
**Round steel short link chains for general
lifting purposes — Medium tolerance
sling chains for chain slings — Grade 8**

*Chaînes de levage général en acier, de section ronde, à maillons
courts — Chaînes de tolérance moyenne pour élingues — Classe 8*





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Foreword

ISO (the International Organization for Standardization) is a worldwide federation of national standards bodies (ISO member bodies). The work of preparing International Standards is normally carried out through ISO technical committees. Each member body interested in a subject for which a technical committee has been established has the right to be represented on that committee. International organizations, governmental and non-governmental, in liaison with ISO, also take part in the work. ISO collaborates closely with the International Electrotechnical Commission (IEC) on all matters of electrotechnical standardization.

International Standards are drafted in accordance with the rules given in the ISO/IEC Directives, Part 2.

The main task of technical committees is to prepare International Standards. Draft International Standards adopted by the technical committees are circulated to the member bodies for voting. Publication as an International Standard requires approval by at least 75 % of the member bodies casting a vote.

Attention is drawn to the possibility that some of the elements of this document may be the subject of patent rights. ISO shall not be held responsible for identifying any or all such patent rights.

ISO 3076 was prepared by Technical Committee ISO/TC 111, *Round steel link chains, chain slings, components and accessories*, Subcommittee SC 1, *Chains and chain slings*.

This third edition cancels and replaces the second edition (ISO 3076:1984), which has been technically revised.

Round steel short link chains for general lifting purposes — Medium tolerance sling chains for chain slings — Grade 8

1 Scope

This International Standard specifies the requirements for medium tolerance sling chains of grade 8 for use in chain slings and for general lifting purposes.

They are round steel short link chains ($3 d_n$), electrically welded, heat treated and tested; they comply with the general conditions of acceptance of ISO 1834.

NOTE 1 Butt welding and flash butt welding are listed in ISO 4063.

The range of nominal sizes covered by this International Standard is from 4 mm to 45 mm. They are for use in the temperature range -40 °C to $+400\text{ °C}$.

NOTE 2 Concerning the use and maintenance of chain slings of grade 8, see ISO 3056.

2 Normative references

The following referenced documents are indispensable for the application of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

ISO 148-1, *Metallic materials — Charpy pendulum impact test — Part 1: Test method*

ISO 643, *Steels — Micrographic determination of the apparent grain size*

ISO 1035-1, *Hot-rolled steel bars — Part 1: Dimensions of round bars*

ISO 1834, *Short link chain for lifting purposes — General conditions of acceptance*

ISO 7500-1, *Metallic materials — Verification of static uniaxial testing machines — Part 1: Tension/compression testing machines — Verification and calibration of the force-measuring system*

ISO 14556, *Steel — Charpy V-notch pendulum impact test — Instrumented test method*

ISO 16124, *Steel wire rod — Dimensions and tolerances*

3 Terms and definitions

For the purposes of this document, the terms and definitions given in ISO 1834 apply.

4 General conditions of acceptance

The sling chains shall comply with the requirements of ISO 1834 as well as those of this International Standard.

5 Dimensions

5.1 Nominal size, d_n

The nominal size, d_n , of the sling chain shall be one of the nominal sizes listed in Table 1, column 1, corresponding to the nominal diameter of the steel wire in accordance with ISO 16124 or bar in accordance with ISO 1035-1 from which the sling chain is made.

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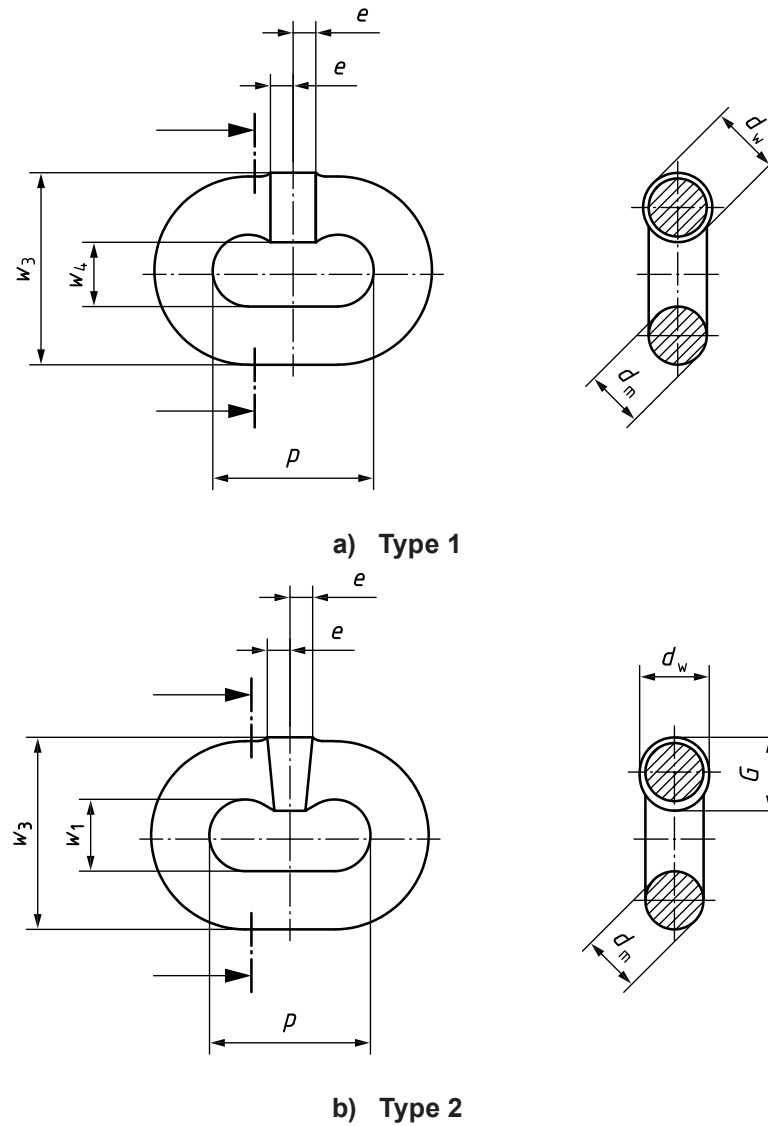
Other nominal sizes may be used, provided the dimensions and tolerances are calculated in accordance with Annex A.

NOTE Intermediate nominal chain sizes increase the potential of mismatch with mating components. Manufacturers of sling chain and component assemblies are expected to ensure that the sling chain and components are compatible.

Table 1 — Dimensions

Dimensions in millimetres

1	2	3	4	5	6	7	8	9
Nominal size d_n	Diameter tolerance	Pitch		Internal Type 2 w_1 min.	Width		Weld diameter	
		p_n	Tolerance		External Types 1 and 2 w_3 max.	Internal Type 1 w_4 min.	Types 1 and 2 d_w max.	Type 2 G max.
4	+0,08/-0,24	12	±0,4	5,0	14,8	5,2	4,4	5,0
6	+0,12/-0,36	18	±0,5	7,5	22,2	7,8	6,6	7,5
7	+0,14/-0,42	21	±0,6	8,8	25,9	9,1	7,7	8,8
8	+0,16/-0,48	24	±0,7	10,0	29,6	10,4	8,8	10,0
10	+0,20/-0,60	30	±0,9	12,5	37,0	13,0	11,0	12,5
13	+0,26/-0,78	39	±1,2	16,3	48,1	16,9	14,3	16,3
16	+0,32/-0,96	48	±1,4	20,0	59,2	20,8	17,6	20,0
18	±0,9	54	±1,6	22,5	66,6	23,4	19,8	22,5
19	±0,95	57	±1,7	23,8	70,3	24,7	20,9	23,8
20	±1,0	60	±1,8	25,0	74,0	26,0	22,0	25,0
22	±1,1	66	±2,0	27,5	81,4	28,6	24,2	27,5
26	±1,3	78	±2,3	32,5	96,2	33,8	28,6	32,5
28	±1,4	84	±2,5	35,0	104,0	36,4	30,8	35,0
32	±1,6	96	±2,9	40,0	118,0	41,6	35,2	40,0
36	±1,8	108	±3,2	45,0	133,0	46,8	39,6	45,0
40	±2,0	120	±3,6	50,0	148,0	52,0	44,0	50,0
45	±2,25	135	±4,1	56,3	167,0	58,5	49,5	56,3



Key

- p pitch (internal link length)
- d_m measured diameter of the material, except at the weld
- d_w measured diameter of the material at the weld (type 1) or weld dimension perpendicular to the plane of the link (type 2)
- G dimension in other planes (type 2)
- e length affected by welding, on either side of the centre of the link
- w_1 internal link width away from the weld (type 2)
- w_3 external link width over the weld (types 1 and 2)
- w_4 internal link width at the weld (type 1)

Figure 1 — Chain link

5.2 Material diameter and tolerance

The definition of material diameter and method of measurement shall be in accordance with ISO 1834. The diameter tolerance for the nominal sizes shall be as listed in Table 1, column 2, calculated in accordance with Annex A.

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5.3 Weld diameter

The maximum diameter at the weld (see Figure 1 and Table 1, columns 8 and 9) shall not exceed the following:

- type 1: the maximum diameter at the weld shall not be in excess of 10 % above the nominal size in any direction;
- type 2: the maximum diameter at the weld shall not be in excess of 10 % above the nominal size in any direction perpendicular to the plane of the link and 25 % in the other planes.

NOTE Type 1 eliminates functional problems, such as kinking or locking, by severely limiting the weld oversize to 10 % of the nominal diameter. Type 2 ensures freedom from these hazards by limiting the oversize beyond the 10 % allowed under type 1 to certain areas of the link only (see Figure 1), thus providing clearance where required.

5.4 Length dimensionally affected by welding

The length dimensionally affected by welding, e , shall not extend by more than $0,6 d_n$ to either side of the centre of the link (see Figure 1).

5.5 Pitch

The dimensions and tolerances for the pitch, p , shall be as given in Table 1, columns 3 and 4 and as shown in Figure 1 calculated in accordance with Annex A.

5.6 Width

The dimensions for the widths, w , shall be as given in Table 1, columns 5, 6 and 7 and as shown in Figure 1 calculated in accordance with Annex A.

6 Material and manufacture

6.1 Quality of material

Within the limitations given in 6.1.1 to 6.1.4, it is the responsibility of the manufacturer of the sling chain to select the type of steel to be used so that the finished sling chain, where suitably heat treated, complies with the mechanical properties specified in this International Standard and also possesses adequate low-temperature ductility and toughness to provide resistance against impact loading.

The low-temperature ductility and toughness shall be achieved either by complying with the alloying elements specified in 6.1.5 or by complying with the toughness-testing requirements specified in 6.4.5.

6.1.1 Type of steel

The steel used shall be produced by the electric process or by an oxygen-blown process.

6.1.2 Deoxidation

The steel shall be fully killed and shall be made in conformity with a suitable deoxidation process in order to obtain an austenitic grain size of 6 or finer where tested in accordance with ISO 643.

To ensure the sling chain is stabilized against strain-age embrittlement during service, the steel shall contain at least 0,025 % aluminium, but not more than 0,050 % aluminium.

6.1.3 Weldability

The steel shall be of reliable weldable quality.

6.1.4 Sulfur and phosphorus content

The content of sulfur and phosphorus shall be restricted as specified in Table 2.

Table 2 — Sulfur and phosphorus content

Element	Maximum mass content as determined by	
	cast analysis	check analysis
	%	%
Sulfur	0,020	0,025
Phosphorus	0,020	0,025
Sum of sulfur and phosphorus	0,035	0,045

6.1.5 Alloying elements

The steel shall contain alloying elements in sufficient quantities so that the finished sling chain, where heat treated in accordance with 6.2, complies with the mechanical properties specified in this International Standard but also possesses adequate low-temperature ductility and toughness to provided resistance to impact loading.

The steel shall contain nickel and at least one of the other elements in the minimum percentage shown in Table 3.

Table 3 — Content of alloying elements

Element	Minimum mass content as determined by
	cast analysis
	%
Nickel	0,40
Chromium	0,40
Molybdenum	0,15

6.1.6 Finished condition

In its finished condition, as supplied to the manufacturer of the sling chain, the steel shall comply with the requirements of 6.1.1 to 6.1.4 and 6.1.5, where appropriate, as determined by check analysis on the rod, wire or finished link.

6.2 Heat treatment

Sling chains shall be hardened from a temperature above the A_{c3} point and tempered before being subjected to the manufacturing proof force (MPF), F_{MP} . The tempering temperature shall be at least + 400 °C.

The tempering conditions shall be at least as effective as the temperature of + 400 °C maintained for a period of 1 h. This requirement is the responsibility of the chain manufacturer. Where proposed for verification, samples of sling chains shall be tested after they have been re-heated to, and maintained for 1 h, at + 400 °C and then cooled to room temperature. These samples shall comply with the requirements of Table 5.

For sling chains with a surface finish other than natural black, samples required for verification shall be taken and re-heat treated prior to the surface finishing process.

6.3 Working load limits (WLLs)

Table 4 gives values for the working load limits (WLLs), calculated on the bases given in Annex A for the appropriate nominal size.

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6.4 Mechanical properties

6.4.1 Manufacturing proof force (MPF)

All sling chains shall be subjected to the manufacturing proof force, F_{MP} , specified in Table 4, column 3, calculated on the bases given in Annex A for the appropriate nominal size.

For other nominal sizes, the mechanical properties shall be calculated in accordance with Annex A.

Table 4 — Working load limits and test requirements

1	2	3	4	5
Nominal size d_n	Working load limit (WLL) t	Manufacturing proof force (MPF) F_{MP} kN min.	Breaking force (BF) F_B kN min.	Bend deflection f mm min.
4	0,5	13	20	3,2
6	1,12	28	45	4,8
7	1,5	38	62	5,6
8	2	50	80	6,4
10	3,15	79	130	8
13	5,3	130	210	10
16	8	200	320	13
18	10	250	410	14
19	11,5	280	450	15
20	12,5	310	500	16
22	15	380	610	18
26	21,2	530	850	21
28	25	620	990	22
32	31,5	800	1 300	26
36	40	1 000	1 600	29
40	50	1 300	2 000	32
45	63	1 600	2 500	36

6.4.2 Breaking force (BF)

Samples of sling chains shall have a breaking force, F_B , at least equal to that specified in Table 4, column 4 calculated on the basis given in Annex A for the appropriate nominal size.

6.4.3 Total ultimate elongation, A

On completion of the tensile test, the minimum total ultimate elongation, A , as defined in ISO 1834 for chain in natural black, shall be 20 %, and for other surface finishes, A shall be 17 %.

6.4.4 Bend deflection, f

Samples of single chain links shall withstand the minimum value of the deflection, f , specified in Table 4, column 5, calculated on the basis given in Annex A, for the appropriate nominal size and shall be free from visible defects.

6.4.5 Toughness

The toughness of the finished chain shall be verified by impact test method on full-size, sub-size or super-sub-size specimens.

Full-size specimens shall be tested in accordance with ISO 148-1. Sub-size specimens shall be tested in accordance with ISO 14556. If the chain leg is too short to extract a full-length sub-size specimen, the sub-size specimens shall be produced according to Figure 3, by joining additional leg parts using laser welding. Super-sub-size specimens shall be tested in accordance with ISO 14556, except that the specimen dimensions shall be in accordance with Figure 4. Super-sub-size specimens shall be produced by joining additional leg parts using pulsed micro-laser welding. The settings for laser welding and pulsed micro-laser welding shall be such that the hardness and micro-structure of the specimen is not affected in the area of the notch. After welding, specimens shall be machined to the specified dimensions.

Either pendulum impact type or drop weight type test equipment may be used, taking account of the accuracy of measurement of the toughness value.

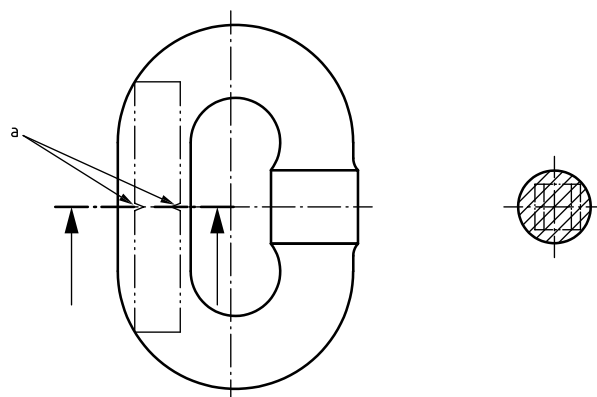
If the chain link is large enough to extract a full-size specimen, the tests shall be carried out on full-size specimens. Three specimens shall be tested, each of which shall achieve a KV toughness of at least 30 J at a test temperature of $-40\text{ }^{\circ}\text{C}$.

If the chain link is too small to extract a full-size specimen, but large enough to extract a sub-size specimen or a welded-on sub-size specimen, the tests shall be carried out on sub-size specimens, which shall achieve a KV toughness of at least 3,5 J at a test temperature of $-40\text{ }^{\circ}\text{C}$. To ensure that the distance of the test temperature to the brittle-tough-transition temperature is sufficient, KV toughness 3,5 J shall be $1/2 E_{US} + 1\text{ J}$ [half upper shelf energy (USE) + 1 J] or more. The test shall be carried out on 10 specimens, and the mean value used as the KV toughness value. The range of scattering shall be within 1,5 J.

If the chain link is too small to extract a sub-size specimen, the tests shall be carried out on super-sub-size specimens extracted from the chain and full-size specimens made of the same material as the chain, which is heat treated so as to achieve the same ultimate tensile strength of hardness and material as the finished chain. Three full-size specimens shall be tested, each of which shall achieve a KV toughness of at least 30 J at a test temperature of $-40\text{ }^{\circ}\text{C}$. Three super-sub-size specimens shall be tested and shall show 80 % or more non-crystalline area where tested at $-90\text{ }^{\circ}\text{C}$.

NOTE It is assumed that the transition temperature is $-90\text{ }^{\circ}\text{C}$ or lower in that case.

The above-mentioned tests shall be repeated if the steel manufacturer or type of steel is changed or the chain manufacturer changes the manufacturing process.

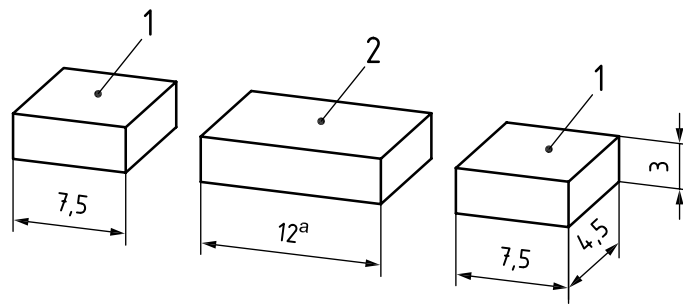


a Alternatives for orientation of the notch.

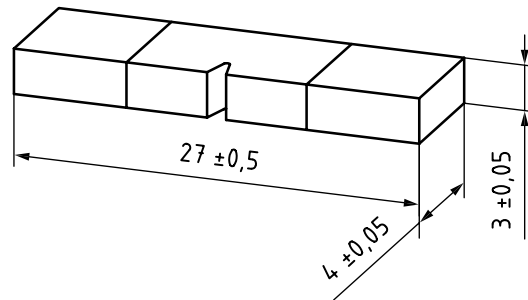
Figure 2 — Source of specimen and orientation of the notch

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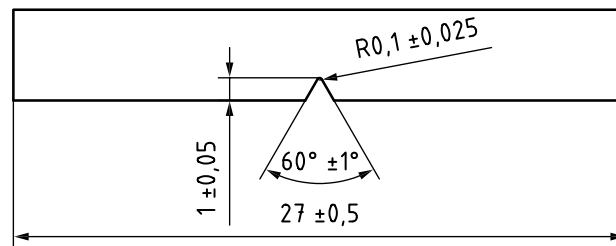
Dimensions in millimetres



a) Typical geometry of the specimen before welding



b) Welded on specimen after machining



c) Notch dimensions

Key

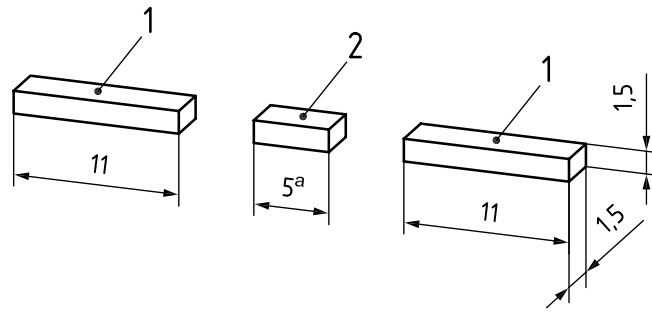
- 1 part for welding on
- 2 part of the chain leg

The geometry of the pendulum is in accordance with ISO 14556:2000/Amd.1:2006, Figure D.1.

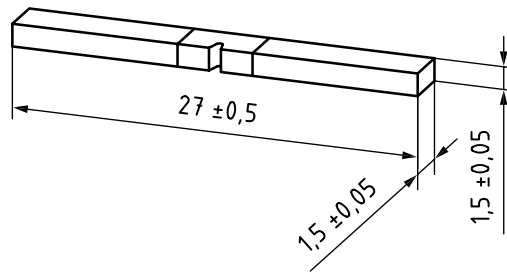
^a Minimum length of the chain material to be tested.

Figure 3 — Sub-size specimen

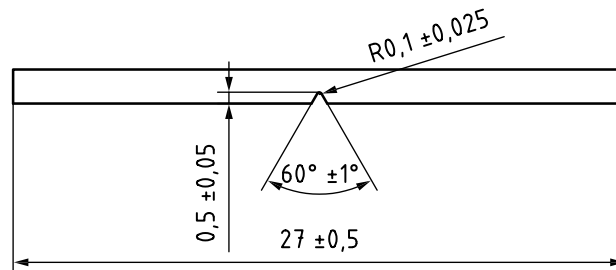
Dimensions in millimetres



a) Typical geometry of the specimen before welding



b) Notched specimen after welding



c) Notch dimensions

Key

- 1 part for welding on
- 2 part of the chain leg

The geometry of the pendulum is in accordance with ISO 14556:2000/Amd.1:2006, Figure D.1.

^a Minimum length of the chain material to be tested.

Figure 4 — Super-sub-size specimen

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Table 5 — Mechanical properties

Mechanical property	Requirements
Specified minimum nominal stress at breaking force, F_B : $\frac{2(F_B)}{\pi d_n^2}$	800 N/mm ²
Specified minimum nominal stress at manufacturing proof force, F_{MP} : $\frac{2(F_{MP})}{\pi d_n^2}$	500 N/mm ²
Percentage ratio of specified minimum nominal stress at manufacturing proof force to specified minimum nominal stress at breaking force: $\frac{F_{MP}}{F_B}$	62,5 %
Specified minimum total ultimate elongation for sling chains in natural black	20 %
Specified minimum total ultimate elongation for sling chains in other surface finishes	17 %
Specified minimum bend deflection, f	0,8 d_n mm
Specified maximum nominal stress at working load limit	200 N/mm ²
NOTE 1 The nominal stresses given in this table are obtained by dividing the force by the total cross-section of both sides of the chain link. The stresses are in fact not uniform and at the extrados, particularly at the crown, the maximum fibre stress is considerably greater.	
NOTE 2 The values for the working load can be selected to comply with national regulations, but in no case are they intended to exceed the values for the working load limit in Table 4, column 2.	

7 Verification of safety requirements

7.1 Size of lot and selection of samples

The size of the lot from which samples shall be selected shall be 200 m. An excess fraction of the length of lot shall be considered as a separate lot. Samples shall be selected as specified in ISO 1834.

7.2 Manufacturing proof force, breaking force and total ultimate elongation

7.2.1 Static tensile test

The testing machine and test procedure for the static tensile test shall be as specified in ISO 1834.

The testing machines and equipment used in the tests specified in 7.2.3 and 7.3.1 shall comply with ISO 7500-1, class 1.

7.2.2 Manufacturing proof force — Acceptance criteria

All the sling chains shall be subject to the manufacturing proof force specified in 6.4.1.

7.2.3 Breaking force and total ultimate elongation — Acceptance criteria

On completion of the static tensile test, the requirements of 6.4.2 and 6.4.3 shall be met.

7.3 Bend deflection

7.3.1 Bend test

The test equipment and procedure shall be as specified in ISO 1834.

Each single link sample shall be bent by a deflection, f , as given in Table 4, column 5, and shown in Figure 5. Following the removal of the force, the link sample shall be examined by a competent person (as specified in ISO 1834).

NOTE Where necessary, a surface coating can be removed after the bend test to enable this examination to be carried out.

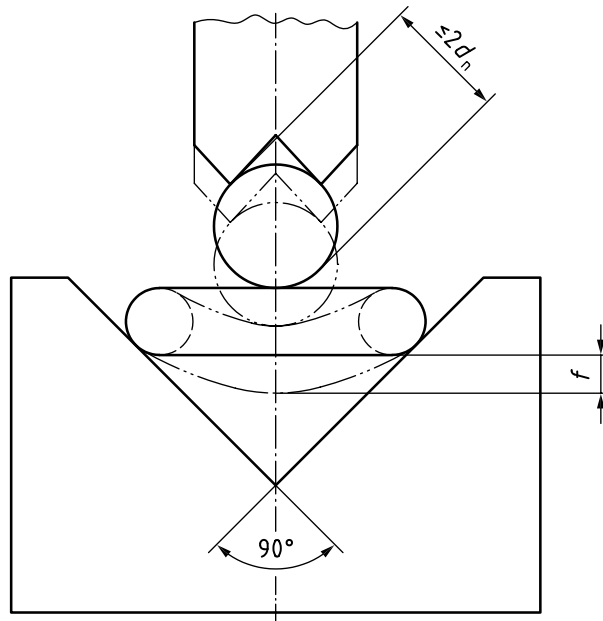


Figure 5 — Bend deflection, f

7.3.2 Bend deflection — Acceptance criteria

On completion of the bend test, the requirements of 6.4.4 shall be met.

7.4 Toughness of chain test material

7.4.1 Toughness test

Specimens shall be tested in accordance with ISO 148-1 or ISO 14556, as appropriate according to the size of the specimen.

7.4.2 Toughness test — Acceptance criteria

The requirements of 6.4.5 shall be met. The requirements shall be verified by the testing of a specimen at a temperature in the upper shelf with a 100 % non-crystalline area as the bases for Formula (1).

$$E_D \geq \frac{1}{2} E_{US} + 1 J \quad (1)$$

where

E_D is the design energy, expressed in joules;

E_{US} is the upper shelf energy, expressed in joules.

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8 Marking

8.1 Grade marking

The grade mark for the medium tolerance sling chain is “8”. The marking shall conform to ISO 1834 and shall be applied as specified in ISO 1834.

8.2 Identification marking

The identification marking shall be as specified in ISO 1834.

8.3 Inspection marking

The inspection marking shall be as specified in ISO 1834.

9 Manufacturer’s certificate

The manufacturer shall, if required, supply a certificate of testing and examination with every supply of sling chain containing the information detailed in ISO 1834.

Annex A (informative)

Bases for calculation

A.1 Dimensions and tolerances

A.1.1 Diameter tolerance

For nominal sizes less than 18 mm, the diameter of the material in the finished chain link should nowhere differ from the nominal diameter by more than +2 %/–6 %, except at the weld.

For nominal sizes 18 mm and greater, the diameter of the material in the finished chain link should nowhere differ from the nominal diameter by more than ± 5 %, except at the weld.

A.1.2 Pitch and tolerance

The values for the nominal pitch, p_n , are based on $3 \times d_n$. The calculated values are rounded to 1 mm. These rounded values are listed in Table 1, column 3.

The pitch tolerances are based on ± 3 %. The calculated values are rounded to 0,1 mm. These rounded values are listed in Table 1, column 4.

A.1.3 Width

The values for the internal width of type 2 w_1 are based on $1,25 \times d_n$. The calculated values are rounded to 0,1 mm. These rounded values are listed in Table 1, column 5.

The values for the external width of types 1 and 2 w_3 are based on $3,7 \times d_n$. The calculated values of < 100 mm are rounded to 0,1 mm. The calculated values of ≥ 100 mm are rounded to 1 mm. These rounded values are listed in Table 1, column 6.

The values for the internal width of type 1 w_4 are based on $1,3 \times d_n$. The calculated values are rounded to 0,1 mm. These rounded values are listed in Table 1, column 7.

A.1.4 Weld diameter

The values for the weld diameter of type 1 or for the weld dimension perpendicular to the plane of the link of type 2 d_w are based on $1,1 \times d_n$. The calculated values are rounded to 0,1 mm. These rounded values are listed in Table 1, column 8.

The values for the dimension in other planes of type 2 G are based on $1,25 \times d_n$. The calculated values are rounded to 0,1 mm. These rounded values are listed in Table 1, column 9.

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A.2 Working load limits and test requirements

A.2.1 General

The stresses used in the calculation of values for the working load limit and the test requirements in Formulae (A.1) to (A.3), given in A.2.2 to A.2.4, are nominal stresses as follows:

- a) nominal working stress = 200 N/mm²;
- b) nominal manufacturing proof stress = 500 N/mm²;
- c) nominal breaking stress = 800 N/mm².

A.2.2 Working load limit (WLL)

The values for the working load limit (WLL) are based on Formula (A.1):

$$M_{WLL} = \frac{2 \times \frac{1}{4} \times \pi \times 200 \times d_n^2}{g \times 1000} \quad (\text{A.1})$$

$$M_{WLL} = 0,032\ 035 \times d_n^2$$

where

M_{WLL} is the working load limit (WLL), expressed in tonnes;

g is the acceleration due to gravity, expressed in metres per square second (m/s², i.e. 9,806 65).

Based upon ISO 2374, the calculated values are rounded down to the nearest lower value of the R40 series of preferred numbers in accordance with ISO 497. These rounded values are listed in Table 4, column 2.

A.2.3 Manufacturing proof force (MPF)

The values for the manufacturing proof force (MPF) are based on Formula (A.2):

$$F_{MP} = \frac{2 \times \frac{1}{4} \times \pi \times 500 \times d_n^2}{1000} \quad (\text{A.2})$$

$$F_{MP} = 0,785\ 398 \times d_n^2$$

where F_{MP} is the manufacturing proof force (MPF), expressed in kilonewtons.

The calculated values < 100 kN are rounded to 1 kN. The calculated values ≥ 100 kN but < 1 000 kN are rounded to 10 kN. The calculated values ≥ 1 000 kN are rounded to 100 kN. These rounded values are listed in Table 4, column 3.

A.2.4 Breaking force (BF)

The values for the breaking force (BF), F_B , are based on Formula (A.3):

$$F_B = \frac{2 \times \frac{1}{4} \times \pi \times 800 \times d_n^2}{1\,000} \quad (\text{A.3})$$

$$F_B = 1,256\,637 \times d_n^2$$

where F_B (BF) is the breaking force, expressed in kilonewtons.

The calculated values < 100 kN are rounded to 1 kN. The calculated values \geq 100 kN but < 1 000 kN are rounded to 10 kN. The calculated values \geq 1 000 kN are rounded to 100 kN. These rounded values are listed in Table 4 column 4.

A.2.5 Bend deflection

The values for the bend deflection, f , are based on Formula (A.4):

$$f = 0,8 \times d_n \quad (\text{A.4})$$

where f is the bend deflection, expressed in millimetres.

The calculated values < 10 mm are rounded to 0,1 mm. The calculated values \geq 10 mm are rounded to 1 mm. These rounded values are listed in Table 4, column 5.

Annex B (informative)

Mass of sling chains

The values for the approximate mass per metre, W , are based on Formula (B.1):

$$W = 2,842 \times \rho \times 10^{-3} \times d_n^2 \quad (\text{B.1})$$

where

W is the approximate mass per metre, expressed in kilograms per metre;

ρ is the mass density, expressed in kilograms per cubic metre (i.e. 7,85).

The calculated values < 1 kg/m are rounded to 0,01 kg/m. The calculated values ≥ 1 kg/m but < 10 kg/m are rounded to 0,1 kg/m. The calculated values ≥ 10 kg/m are rounded to 1 kg/m. These rounded values are listed in Table B.1, column 2.

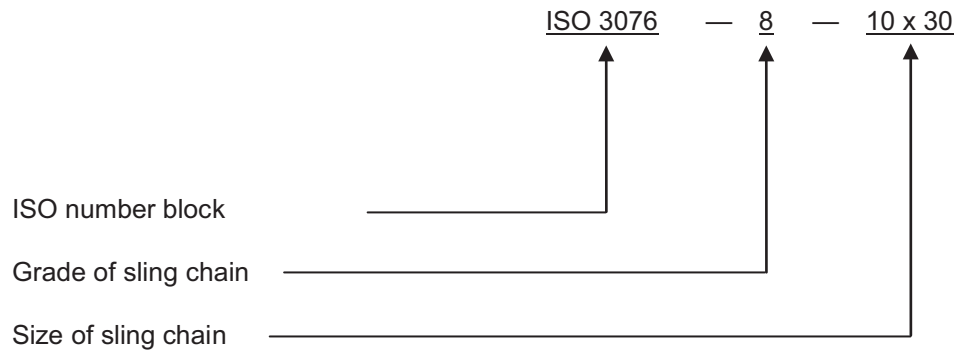
Table B.1 — Mass of sling chains

1	2
Nominal size	Mass per metre
d_n	W
mm	kg/m
4	0,36
6	0,80
7	1,1
8	1,40
10	2,20
13	3,80
16	5,70
18	7,20
19	8,10
20	8,90
22	11,00
26	15,00
28	17,00
32	23,00
36	29,00
40	36,00
45	45,00

Annex C (informative)

Designation system

General format



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- [1] ISO 2374, *Lifting appliances, range of maximum capacities for basic models*
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