INTERNATIONAL STANDARD

ISO 14692-1

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Petroleum and natural gas industries — Glass-reinforced plastics (GRP) piping —

Part 1:

Vocabulary, symbols, applications and materials

Industries du pétrole et du gaz naturel — Canalisations en plastique renforcé de verre (PRV) —

Partie 1: Vocabulaire, symboles, applications et matériaux



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Foreword

ISO (the International Organization for Standardization) is a worldwide federation of national standards bodies (ISO member bodies). The work of preparing International Standards is normally carried out through ISO technical committees. Each member body interested in a subject for which a technical committee has been established has the right to be represented on that committee. International organizations, governmental and non-governmental, in liaison with ISO, also take part in the work. ISO collaborates closely with the International Electrotechnical Commission (IEC) on all matters of electrotechnical standardization.

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The main task of technical committees is to prepare International Standards. Draft International Standards adopted by the technical committees are circulated to the member bodies for voting. Publication as an International Standard requires approval by at least 75 % of the member bodies casting a vote.

Attention is drawn to the possibility that some of the elements of this document may be the subject of patent rights. ISO shall not be held responsible for identifying any or all such patent rights.

ISO 14692-1 was prepared by Technical Committee ISO/TC 67, *Materials, equipment and offshore structures* for petroleum, petrochemical and natural gas industries, Subcommittee SC 6, *Processing equipment and systems*.

ISO 14692 consists of the following parts, under the general title *Petroleum and natural gas industries* — *Glass-reinforced plastics (GRP) piping*:

- Part 1: Vocabulary, symbols, applications and materials
- Part 2: Qualification and manufacture
- Part 3: System design
- Part 4: Fabrication, installation and operation

Introduction

ISO 14692 (all parts) for the use of glass-reinforced plastics (GRP) piping in oil and natural gas industries is based on the document *Specifications and recommended practice for the use of GRP piping offshore* published by the United Kingdom Offshore Operators Association (UKOOA) in 1994. The objective of ISO 14692 (all parts) is to provide the oil and gas industry, and the supporting engineering and manufacturing industry, with mutually agreed specifications and recommended practices for the design, purchase, manufacturing, qualification testing, handling, storage, installation, commissioning and operation of GRP piping systems.

ISO 14692-2, ISO 14692-3 and ISO 14692-4 follow the individual phases in the life cycle of a GRP piping system, i.e. from design through manufacture to operation. Each part is therefore aimed at the relevant parties involved in that particular phase. It is primarily intended for offshore applications on both fixed and floating topsides facilities, but it may also be used as guidance for the specification, manufacture, testing and installation of GRP piping systems in other similar applications found onshore, e.g. produced-water and firewater systems.

- Part 1: Vocabulary, symbols applications and materials. It defines terms and symbols, and identifies the applications that ISO 14692 (all parts) is intended to cover, together with anticipated end users. It also defines limits on the material used for the construction of components and describes the pressure terminology used throughout ISO 14692 (all parts). Main users are envisaged to include all parties in the life cycle of a typical GRP piping system. ISO 14692-1 should be used in conjunction with the part of specific relevance.
- Part 2: Qualification and manufacture. Its objective is to enable the purchase of GRP components with known and consistent properties from any source. Main users of the document are envisaged to be the principal and the manufacturer, certifying authorities and government agencies.
- Part 3: System design. Its objective is to ensure that piping systems, when designed using the components qualified in ISO 14692-2, meet the specified performance requirements. Main users of the document are envisaged to be the principal, design contractors, suppliers contracted to do the design, certifying authorities and government agencies.
- Part 4: Fabrication, installation and operation. Its objective is to ensure that installed piping systems meet the specified performance requirements throughout their operational life. Main users of the document are envisaged to be the principal, fabrication/installation contractors, repair and maintenance contractors, certifying authorities and government agencies.

Petroleum and natural gas industries — Glass-reinforced plastics (GRP) piping —

Part 1:

Vocabulary, symbols, applications and materials

1 Scope

This part of ISO 14692 gives the terms, definitions and symbols used in the specification, manufacture, testing and installation of glass-reinforced plastics (GRP) piping installations associated with offshore applications on both fixed and floating topsides facilities for oil and gas industry production and processing. It also describes the philosophy and provides guidance on the range of suitable applications for such piping, and defines limitations to the materials of construction for these applications.

It is intended to be used in conjunction with the other parts of ISO 14692.

This part of ISO 14692 also describes the pressure terminology used in ISO 14692 (all parts).

2 Terms and definitions

For the purposes of this document, the following terms and definitions apply.

2.1 General terms

2.1.1

authority having jurisdiction

third-party organization required to be satisfied with the standard of engineering proficiency and safety of a project

EXAMPLE A classification society, verification body or government regulatory body.

2.1.2

contractor

party which carries out all or part of the design, engineering, procurement, construction and commissioning for a project or operation of a facility

NOTE The **principal** (2.1.9) may undertake all or part of the duties of the contractor.

2.1.3

designer

party which carries out all or part of the design for a project or facility

2.1.4

installer

party which carries out all or part of the construction and commissioning of composite pipe installations and installation work for a project

2.1.5

installation inspector

person able to perform satisfactory and independent inspection of composite pipe installations and installation

2.1.6

installation supervisor

tradesman able to perform practical supervision of the installation and joining of composite pipes

2.1.7

manufacturer

party which manufactures or supplies equipment to perform the duties specified by the contractor

2.1.8

operator

party which assumes ultimate responsibility for the operation and maintenance of the piping system

NOTE The operator may or may not be the same as the principal or principal's agent.

2.1.9

principal

party that initiates the project and ultimately pays for its design and construction

The principal generally specifies the technical requirements and is ultimately responsible for ensuring that safety and all other issues are addressed. The principal may also include an agent or consultant, authorized to act for the principal.

2.1.10

site

location where piping system is installed

2.2 Technical terms

2.2.1

accelerator

substance which, when mixed with a catalyst or a resin, will speed up the chemical reaction between catalyst and resin

2.2.2

active fire protection

method of extinguishing fire by application of substances such as halon, water, CO₂, foam, etc.

2.2.3

adhesive joint

adhesive bond

bonded joint

glued joint

socket joint

rigid type of joint between two components made using an adhesive

NOTE Generally consists of a slightly conical (tapered) bell end and a machined (cylindrical or tapered) spigot end.

2.2.4

anisotropic

exhibiting different properties when tested along axes in different directions

2.2.5

carbon fibre

fibre produced by the pyrolysis of organic precursor fibres, such as rayon, polyacrylonitrile or pitch, in an inert environment

2.2.6

cavitation

formation of pockets of vapour in a liquid that suddenly collapse, causing very high localized pressures which can lead to serious erosion of boundary surfaces

2.2.7

chemical-resistant glass

glass fibre or synthetic veil having a specific chemical resistance against acids

NOTE Such glass is used primarily as a reinforcement for the resin-rich internal liner of GRP pipe

2.2.8

collapse pressure

external pressure differential which causes buckling collapse of a component

2.2.9

component variant

individual component

2.2.10

composite

reinforcing fibres laid up in a resin matrix

2.2.11

composite pipe

pipe manufactured using fibre-reinforced thermoset plastics

NOTE Thermoplastic resins are excluded from ISO 14692 (all parts).

2.2.12

chopped strand mat

CSM

reinforcement structure in which short lengths of glass fibre tows, held together by an emulsion or powder binding agent, are dispersed in random directions within a single plane

2.2.13

cure

change irreversibly the properties of a thermosetting resin by chemical reaction

NOTE 1 Examples of such chemical reaction are condensation, ring closure and addition.

NOTE 2 Cure may be accomplished by the addition of a cross-linking agent, with or without heat and pressure.

2.2.14

cure cycle

time/temperature/pressure cycle used to cure a thermosetting resin system

2.2.15

curing agent

catalytic or reactive agent that, when added to a resin, causes polymerization

NOTE Also called hardener, for epoxies.

2.2.16

delamination

separation of two adjacent plies or layers of material in a laminate resulting from lack of adhesion

NOTE May occur either locally or covering a wide area.

2.2.17

design external pressure

maximum positive external pressure differential, i.e. external minus internal pressure, intended to be experienced by a component during its service life

2.2.18

design pressure

maximum positive internal pressure differential, i.e. internal minus external pressure, intended to be experienced by a component during its service life

2.2.19

design temperature

for each design condition, maximum fluid temperature that can be reached during service

2.2.20

differential scanning calorimetry

DSC

method for determining the glass transition temperature of a polymer

2.2.21

dynamic mechanical thermal analysis

DMTA

method for determining the glass transition temperature of a polymer or FRP (2.2.33) component

2.2.22

earth, verb, GB

ground, verb, US

provide electrical contact with earth

2.2.23

E-glass

glass fibre normally used to reinforce GRP (2.2.48) pipes, consisting mainly of SiO₂, Al₂O₃ and MgO

2.2.24

elastomeric bell-and-spigot seal lock joint

rubber seal lock joint

rubber sealed key lock joint

joint connection made up of a spigot end and a socket end with "O" or lip-sealing rings

2.2.25

electrically conductive

conductive

having a volume resistivity equal to or lower than $10^4 \Omega \cdot m$

2.2.26

electrostatic dissipative

conductive

having a volume resistivity higher than $10^4 \Omega$ m but lower than $10^9 \Omega$ m or a surface resistivity less than $10^{10} \Omega$ measured at ambient temperature and 50 % relative humidity

2.2.27

environmental stress cracking

ESC

formation of cracks in a polymer or composite caused by exposure to a chemical or environment under stress

2.2.28

epoxide

epoxy

compound containing at least two epoxy or oxirane rings

NOTE 1 Chemically, an epoxy ring is a three-membered ring containing two carbon atoms and one oxygen atom.

NOTE 2 The most widely used epoxy resin is termed DGEBA (diglycidyl ether of bisphenol A). Epoxy resins are always used in conjunction with curing agents or hardeners, i.e. substances that react with the epoxy rings, producing hydroxyl groups and other products, and linking the originally linear molecules into a rigid three-dimensional network.

2.2.29

factored qualified pressure

pressure to be used in determining the safe operating envelope of the GRP pipe or piping system

NOTE Factored qualified pressure is based on the qualified pressure and takes account of specific service conditions that could not be considered in the qualification programme, e.g. temperatures other than 65 °C and the effect of exposure to chemical environments other than water.

2.2.30

factored stress

hoop stress based on the factored qualified pressure (2.2.29)

2.2.31

failure

loss of structural integrity and/or transmission of fluid through the wall of a component or a joint

2.2.32

fibre

filamentary material with a finite length that is at least 100 times its diameter and prepared by drawing from a molten bath, spinning or deposition on a substrate

NOTE Filaments are usually of extreme length and very small diameter, usually less than 25 µm. Normally, filaments are assembled as twisted (yarn) or untwisted (tow) bundles comprising hundreds of filaments.

2.2.33

fibre-reinforced plastic

FRP

plastic-based composite that is reinforced with any type of fibre, not necessarily glass

2.2.34

filament winding

process for fabricating a composite structure in which continuous reinforcements, e.g. fibre tows, are either previously impregnated with a matrix material or impregnated during the winding

2.2.35

fire classification code

code designation of the fire performance of pipe component in terms of fire endurance and fire reaction properties

2.2.36

fire endurance

fire resistance

ability to maintain functional performance in a fire

2.2.37

fire-reaction property

material property which contributes to spread of fire, heat release and smoke/toxic emissions

2.2.38

fitter

jointer

pipe bonder

tradesman able to perform satisfactory and independent work in the installation and joining of composite pipes

2.2.39

fitting

pressure-tight fluid-containing components with a geometry different from straight pipe.

EXAMPLES Flanges, tees, elbows, reducers and fabricated branch.

2.2.40

flame retardant

chemical that is used to reduce or eliminate the tendency of a resin to burn

2.2.41

flange joint

mechanical joint with face flanges for which the bolt circle and face dimensions conform to a recognized standard

2.2.42

flexibility factor

ratio of the flexibility in bending of a component/fitting to that of the flexibility of a straight pipe of the same lamination, Young's modulus and thickness having a length corresponding to the developed length of the fitting

2.2.43

free-end testing

pressure-testing arrangement using pipe end closures of a type such that internal pressure produces axial, as well as hoop and radial, stresses in the component wall

cf. axial load-free testing (2.2.110)

2.2.44

function

ability of the piping system to perform its primary purpose, i.e. to deliver a minimum quantity of fluid above a minimum pressure

2.2.45

furnace test

test in a compartment furnace where the time-temperature curve to be followed is to a defined standard

2.2.46

gel coat

quick-setting resin applied to the surface of a mould and gelled before lay-up

NOTE The gel coat becomes an integral part of the finished laminate, and is usually used to provide specific service characteristics (see liner, 2.2.69).

2.2.47

glass-fibre-reinforced epoxy

GRE

epoxy resin-based composite that is reinforced with glass fibre

2.2.48

glass-fibre-reinforced plastic

GRP

fibreglass

composite

reinforced plastic

reinforced thermosetting resin plastic

RTR plastic

polymeric resin-based composite that is reinforced with glass fibre

NOTE 1 The predominant glass fibre is **E-glass** (2.2.23).

NOTE 2 ISO 14692 (all parts) is restricted to the use of **thermosetting** (2.2.120) resins.

2.2.49

glass transition temperature

 T_{q}

temperature at which amorphous polymer undergoes a marked change in properties on passing from the rubbery to glassy state

NOTE This observed change in properties is associated with the virtual cessation of local molecular motion in the polymer. Below their glass-transition temperature, amorphous polymers have many of the properties associated with ordinary inorganic glasses, whilst above this temperature the polymers possess rubbery characteristics.

2.2.50

grounding clamp

metal fitting attached to the pipe component to provide an electrical connection to earth

2.2.51

hand lay-up

process for fabricating a composite structure in which discontinuous reinforcements, e.g. woven mats, chopped strand mats, are impregnated with a matrix material and are manually applied on a mandrel

2.2.52

hardener

substance or mixture added to a plastic composition to promote or control the curing action by taking part in it

2.2.53

hazardous area

three-dimensional space in which a flammable atmosphere may be expected to be present frequently enough to require special precautions for the control of potential ignition sources

2.2.54

heat-distortion temperature

temperature at which a standard test bar deflects a specified amount under a stated load

2.2.55

heat flux

density of heat flow rate

quantity of heat divided by area and time

2.2.56

hydrocarbon pool fire

fire caused by ignition of a pool of hydrocarbon liquid

2.2.57

hydrotest

pressure test to verify the pressure-retention integrity of a piping system after installation

cf. mill hydrostatic test (2.2.78)

NOTE Also used as a leak test.

2.2.58

impregnate

saturate the reinforcement with a resin

2.2.59

incendive discharge

electrostatic spark discharge of sufficient energy to ignite a flammable atmosphere

2.2.60

integrity

minimum structural capability required to enable the pipe system to fulfil its function

2.2.61

intumescent

passive fire-protection coating which, in the presence of fire, expands to create an inert "char" layer

2.2.62

jet fire

turbulent diffusion flame resulting from the combustion of a fuel continuously released with significant momentum in a particular range of directions

2.2.63

ioint

means of connecting two or more components

EXAMPLE Plain pipe to a fitting, or plain pipe to plain pipe.

2.2.64

laminae

thin sheets of reinforcing fibres in a resin matrix built up into a flat or curved arrangement

2.2.65

laminate, verb

unite laminae with a bonding material, usually using pressure and heat

Normally used with reference to flat sheets, but can also refer to tubes. A product made by such bonding is NOTE referred to as a laminate.

2.2.66

laminated joint

butt-and-wrap joint

butt-and-strap joint

butt-welded joint

joint consisting of plain-ended pipe and fittings laminated together with reinforcing fibres and resin/hardener mixture

2.2.67

laying length

actual length of a line, corresponding to the initial length plus the increase afforded by the fitting or integral joint when installed

2.2.68

leak test

pressure test to determine the presence of leaks at joints

NOTE Usually carried out at a pressure lower than the hydrotest and for a longer period.

2.2.69

liner

continuous resin-rich coating on the inside surface of a pipe component, used to protect the laminate from chemical attack or to prevent leakage under stress

NOTE The liner may also be used to provide enhanced abrasion and erosion resistance.

2.2.70

long-term hydrostatic pressure

LTHP

extrapolated long-term mean static failure pressure of a component with free ends based on a 20-year lifetime

NOTE LTHP is determined in accordance with ASTM D2992 Procedure B.

2.2.71

long-term hydrostatic strength

LTHS

extrapolated long-term mean failure strength of a plain pipe with free ends based on a 20-year lifetime

NOTE LTHS is determined in accordance with ASTM D2992 Procedure B.

2.2.72

lower confidence limit

LCL

97,5 % confidence limit of the long-term hydrostatic pressure or stress based on a 20-year lifetime

2.2.73

mandrel

core tool around which resin-impregnated reinforcement is wound to form pipes, fittings and structural shell shapes

2.2.74

manufacturer's pressure rating

pressure rating given by manufacturer in product literature

2.2.75

matrix

homogeneous resin or polymer material in which the fibre system is imbedded in a laminar arrangement

2.2.76

mechanical joint

joint between GRP piping components which is not made by bonding

NOTE A mechanical joint typically involves use of proprietary devices.

2.2.77

megohmmeter

high-voltage instrument used for measuring electrical resistance

2.2.78

mill hydrostatic test

short-term hydrotest at the mill, or factory, used as a quality control check which is carried out at a pressure above the design pressure

2.2.79

modulated differential scanning calorimetry

MDSC

type of DSC (2.2.20) which enables reversible reactions to be distinguished from irreversible processes

2.2.80

nominal diameter

numerical designation of size that is common to all components in a piping system, other than components designated by outside diameters or by thread size

NOTE It is a convenient round number for reference purposes and is only loosely related to manufacturing dimensions.

2.2.81

operating pressure

normal or anticipated standard internal pressure difference, i.e. internal minus external pressure, to be experienced by the pipe or piping system which should not exceed the design pressure

2.2.82

ovality

irregularity of the circular section of a component, quantified by the difference in the largest and smallest cross-sectional axes

2.2.83

part factor f_1

ratio of the 97,5 % confidence limit of LTHP to the mean value of LTHP

2.2.84

part factor f_2

derating factor related to confidence in the pipework system, the nature of the application and the consequences of failure

2.2.85

part factor f_3

part factor that takes account of non-pressure-related axial loads, e.g. bending

2.2.86

passive fire protection

method of minimizing fire damage by use of sacrificial or non-combustible coatings

2.2.87

performance standard

defined limit placed on characteristics of materials, products or services

2.2.88

phenolic

class of polymer resins made from phenol and formaldehyde, and cured by air drying or heat baking

NOTE Chemical resistance can be further increased via heat and catalyst treatment.

2.2.89

pipe support

pipe fixture or structural attachment which transfers the load from the pipe or structural attachment to the supporting structure or equipment

NOTE 1 Fixtures include hanging-type fixtures such as hanger rods, spring hangers, sway braces, counterweights, turnbuckles, struts, chains, guides and anchors; and bearing-type fixtures such as saddles, bases, rollers, brackets and sliding supports.

NOTE 2 Structural attachments include elements which are bonded or moulded into the pipe, such as clips, lugs, rings, clamps, clevises, straps and skirts.

2.2.90

piping

assemblies of piping components used to convey, distribute, mix, separate, discharge, meter, control or restrict fluid flows

2.2.91

piping component

component

mechanical element suitable for joining or assembly into a pressure-tight fluid-containing piping system

EXAMPLES Pipe, fittings, flanges, gaskets, bolting, valves, and devices such as expansion joints, flexible joints, pressure hoses, liquid traps, strainers and in-line separators.

2.2.92

piping system

interconnected piping subject to the same set or sets of design conditions

NOTE The piping system also includes pipe supports, but does not include support structures.

2.2.93

pipeline system

pipe with components subject to the same design conditions and typically used to transport fluids between wells and field facilities, field facilities and processing plants, processing plants and storage facilities

2.2.94

Poisson's ratio

ratio of axial strain to the corresponding hoop strain below the proportional limit

2.2.95

proportional limit

greatest stress which a material is capable of sustaining without deviation from linear proportionality of stress and strain

2.2.96

postcure

additional elevated-temperature cure, usually without pressure, to improve final resin properties and/or complete the cure, or decrease the percentage of volatiles in the compound

NOTE In certain resins, complete cure and ultimate mechanical properties are attained only by exposure of the cured resins to temperatures higher than those of curing.

2.2.97

pot life

length of time that a catalysed thermosetting resin system retains a viscosity low enough to enable processing and sufficient reactivity to achieve specified properties after processing

2.2.98

pressure rating

rated pressure

rating for a component, relating to its long-term resistance to failure when subjected to either static or standardized cyclic internal pressure loading

2.2.99

pressure stress multiplier

PSM

fractional increase in hoop stress loading due to applied axial loads acting on a fitting

2.2.100

product family

component type all of whose variants have the same function

EXAMPLES Plain pipe, bend, tee, reducer, etc.

2.2.101

product family representative

component that is taken to be representative of that particular product family (2.2.100)

Examples include plain pipe, pipe plus joint, elbows and reducers, tees, and flanges. Also included are fabrication processes used in the factory or on-site, that are not qualified as part of the process for manufacturing stock items.

2.2.102

product sector

subdivision of a product family (2.2.100) that groups variants into specific diameter and pressure ranges

2.2.103

product sector representative

component variant taken to be representative of that product sector (2.2.102) and upon which the basic qualification testing is performed

2.2.104

qualification

process of demonstrating that a component is in accordance with the requirements of ISO 14692-2

2.2.105

qualified pressure

component pressure rating determined in accordance with qualification requirements given in 2.2.104

2.2.106

qualified stress

hoop stress based on the qualified pressure (2.2.105)

2.2.107

rated temperature

maximum design temperature at the factored pressure determined in accordance with ISO 14692-2 and ISO 14692-3

2.2.108

reducer

component that allows pipes of different sizes to be connected

2.2.109

reinforcement

strong material embedded into a matrix to improve its mechanical properties

Reinforcements are usually long fibres, whiskers, particulates, etc. The term should not be used synonymously with filler.

2.2.110

axial load-free testing

pressure-testing arrangement using a pipe-sealing device or mechanism such that internal pressure produces hoop and radial stresses only in the component wall

2.2.111

roving

number of strands, tows or ends collected into a parallel bundle with little or no twist

2.2.112

saddle

length of an arc of GRP material adhesively bonded to the outside of the pipe

2.2.113

short-term hydrostatic pressure

STHP

short-term burst pressure determined with free ends at SLT (2.2.116)

NOTE STHP is determined in accordance with ASTM D1599.

2.2.114

sizing agent

coating on glass fibres used to promote bonding of glass-reinforcement to resin

2.2.115

spoolpiece

permanent assembly of pipe and fittings fabricated in the factory using laminated or adhesive joints

2.2.116

standard laboratory temperature

SLT

temperature as defined by a recognized standard with standard tolerance

EXAMPLE 23 °C \pm 2 °C.

2.2.117

stress intensification factor

SIF

ratio of the actual/effective stress in a component/fitting under external load to the nominal stress in that component/fitting as determined based on a straight pipe run with the same section modulus and Young's modulus

2.2.118

system

assembled section of piping consisting of a representative range of pipes, fittings, connections, attachments, supports, penetrations and associated coatings, e.g. for thermal insulation or fire protection, as would be found in service

2.2.119

thermoset

plastic which, when cured by application of heat and/or chemical reaction, changes into a substantially infusible and insoluble material

2.2.120

thermosetting polyester

thermosetting class of resin produced by dissolving unsaturated, generally linear, alkyd resins in a vinyl-type active monomer such as styrene, methylstyrene or diallyl phthalate

NOTE Cure is effected through vinyl polymerization using peroxide catalysts and promoters or heat to accelerate the reaction.

2.2.121

tow

untwisted fibrous bundle

2.2.122

tow tex

mass of a fibrous bundle expressed per unit length

2.2.123

tribocharging

generation of electrostatic charge caused by moving contact of one insulating material over another

2.2.124

type

components of common function

NOTE Pipes, prime connections, flanges, reducers, tees and elbows are examples of different component types.

2.2.125

type testing

exposure of a system to a fire insult to qualify the assembled system components for a defined range of service conditions

2.2.126

ultraviolet radiation

UV

electromagnetic radiation in the frequency band just above the visible spectrum

2.2.127

variant

component with a unique combination of nominal diameter, type and pressure rating

2.2.128

vinyl ester

class of thermosetting resin containing esters of acrylic and/or methacrylic acids, many of which have been made from epoxy resin

NOTE Cure is accomplished, as with unsaturated polyesters, by copolymerization with other vinyl monomers such as styrene.

2.2.129

water hammer

shock load or high-pressure surge caused by sudden halting of flow in a pipe

3.2.130

winding angle

angle of main reinforcement to pipe axial axis

NOTE The angle can be either positive or negative.

2.2.131

woven roving

cloth reinforcement structure in which fibre bundle tows are woven together in a single plane to provide reinforcement which is usually orientated to provide strength in the orthogonal 0° and 90° directions

Symbols and abbreviated terms

Symbols 3.1

- partial factor for temperature A_1
- partial factor for chemical resistance A_2
- A_3 partial factor for cyclic service
- coefficient of thermal expansion in the axial direction α_{a}
- coefficient of thermal expansion in the hoop direction $lpha_{\mathsf{h}}$

 b_1 width of the saddle support Ccapacitance D mean diameter of the reinforced wall of the component internal diameter of the reinforced wall of the component D_{i} average optical density D_{m} nominal wall diameter D_{n} d_{ID} internal diameter of component outside diameter of component d_{OD} effective design temperature change to be used for stress analysis $\Delta T_{\rm eff}$ temperature difference between ambient temperature and the process design temperature ΔT_{pa} axial pressure correction factor δ_{a} hoop pressure correction factor δ_{h} axial modulus $E_{\mathbf{a}}$ axial modulus of pipe $E_{\mathsf{a},\mathsf{pipe}}$ axial modulus of bend $E_{\mathsf{a},\mathsf{bend}}$ hoop modulus E_{h} $E_{
m h,bend}$ hoop modulus of bend strain ε $F_{\mathsf{a},\mathsf{max}}$ maximum axial compressive load F_{e} safety factor for external loading maximum load (or stress) of the load (or stress) cycle F_{max} minimum load (or stress) of the load (or stress) cycle F_{min} scale factor of ratio short-term to long-term failure envelope f_{scale} part factor that provides a measure of the degree of scatter in the long-term pressure tests f_1 part factor for loading (safety factor) f_2 f_3 part factor to take account of limited axial load capability of GRP pipe value of f_3 assigned by manufacturer for quotation purposes $f_{3,man}$

G	slope of static regression curve
$G_{default}$	default slope of static regression curve
G_{shear}	shear modulus
γ	shear strain
I_{b}	second moment of area about an axis through the centroid normal to the bend axis
I_{p}	second moment of area about an axis through the centroid normal to the pipe axis
I_{t}	second moment of area about an axis through the centroid normal to the tee axis
K_{S}	support type factor
k	factor to take account of the low thermal conductivity of GRP
κ_{b}	flexibility factor for GRP bends
κ_{t}	flexibility factor for GRP tees
L	length of pipe
$L_{\sf max}$	maximum overall length of fittings (bends, tees and reducers)
L_{S}	support span
λ_{b}	pipe factor for bends
M	bending moment
M_{i}	applied in-plane bending moment
M_{O}	applied out-of-plane bending moment
M_{T}	applied torsional moment
m_{psb}	pressure stress multiplier for bends
m_{pst}	pressure stress multiplier for tees
N	total number of cycles during service life
p	applied pressure
p_{C}	external collapse pressure
p_{d}	design pressure
$p_{d,max}$	maximum design pressure
p_{LCL}	lower confidence limit

 p_{LTHP} long-term hydrostatic pressure

 p_{LTHS} long-term hydrostatic strength

 p_{NPR} manufacturer's nominal pressure rating

 p_{q} qualified pressure

 $p_{
m qf}$ factored qualified pressure

 p_{STHP} short-term hydrostatic pressure

 π pi = 3,141 59 (only to six significant figures)

 θ total saddle angle

 $Q_{\rm CFE}$ critical flux at extinguishment

 Q_{sb} heat for sustained burning

Qt total heat release

 $q_{\rm p}$ peak heat release

 R_{b} mean pipe bend radius

 $R_{\rm c}$ design cyclic severity of the piping system

 $R_{\rm i}$ inside radius

 R_{o} outside radius

r short-term biaxial strength ratio at 0:1 and 2:1 stress ratios

 $ho_{
m C}$ density of GRP

 $ho_{
m L}$ density of fluid within the pipe

 S_{f} stress intensification factor (SIF)

 $S_{\rm ft}$ stress intensification factor for tees

 $S_{\mathrm{fa,ib}}$ axial SIF under in-plane bending

 $S_{fa,ob}$ axial SIF under out-of-plane bending

 $S_{\text{fh.ib}}$ hoop SIF under in-plane bending

 $S_{\text{fh,ob}}$ hoop SIF under out-of-plane bending

 $\sigma_{\rm a}$ axial stress

 $\sigma_{\rm al(0:1)}$ idealized long-term axial (longitudinal) strength at 0:1 stress ratio

$\sigma_{\!ab}$	non-pressure-induced axial stress
$\sigma_{\!a,bp}$	axial stress due to internal pressure and bending due to self-weight
$\sigma_{\rm aeff,b}$	effective axial stress in bends
$\sigma_{ m aeff,t}$	effective axial stress in tees
$\sigma_{\!ap}$	axial stress due to internal pressure
$\sigma_{\!a,sum}$	sum of all axial stresses
$\sigma_{\!fs}$	factored stress
$\sigma_{\!h}$	hoop stress
$\sigma_{ m heff,b}$	effective hoop stress in bends
$\sigma_{ m heff,t}$	effective hoop stress in tees
σ_{hb}	hoop stress due to bending
σ_{hp}	hoop stress due to internal pressure
$\sigma_{ m h,sum}$	sum of all hoop stresses (pressure plus system design)
$\sigma_{\!$	qualified stress
$\sigma_{\rm sa(0:1)}$	short-term axial strength at 0:1 stress ratio
$\sigma_{\rm sa(1:1)}$	short-term axial strength at 1:1 stress ratio
$\sigma_{ m sh(1:1)}$	short-term hoop strength at 1:1 stress ratio
$\sigma_{\rm sa(2:1)}$	short-term axial strength at 2:1 stress ratio
$\sigma_{ m sh(2:1)}$	short-term hoop strength at 2:1 stress ratio
$\sigma_{\!\scriptscriptstyle \sf U}$	axial elastic buckling stress, for a cylinder in pure bending
t	time
T_{g}	glass transition temperature
T_{TD}	ratio of the test pressure divided by the design pressure
T _{P1 000}	test pressure to be used in 1 000-hour survival test
t	nominal wall thickness
t_{b}	reinforced wall thickness of the reference laminate of the bend

average wall thickness of the branch laminate of the tee t_{br} wall thickness of the reference laminate of the bend t_{d} minimum wall thickness t_{min} reinforced wall thickness of the reference laminate of the pipe t_{pipe} average reinforced wall thickness of the component t_{r} average wall thickness of the reinforced laminate of the tee t_{t} shear stress maximum shear stress au_{\max} Poisson's ratio, axial to hoop strain resulting from a stress in the hoop direction v_{ha} Poisson's ratio, hoop to axial strain resulting from a stress in the axial direction v_{ah} Velectric potential Welectrical energy of a charged surface pipe and fluid dead mass per length of pipe w_{o} torsional stress ξ Z factor to enable P_{LCL} to be derived from P_{STHP} such that $P_{LCL} = P_{STHP} / Z$

3.2 Subscripts

b bend

fr family representative

cv component variant

psr product sector representative

t tee

3.3 Abbreviated terms

ANSI American National Standards Institute

API American Petroleum Institute

ASME American Society of Mechanical Engineers

ASTM American Society of Testing and Materials

BSI British Standards Institution

DIN Deutsches Institut für Normung

HSE Health and Safety Executive (UK)

IMO International Maritime Organization

NDE non-destructive examination

NDT non-destructive testing

PTFE polytetrafluoroethylene

SLT standard laboratory temperature

Principle

ISO 14692 (all parts) advocates the use of a standard methodology for materials selection that is based on performance and not specification, called "performance-based material selection" (PBMS). PBMS reflects true functional needs, excludes arbitrary requirements and does not specify materials. The four key steps to PBMS

- identification and documentation of all performance factors relevant to the application; a)
- quantification of functional performance requirements; b)
- qualification of materials for technical acceptability; C)
- final selection.

The above methodology provides a standardized auditable approach to material selection.

Applications

Principal applications

ISO 14692 (all parts) applies to GRP piping installations associated with oil and gas industry processing and utility service applications. It is primarily intended for offshore applications on both fixed and floating topsides facilities, but it may also be used as guidance for the specification, manufacture, testing and installation of GRP piping systems in other similarly high-criticality applications found onshore.

Typical current and potential applications for the use of GRP piping are given in Table 1.

Applications to hydrocarbon service, including crude oil or condensate, diesel oil, solvent-based chemicals or hazardous drain systems, may also be considered subject to satisfactory results of a risk analysis. This risk analysis shall be designed to identify any risk inherent in the selection of GRP piping materials and to compare this risk with a metallic piping system operating under the same conditions. GRP may be selected where no significant potential of failure is identified or where the consequences of failure are determined to be of low significance.

High-pressure hydrocarbon applications require more rigorous consideration of fire engineering and fire performance requirements.

In the case of piping which is fully embedded within concrete, such as ballast piping in a concrete gravity-base structure, where the piping forms an impervious form within the concrete, alternative standards may be acceptable. However, it is recommended that specific attention be paid to loads that may be applied to the piping during construction and installation of the structure, including at penetrations and changes in section.

For floating installations, reference should be made to the design, construction and certification standards for the hull or vessel, since these may allow alternative codes and standards for GRP piping associated with marine and/or ballast systems. However, it is recommended that ISO 14692 (all parts) be used for such applications to the maximum degree attainable, and that attention be paid to specific design details, taking into account factors such as hull motions, differential displacements and bulkhead penetrations.

Whilst ISO 14692 (all parts) may be used as the general basis for specification of pipe used for pump caissons, stilling tubes, I-tubes, seawater lift risers and other similar items, it should be noted that such applications normally require consideration of combined internal pressure and structural loadings. These items should therefore be individually designed to accommodate all loading conditions.

Table 1 —Typical current and potential GRP piping applications

Alkyl chloride	Jet-A fuel
Ballast water	Mogas
Boiler feed water	Oil
Brine	Oil plus associated gas
Condensate (water and gas)	Potable water
Cooling water	Process water
CO ₂	Produced water
Drains (non-hazardous)	Seawater
Emulsions (oil/water)	Service water
Inert gas	Sewer (grey water)
Injection water	Sewer (red water)
Fire water (ring main and wet or dry deluge)	Shallow gas
Formation water	Sodium hypochlorite
Fuel	Sodium hydroxide
Fresh water	Unstabilized oil
Gas (methane, etc.)	Vents
Glycol	Wastewater
HCI	Ballast piping systems
Hydrogen chloride gas	Pump caissons, stilling tubes, or seawater lift pump risers

5.2 Other applications

The broad range of other systems to which ISO 14692 (all parts) is applicable includes:

- onshore pipeline and piping systems transporting both oil and associated gas;
- pipeline and piping systems for chemicals.

NOTE ISO 14692 (all parts) is not specifically intended to be utilized for buried pipelines (onshore or offshore). However, much of the content may be adapted in the specification of qualification, manufacturing and installation requirements for pipeline applications.

Materials

Application of ISO 14692 (all parts) shall be limited to the manufacture of rigid components made from fibrereinforced thermosetting resins. Typical resins are epoxy, polyester, vinyl ester and phenolic. Thermoplastic resins are excluded.

The principal reinforcement material of the component wall shall be glass fibre, e.g. continuous and woven rovings. Application of ISO 14692 (all parts) to pipes manufactured with other reinforcement fibres shall be done with caution and in agreement with the principal (2.1.9). See Note 1.

ISO 14692 (all parts) is not applicable to pipe systems that incorporate internal thermoplastic or elastomeric liners. This is because such materials may introduce significant changes in performance characteristics of the GRP piping. See Notes 2 and 4.

The maximum allowable temperature is determined by the resin type and state of cure. Suggested maximum allowable temperatures, based on experience with typical GRP pipe systems, are given in Table 2 as a function of resin type. The temperatures listed in Table 2 are for initial guidance only.

Resin type	Maximum temperature	
Ероху	110 °C	
Vinyl ester	100 °C	
Polyester	70 °C	
Phenolic	150 °C	

Table 2 —Temperature limitations

The maximum allowable operating temperature for a GRP pipeline or piping system may, however, be considerably lower, depending on the aggressiveness of the specific fluid and its concentration, and on the specific curing agent.

The minimum recommended temperature for GRP regardless of the resin system is -35 °C, although lower temperatures may be considered.

The resins as listed are generic compounds. Their performance and properties of thermal, mechanical and chemical resistance vary significantly depending on the resin and curing agent used to cure them. The user is cautioned to ascertain that the resin and curing agent are known for the resin system planned to be used and that these have all the properties that ISO 14692 (all parts) requires for the resin system.

Thermoplastic resins are excluded because of the lack of experience in piping applications covered by this NOTE 2 part of ISO 14692.

Glass fibre is the preferred reinforcement material because there is little information available about the longterm pressure retention, impact and fire performance of pipes manufactured from other reinforcement materials such as carbon or aramid fibre.

NOTE 4 The use of a thermoplastic liner will result in change of the failure mode for pressure retention. Such liners also have an influence on the fire endurance and electrostatic properties of the pipe.

Dimensions

For guidance purposes, the typical pressure-diameter range of pipes covered by ISO 14692 (all parts) is indicated by Figure 1, which represents a compromise between the current application experience envelope of GRP pipelines and piping systems and commercial availability.

The structural calculations given in ISO 14692 (all parts) are only valid for thickness-to-diameter ratios that are in accordance with Equation (1).

$$\left(\frac{t_{\rm r}}{D}\right) \leqslant 0.1\tag{1}$$

where

- t_r is the reinforced thickness of the wall, in millimetres, i.e. excluding liner and added thickness for fire protection;
- *D* is the mean diameter, in millimetres, of the structural portion of the wall.

ISO 14692 (all parts) covers all the main components that form part of a GRP pipeline and piping system (pipe, bends, reducers, tees, supports, flanged joints) with the exception of valves and instrumentation.

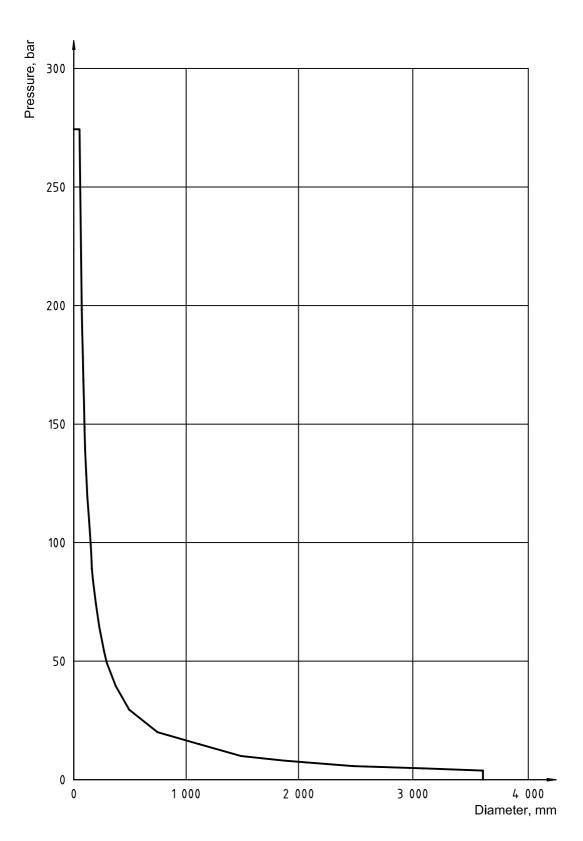


Figure 1 — Envelope of pressure/diameter range of GRP pipes and piping systems based on current experience

8 Pressure terminology

The pressure terminology used in this part of ISO 14692 is dependent on the context in which it is used. The term pressure rating, as quoted by the supplier, is avoided to prevent confusion as to whether it refers to a manufacturer's catalogue value, design pressure or operating pressure.

In ISO 14692-2, manufacturers assign all components a *qualified pressure*, $p_{\rm q}$ expressed in megapascals (MPa) (with equivalent provided in bars) which corresponds to a 20-year minimum long-term performance of the pipe subject to unrestrained ends, i.e. 2:1 pressure loading in the hoop and axial directions. The default design temperature is 65 °C. Factoring and interpolation of data to other temperatures is permitted depending on the availability of suitable test data. The qualified pressure is not the same as the *manufacturer's nominal pressure rating*, $p_{\rm NPR}$, which includes a derating factor chosen by the manufacturer based on experience. Use of the manufacturer's rating shall only be for guidance purposes.

The maximum design pressure $p_{d,max}$ for the GRP pipe and joint/fitting is given by equation (2):

$$p_{d,\text{max}} = f_2 \cdot f_3 \cdot p_{q} \tag{2}$$

where

- $p_{\rm q}$ is the qualified pressure, in megapascals;
- f_2 is related to confidence in the pipework system, the nature of the application and the consequences of failure. The default partial factor used for the evaluation of operational sustained loads, excluding thermal effects, is 0,67;
- f_3 is not a fixed parameter and is used to take account of the limited axial load capability of GRP. The maximum allowable value of f_3 is 1,0 (which would normally only be applicable to a below-ground application).

The qualified pressure is factored to give the *factored qualified pressure*, p_{qf} , which takes account of the performance at temperatures other than 65 °C and the effect of exposure to chemical environments other than water.

In ISO 14692-3, the system design pressure p_d for a component is given by Equation (3):

$$p_{\mathsf{d}} \leqslant f_2 \cdot f_3 \cdot p_{\mathsf{af}} \tag{3}$$

The system design pressure, $p_{\rm d}$, is limited by the component with the smallest value of f_3 . Since the value of f_3 is dependent on the magnitude of axial stress, the component with the smallest f_3 cannot be determined until after the system stress analysis has been completed. If the stresses exceed the failure envelope, the designer is obliged to either redesign the system in order to reduce the stresses or else select pipe components with a higher value of qualified pressure.

The factored qualified pressure is used to determine the qualified stress, σ_{qs} . The qualified stress for plain pipe is the maximum hoop stress at which the system is designed to operate under sustained conditions. The qualified stress is used with other information provided by the manufacturer to produce a design failure envelope. It is the responsibility of the system designer to ensure that the system stresses do not fall outside the factored long-term design envelope, as described in 7.11 of ISO 14692-3:2002.

In ISO 14692-4, the installer requires knowledge of the system design pressure and the qualified pressure in order to construct and commission the piping system. The operator also requires knowledge of the qualified pressure in order to carry out repairs and modifications.

The *operating pressure* is the pressure at which a system is operated, which should not exceed the design pressure.

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