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ISO 12485

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Tower cranes — Stability requirements

Grues à tour - Exigences relatives à la stabilité

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International Organization for Standardization
Case postale 56 • CH-1211 Genève 20 • Switzerland
Internet iso@iso.ch

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Tower cranes — Stability requirements

1 Scope

This International Standard specifies the conditions to be met when verifying, by calculation, the stability of a tower crane, as defined in ISO 4306-3, that is subject to tipping and drifting; it assumes that the crane is standing on a firm, level supporting surface or track.

2 Normative references

The following standards contain provisions which, through reference in this text, constitute provisions of this International Standard. At the time of the publication, the editions indicated were valid. All standards are subject to revision, and parties to agreements based on this International Standard are encouraged to investigate the possibility of applying the most recent editions of the standards indicated below. Members of IEC and ISO maintain registers of currently valid International Standards.

ISO 4302:1981, Cranes — Wind load assessment.

ISO 4306-3:1991, Cranes — Vocabulary — Part 3: Tower cranes.

ISO 8686-3:—1), Cranes — Design principles for loads and load combinations — Part 3: Tower cranes.

3 Definitions

For the purposes of this International Standard, the definitions given in ISO 4306-3 apply.

4 Stability

4.1 Calculations

- **4.1.1** A crane is said to be stable when the algebraic sum of the stabilizing moments is greater than or equal to the sum of the overturning moments.
- **4.1.2** Calculations shall be made to verify the stability of the crane by computing the sum of the overturning moments using the values given in table 1.

¹⁾ To be published.

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In all calculations, the position of the crane and its components, and the effect of all loads and forces, shall be considered in their least favourable combination, direction and effect.

4.1.3 For cranes designed to travel with load, the forces induced by the maximum allowable vertical track variation as specified by the manufacturer shall be taken into account, in addition to other loads specified in condition II of table 1.

Table 1 — Crane stability — Load factors

	Condition	Loading	Load factor to be considered
		Loads induced by the dead weight	1,0
	I. Basic stability	Applied load	1,6 <i>P</i>
		Wind load	0
IN		Inertia forces	0
		Loads induced by the dead weight	1,0
	II. Dynamic stability	Applied load	1,35 P
SERVICE		Wind load	1,0 W ₁
		Inertia forces	1,0 D
		Loads induced by the dead weight	1,0
	III. Backward stability	Applied load	-0,2 P
	(sudden release of load)	Wind load	1,0 W ₁
		Inertia forces	0
		Loads induced by the dead weight	1,0
ОИТ	IV. Extreme wind loading	Applied load	1,0 P ₁
		Wind load	1,2 W ₂
OF		Inertia forces	0
		Loads induced by the dead weight	1,0
SERVICE	V. Stability during erection	Applied load	1,25 P ₂
	or dismantling	Wind load	1,0 W ₃
		Inertia forces	1,0 D

where

- D are the inertia forces from drives in accordance with ISO 8686-3; $\Phi_5 = 1$
- P is the net load;
- P₁ is the mass of the fixed load lifting attachment;
- P_2 is the mass of the part being installed/removed during erection or dismantling;
- W_1 is the in-service wind effect in accordance with ISO 4302;
- W_2 is the out-of-service wind effect in accordance with ISO 4302 (gusting effects are included);
- W_3 is the in-service wind effect W_1 or the effect of the wind limit for erection work in accordance with the instruction handbook of the manufacturer.

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- **4.1.4** Where required, excitation effects appropriate to the particular site or zone shall be considered as an additional loading condition.
- **4.1.5** In the calculations shown in table 1, consideration shall be given to the loads induced by the mass of the crane and its components, including any lifting attachments which are a permanent part of the crane in its working condition.

4.2 Backward stability in service conditions

Backward stability is covered by condition III.

4.3 Application of wind loads

- 4.3.1 In-service wind forces shall always be applied in the least favourable direction.
- **4.3.2** Out-of-service wind forces shall be applied in the least favourable direction for those cranes which are not free to rotate with the wind. For those cranes which are designed to rotate with the wind, the force shall be applied on the superstructure in the direction contemplated, and in the least favourable direction on the lower structure.

5 Crane base

The crane manufacturer shall specify the forces imposed by the crane on the ground or supporting structure. The information given by the manufacturer should state all applicable conditions for which the forces have been stipulated (including out-of-service wind). Where the crane base provides all or part of the stability of the crane, the manufacturer shall specify the requirement applicable to the crane base.

Where the crane is required to operate on an inclined surface, the manufacturer shall take the specified conditions into account.

6 Temporary additional stability devices

Tower cranes shall be stable in their operating configuration (conditions I to IV in table 1) without use of temporary additional devices.

Temporary additional devices may be used to satisfy condition V in table 1, erection or dismantling.

Detachable ballast may be used to satisfy the case of condition IV in table 1. However, this condition shall be met without this extra ballast, using a factor of 1,1 W_2 .

7 Deformation

Where it can be shown, under the least favourable conditions of loading on the most destabilizing configuration, that the increase in tower moment from considering effects of deflections (second-order theory) is no more than 10 %, then stability calculations may be carried out ignoring deflections (first-order theory) for ease of calculation.

However, when this is done, the overturning moments for each condition in table 1 shall be increased in proportion to the increase from second-order effects found above.

8 Resistance to drifting caused by wind

The resistance to drifting caused by wind shall be proven by calculation for all tower cranes on rails operating in the open air under the conditions in table 2.

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Table 2 — Drifting caused by wind

Condition	Loading	Load factor to be considered
	Loads induced by the dead weight	1,0
II. Dynamic stability	Applied load	1,35 <i>P</i>
	Wind load	1,2 W ₁
	Inertia forces	1,0 D
	Loads induced by the dead weight	1,0
IV. Extreme wind loading	Applied load	1,0 P ₁
	Wind load	1,2 W ₂
	Inertia forces	0

Where rail clamps or similar measures are necessary to avoid out-of-service drifting, the operator's manual shall advise that they have to be applied, when the in-service wind limit has been reached.

The resistance to travel due to friction and the coefficients of friction shown in table 3 shall apply.

Table 3 — Resistance to travel and coefficients of friction

Ratio	:		
Resistance to travel			
F	Radiai load	Coefficient of friction between track and	
Plain bearings	Antifriction bearings	the braked wheel	the rail clamp a)
0,02	0,005	0,14	0,25

a) Higher coefficients of friction may be allowed for if it can be shown that these are present at all surface conditions and qualities (e.g. oil, dirt, ice).

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