is the intention that when RSA is used in a standardized manner, the results can be as useful and as widely applicable as possible.

# Implants for surgery — Roentgen stereophotogrammetric analysis for the assessment of migration of orthopaedic implants

**CAUTION — The RSA method described in this International Standard requires the use of X-rays and exposes the patient to a greater X-ray exposure dose with its associated health risk. Careful consideration of the benefits and drawbacks of this method on a case by case basis is advisable.**

## 1   Scope

This International Standard provides requirements for the clinical assessment of migration of orthopaedic implants with roentgen stereophotogrammetric analysis (RSA).

## 2   Terms and definitions

For the purposes of this document, the following terms and definitions apply.

**2.1**
**absolute movement**
movement of a rigid body relative to a fixed reference rigid body

**2.2**
**accuracy**
closeness of agreement between a measured quantity value and a true quantity value of a measurand

**2.3**
**bias**
estimate of a systematic measurement error

**2.4**
**biplanar technique**
RSA technique where two X-ray cassettes/films/sensors are set at an angle to each other

**2.5**
**calibration cage**
calibration box
reference frame used to create a three-dimensional coordinate system, with definition of position and orientation, and to determine the position of the two roentgen foci

**2.6**
**condition number**
calculated number used to assess the distribution of markers

Note 1 to entry: High condition numbers indicate poor marker distribution, while low condition numbers indicate appropriate marker distribution.

Note 2 to entry: See Annex A, which establishes the methodology to determine the condition number associated with the marker distribution.

**2.7**
**crossing line error**
shortest distance between the two X-rays projecting the centre of a marker in the two RSA images

**2.8**
**double examinations**
two RSA examinations of the same patient within an interval of several minutes

**2.9**
**helical axis**
screw axis
instantaneous axis about which the decomposition of the motion of an object from one position to another has a translation along and a rotation about a single axis

**2.10**
**marker**
small diameter biocompatible metal sphere having a precise size and shape used as landmark

Note 1 to entry: Spherical tantalum markers serve as well-defined landmarks.

Note 2 to entry: The diameter is commonly ≤ 1 mm.

**2.11**
**maximum total point motion**
**MTPM**
length of the translation vector of the marker or virtual marker in a rigid body that has the greatest migration

Note 1 to entry: It can only have positive values, and is not normally distributed.

**2.12**
**mean error of rigid body fitting**
rigid body error
measure indicating the mean change of relative positions of markers (in the same object) over time compared to the initial, reference configuration

Note 1 to entry: Annex A establishes the methodology to determine the mean error associated with the change of relative positions of markers.

**2.13**
**migration**
change in position and orientation of an implant relative to the host bone assessed between follow-up examinations

**2.14**
**model-based RSA**
RSA technique in which the position and orientation of an implant is assessed by matching a virtual projection of a three-dimensional model of the implant to the actual radiographic projection of the implant

**2.15**
**phantom**
object that is used as a representative of an anatomical part

**2.16**
**precision**
degree to which repeated measurements under unchanged conditions show the same results

**2.17**
**reference plate**
planar object holding markers used for calibration of RSA-examinations by linking its two-dimensional coordinate system to the three-dimensional global coordinate system of previous RSA-examinations that were calibrated using a three-dimensional calibration cage

**2.18**
**reference rigid body**
rigid body that defines a fixed coordinate system, the origin of which is located in that rigid body's geometrical centre

**2.19**
**rotation matrix**
mathematical expression of the three-dimensional rotation of a rigid body

**2.20**
**RSA**
**roentgen stereophotogrammetric analysis**
radiostereometry
radiostereometric analysis
roentgen stereophotogrammetry
measurement technique that relies on stereo X-ray images and can be used to assess relative changes in position and orientation of two rigid bodies (e.g. an orthopaedic implant and host bone) relative to each other

Note 1 to entry: In order to reach a high level of accuracy, markers are used as landmarks in the bone and a calibration object (calibration cage or reference plate) is used to assess the position of two synchronised X-ray sources in the global coordinate system defined by the calibration cage.

**2.21**
**virtual marker**
three-dimensional point from visible landmarks or calculated from known geometry to determine a specific point of an implant

Note 1 to entry: Virtual markers were formerly named fictive markers.

**2.22**
**uniplanar technique**
RSA technique where the two X-ray cassettes/films/sensors are in the same plane

## 3   Measurement

### 3.1   Size of markers

Spherical markers made of biocompatible (implant grade) metal and having a high radio-opacity (e.g. tantalum) shall be used to serve as landmarks. Marker diameters of 0,5 mm, 0,8 mm and 1,0 mm are generally used.

### 3.2   Virtual markers

Virtual markers indicate a specific part of the implant and facilitate comparison of migration data within and between studies.

EXAMPLE 1     Within a clinical RSA study of a specific implant, these virtual markers are valuable if one or more implant markers of a certain patient are obscured in the X-ray or have become loose.

In different RSA studies, different prosthesis designs might have markers attached at different locations. In order to compare the translation of specific points on the implant's surface between different implant designs, virtual markers can be used.

EXAMPLE 2     To compare the translation of a specific point, on the tip of different hip stems.

A virtual marker is defined by the observer. Its position is indicated in both images of a single RSA-examination, and the three-dimensional position of the virtual marker is reconstructed according to the common approach of reconstructing the position of an actual prosthesis marker. It is advised that the crossing line error is less than 1 mm. A new rigid body is formed when the position of the virtual marker is combined with the positions of at least three prosthesis markers. This enables the translation of the virtual marker to be determinable in subsequent (or previous) RSA examinations. Therefore, virtual markers are defined such that they move with the implant and they can be used to calculate the translation of this specific point of the prosthesis based on the migration of the implant itself.

## 3.3 Number and distribution of markers

In order to assess translations and rotations with all six degrees of freedom, markers shall be implanted on each rigid body under study so that they are not collinear. For each rigid body, at least three identical markers shall be visible on both radiographs at all examinations.

NOTE 1    In cases where only one or two markers can be used in one of the rigid bodies, only translations can be calculated.

NOTE 2    It is strongly advised to insert at least six to seven bone markers as markers may be obscured by the implant.

## 3.4 Mean error of rigid body fitting

The upper limit of acceptable mean error of rigid body fitting shall be related to the marker configuration of the segment (defined by its condition number). The upper limit accepted shall be reported and should typically not exceed 0,35 mm.

## 3.5 Condition number

For studies of hip, knee and shoulder prostheses, condition numbers shall be below 120.

For studies of small joints, such as in the fingers and the cervical spine, condition numbers shall preferably be below 150. For studies in which these high condition numbers are accepted, it is essential that the precision of the measurements is validated (see 11.2).

## 3.6 Three-dimensional implant models

Model-based RSA techniques do not require the attachment of metal markers to the implant but require an accurate 3D representation of the implant.[7][8] If the model-based techniques are to be used, they shall have been properly evaluated and the precision and bias of these measurements shall have been published in established journals.

## 4 Radiographic arrangement

It shall be indicated whether a uniplanar or a biplanar technique is used. For a biplanar technique, the angle between the recording media needs to be presented. Any other arrangement shall be described in detail.

## 5 Calibration cages and reference plates

Routinely, biplanar calibration cages or uniplanar calibration cages are used.

If cages are used that have not been described previously in scientific papers, this shall be stated in the report. The data shall include the dimensions of the cage, the accuracy of marker placement on the cage, and the cage material.

If calibration examinations and reference plates have been used, the equivalent data (dimensions of the plate, the accuracy of marker placement on the plate, and the plate material) shall be presented for the reference plates.

If any other type of cage is employed, these specific cages shall also be evaluated in experiments that use a phantom object holding a number of stable tantalum markers and that is positioned in a reasonable range of poses that represent the clinical range of poses that can be encountered.

## 6    Radiographs

### 6.1    General

Radiographs can either be analogue or digital.

If the authors use analogue radiographs in combination with manual measurements using a measuring table, the accuracy of the measuring table shall be stated. Information about the brand, type and manufacturer of the measuring table used shall also be given.

If analogue images have been scanned, the spatial resolution and gray-scale resolution have to be presented. Information about the brand, type and manufacturer of the film scanner used shall also be given.

If digital imaging systems have been used, information on the spatial and gray-scale resolution shall be presented. Information about the brand, type and manufacturer of the digital imaging system used shall also be given.

NOTE        A minimum 150 dots per inch spatial resolution and 8 bit gray scale resolution is suggested.

### 6.2    Double examinations

Between two examinations, the patient shall be repositioned within limits that are expected to be encountered during a clinical follow-up study. Double examinations will be performed under unloaded or repeatable loading conditions. In this short time interval, the implant will not have moved with respect to the host bone. Due to measurement errors, however, apparent migration will be calculated. Double exam results are used to determine precision for the system as defined in 11.2.

## 7    Software

To compute the three-dimensional position of bone markers, implants or parts of implants, several different software packages are available. These software packages shall have appropriate documentation and validation of their accuracy and precision. This should be provided by the producer of the software, but additional independent validation studies would be valuable. If custom-made software has been used, a validation study of this software shall be fully described in an established journal before it is used in any clinical study.

## 8    Coordinate systems

### 8.1    Global coordinate system

The calibration cage defines the position and orientation of the global coordinate system. For the reference examination (usually the first examination), the body region of interest (e.g. the proximal femur), which contains the reference rigid body segment markers, should be aligned as closely as possible with the global axis system (e.g. parallel to one of the global axes). This would aid the interpretation of implant migration directions in terms of standard medical terminology (e.g. distal translation, internal rotation). In order to obtain optimum precision, it would be preferable if the region of interest for subsequent examinations were similarly aligned, as closely as possible, with the same global axis.

### 8.2    Implant coordinate system

The local implant coordinate system is commonly aligned with the global coordinate system with its origin either on a point of the implant or, if the implant has markers attached, at the geometric centre of the markers. When using such a coordinate system in migration calculations the migration results between patients are less influenced by patient positioning. In cases where such an implant coordinate system (that is not aligned with the global coordinate system) is used, this coordinate system shall be described, as well as the possible effects on the migration calculations.

## 8.3   Reference rigid body

When migration is evaluated, the host bone shall be considered to be the reference rigid body. If this is not the case, the reference rigid body shall be described. Any deviation from this approach shall be documented.

# 9   Migration

## 9.1   Translations

Translations can be expressed concisely as the components of migration along the orthogonal directions using the implant coordinate system as defined in 8.2. By convention, in order to associate the coordinate system with anatomical directions, the coordinate system is situated on the patient's right side, with positive X being medial, positive Y being proximal and positive Z being anterior. Using this convention, the medial translation of an implant on the patient's left side will be negative, while proximal and anterior translation will remain positive (see Figure 1). Any non-standard orthogonal directions shall be described, as well as the possible effects on the migration calculation.

In case it is necessary to combine results of implants from the patient's right side with implants from the patient's left side, the sign of X-translation for the left side of the patient is to be changed. Translations shall be reported as if it were on the right hand side.

When translations are presented, it is mandatory to account for the chosen point of measurement, either a single marker, the origin of the implant coordinate system, or a virtual marker. The point(s) used to calculate translations of a rigid body shall be standardized and used at all follow-up occasions in all patients.

## 9.2   Rotations

### 9.2.1   General

The implant coordinate system on the patient's right side, as described in 9.1 and shown in Figure 1, is also used to define positive rotations. A positive rotation is defined as being clockwise about an axis when viewing that axis in a direction away from its origin (this is referred to as the right-hand screw rule).

EXAMPLE      For hip stems, on the patient's right side, positive rotation about the x-axis would be extension, about the y-axis it would be internal rotation, and about the Z-axis it would be adduction (Figure 1). On the patient's left side, extension would remain positive, but internal rotation would become negative (i.e. positive external rotation), and adduction would become negative (i.e. positive abduction).

To combine results of left and right prostheses, the signs of the rotations about the y-axis and Z-axis for the left side prostheses shall be changed to comply with anatomical directions and all calculations shall be performed respecting the orthogonal right-hand coordinate system.

In order to clinically interpret the rotation matrix, it is resolved in rotations about three orthogonal axes. The three-dimensional rotation shall be described using three angles, using the Euler sequence rotation XYZ.

NOTE 1      According to Euler's rotation theorem, any three-dimensional rotation may be described using three angles.

NOTE 2      The angle calculations are sequence rotation dependent.

### 9.2.2   Helical axis

In case rotational migration of the implant is smaller than 4°, helical axes shall not be used as they are inaccurate for these small rotations.[9]

# 10 Maximum total point motion

## 10.1 General

In any scientific communications it shall be stated which points have been used to assess MTPM. It shall also be stated that in successive follow-up measurements, different points in the rigid body may have experienced the greatest motion.

NOTE    MTPM not only depends on the amount of migration of an implant, but also on the location of the points of measurement. If these points do not correspond between two different implant designs, any comparison will become incorrect.
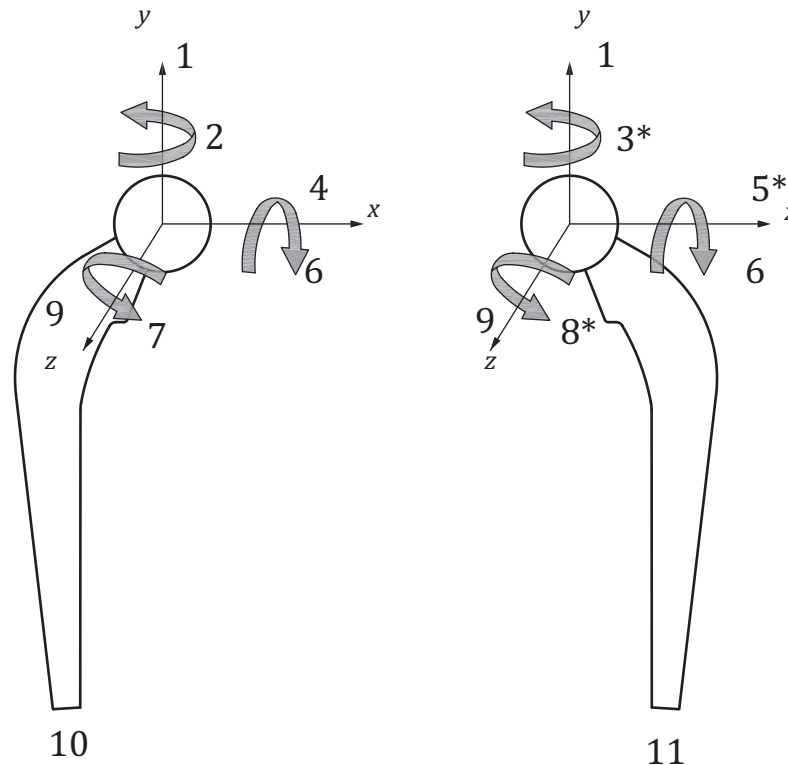
**Key**

| | | | |
|---|---|---|---|
| 1 | proximal | 7 | adduction |
| 2 | internal rotation | 8 | abduction |
| 3 | external rotation | 9 | anterior |
| 4 | medial | 10 | right hip |
| 5 | lateral | 11 | left hip |
| 6 | extension | | |

NOTE 1    Arrows represent positive direction.

NOTE 2    Asterisks on the left hand side indicate the values that need to be multiplied by −1 in order for the anatomical directions to agree with those on the right.

**Figure 1 — Schematic overview of the use of coordinate systems in defining migration of hip stems**

## 10.2 Signed versus unsigned values

In RSA, translation and rotation parameters shall be presented as signed values.

NOTE    Since MTPM is a magnitude only, the value is always positive.

However, when unsigned values are used in addition to signed values, one shall check if these values are normally distributed. If that is not the case, medians and min-max ranges shall be quoted.

# 11 Validation

## 11.1 Accuracy

The accuracy of RSA has to be determined by comparison with another method that has a resolution substantially better than that of RSA (preferably with an error of a few µm). Such determinations are important in RSA, and especially when introducing a new RSA method or starting a new RSA laboratory. Different phantoms have been constructed to enable such determinations.[10][11]

NOTE    Phantom experiments are not an alternative to double examinations that are used to assess precision in clinical RSA studies.

## 11.2 Precision

The precision of RSA shall be assessed by double examinations.

As the precision of RSA depends on several factors that might differ between studies, precision shall be assessed for each clinical or preclinical RSA study. In case no ethical approval is given to perform double examinations the reason for this shall be stated.

Although each individual patient has a unique bone marker configuration, it might not be feasible to make double examinations for all patients. However, a minimum of 25 % of the cases evaluated or 15 cases (whichever of the two represents the largest number of patients) shall be evaluated with double examinations.

Precision shall be presented as the standard deviation of these calculated migrations. In general the differences between double examinations are normally distributed, with a mean difference (bias) close to zero. If so, the error shall be presented as the 95 % or 99 % confidence interval around zero. Assuming a normal distribution, the confidence intervals of the error should be expressed as ± 1,96×SD, for the 95 %, or ± 2,58×SD for the 99 % confidence interval (where SD is the standard deviation). In cases where the calculated migrations are not normally distributed, the sample standard deviation as a measure of precision, and the sample mean as the bias shall be reported.

In case the mean is larger than the standard deviation, this bias has to be reported as well.

# 12 Practical issues

## 12.1 Weight bearing

The position of the patient may influence the results of a clinical RSA study. Thus, the positioning of patients shall be standardized on the basis of joint type in order to make results from RSA studies comparable. Weight bearing (or more precisely, load bearing) can affect fixation, especially in bone impaction grafting in revision surgery,[12][13] and in studies evaluating bony integration with surface coatings. Due to the wide variety of lower limb studies, whether weight bearing is used will depend on practicality issues and study design. Any weight bearing and methods of controlling it should be reported

## 12.2 Follow-up intervals

The following follow-up examinations shall be scheduled for any clinical RSA study: within five days postoperatively, preferably before weight bearing, and six months, one year and two years. Any additional follow-up examinations are optional.

Follow-up intervals shall be as similar as possible, but for practical reasons are allowed ± 1 week for follow-up evaluations within the first postoperative year, ± 2 weeks for the one-year evaluation, ± 3 weeks for the two-year evaluation up to the five-year evaluation, and ± 4 weeks for longer follow-up evaluations. If longer intervals are used this should be stated.

## 12.3 Radiation dose

The radiation dose of an RSA examination shall be assessed by a qualified person, and presented to the local ethics committee, and shall be available on request.

## 12.4 Exclusion of patients

There are several reasons for excluding patients from clinical follow-up studies. Due to the technical character of RSA studies, patients can be excluded as a result of technical shortcomings such as poor image quality, poor bone marking, obscuring markers, etc., which can be quantified in the condition number and the rigid body error and become apparent after the post-operative RSA examination has been analysed. It is essential that the reasons for exclusion of patients are documented. The clinical and radiographic follow-up of these excluded patients shall, of course, be guaranteed. The protocol of the study should contain a paragraph stating that patient inclusion in the study will continue until the proper number of patients that are analysable are included in the study.

## 13 Standardised output

To facilitate comparison between different centres using the same method, the items listed below shall be used to account for the results of a clinical RSA study.

1) Translations shall be expressed in millimetres and rotations in degrees.

2) The accuracy and precision of the arrangement used shall be presented. Follow-up intervals shall be quoted. Type of calibration cage and use of reference plates shall be given.

3) Positioning of subject, calibration cage (object), X-ray tubes and X-ray cassettes shall be standardized or described in detail.

4) The coordinate system(s) used in the analysis shall be described.

5) Method of image acquisition shall be stated, e.g. whether scanned (then scanner details shall to be given) or whether digital radiographs have been used (then system details shall be given).

6) Software used shall be stated, and if appropriate which version.

7) Size of marker beads used shall be given.

8) The method of determining the position of the implant, whether based on attached beads or model-based shall be stated. If appropriate, reference to any new/novel technique shall be given.

9) The following shall be stated: cut-off level for condition number and rigid body fitting error for exclusion of subjects from study.

10) The precision of the measurements assessed by double examinations of a sufficient number of patients enrolled in the study shall be stated.

11) Migration data shall be given in terms of translations, and angular rotations. Reporting MTPM is optional. In principle, all six degrees of freedom shall be reported. If not, the authors shall state

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why some data are not reported, and these data shall be available from the authors on request. The point(s) used to measure translations shall be indicated (either a (virtual) marker, or the origin of the implant coordinate system), and its (their) location(s) on the implant (or in the bone) shall always be presented.

# Annex A
## (informative)

## Relevant formulae

## A.1 General

The formulas of condition number and mean error of rigid body fitting presented in this annex are based on References[1] and.[6]

## A.2 Condition number

Let $a_1, \ldots, a_n$, be the three-dimensional positions of n markers (in mm) that are used in the migration calculation of the rigid body.

Denote the mean value vector of $a_i$, i = 1 ., . . ., n, by $\underline{a}$ (the geometrical centre of the markers), and introduce the matrix $A = [a_1 - \underline{a}, \ldots, a_n - \underline{a}]$.

If we assume that the errors in the positions of the markers are small, the condition number with respect to absolute errors in the matrix A is:

$$C_A = \frac{1\,000}{\sqrt{\sigma_2^2 + \sigma_3^2}}$$

where $\sigma_2$ and $\sigma_3$ are the two smallest singular values, in millimetres, resulting from the singular value decomposition of the matrix $A$.

NOTE    The condition number is not dimensionless, so, the multiplication factor of 1 000 in the formula is necessary to calculate the condition number in meters$^{-1}$.

## A.3 Mean error of rigid body fitting

Let $a_1, \ldots a_n$, be the positions of n markers at time point 1 and $b_1, \ldots b_n$, be the positions of the same markers in the same order at time point 2. The mean error of rigid body fitting is defined as:

$$ME = \sqrt{\frac{1}{n}\sum_{i=1}^{n}\varepsilon_i^2}$$

where $\varepsilon_i$ is the distance between the point $b_i$ and $a_i^t$, which is the point $a_i$ transformed by the computed absolute movement. Note that in case this absolute movement is described by a rotation matrix $M$ and a translation vector $d$, the following expression also describes the mean error of rigid body fitting:

$$ME = \sqrt{\frac{1}{n}\sum_{i=1}^{n}\left\| Ma_i + d - b_i \right\|^2}$$

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