INTERNATIONAL STANDARD

ISO 1585

Third edition 1992-11-01

Road vehicles — Engine test code — Net power

Véhicules routiers - Code d'essai des moteurs - Puissance nette



Reference number ISO 1585: 1992 (E)

Foreword

ISO (the International Organization for Standardization) is a worldwide federation of national standards bodies (ISO member bodies). The work of preparing International Standards is normally carried out through ISO technical committees. Each member body interested in a subject for which a technical committee has been established has the right to be represented on that committee. International organizations, governmental and non-governmental, in liaison with ISO, also take part in the work. ISO collaborates closely with the International Electrotechnical Commission (IEC) on all matters of electrotechnical standardization.

Draft International Standards adopted by the technical committees are circulated to the member bodies for voting. Publication as an International Standard requires approval by at least 75 % of the member bodies casting a vote.

International Standard ISO 1585 was prepared by Technical Committee ISO/TC 22, *Road vehicles*, Sub-Committee SC 5, *Engine tests*.

This third edition cancels and replaces the second edition (ISO 1585: 1982), of which it constitutes a technical revision.

NOTE - This international Standard is also the basis for the following parallel documents:

ISO 2288 : 1989, Agricultural tractors and machines — Engine test code (bench test) — Net power.

ISO 4106: 1978, Road vehicles - Motorcycles - Engine test code - Net power.

ISO 4164: 1978, Road vehicles - Mopeds - Engine test code - Net power.

ISO 9249: 1989, Earth-moving machinery - Engine test code - Net power.

ISO 2534: 1974, Road vehicles — Engine test code — Gross power, provides a similar test code for gross power.

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Road vehicles — Engine test code — Net power

1 Scope

This International Standard specifies a method for testing engines designed for automotive vehicles. It applies to the evaluation of their performance with a view, in particular, to presenting curves of power and specific fuel consumption at full load as a function of engine speed.

It applies only to net power assessment.

This International Standard concerns internal combustion engines used for propulsion of passenger cars and other motor vehicles, excluding motorcycles, mopeds and agricultural tractors (see the note in the foreword), normally travelling on roads and included in one of the following categories:

- reciprocating internal combustion engines (sparkignition or compression-ignition) but excluding free piston engines;
- rotary piston engines.

These engines may be naturally aspirated or pressure-charged, either using a mechanical supercharger or turbocharger.

2 Normative references

The following standards contain provisions which, through reference in this text, constitute provisions of this International Standard. At the time of publication, the editions indicated were valid. All standards are subject to revision, and parties to agreements based on this International Standard are encouraged to investigate the possibility of applying the most recent editions of the standards indicated below. Members of IEC and ISO maintain registers of currently valid International Standards.

ISO 2710 : 1978, Reciprocating internal combustion engines — Vocabulary.

ISO 3104: 1976, Petroleum products — Transparent and opaque liquids — Determination of kinematic viscosity and calculation of dynamic viscosity.

ISO 3173: 1974, Road vehicles — Apparatus for measurement of the opacity of exhaust gas from diesel engines operating under steady state conditions.

ISO 3675 : —1), Crude petroleum and liquid petroleum products — Laboratory determination of density or relative density — Hydrometer method.

ISO 5163: 1990, Motor and aviation-type fuels — Determination of knock characteristics — Motor method.

ISO 5164: 1990, Motor fuels — Determination of knock characteristics — Research method.

ISO 5165: 1992, Diesel fuels — Determination of ignition quality — Cetane method.

ISO 7967-1: 1987, Reciprocating internal combustion engines — Vocabulary of components and systems — Part 1: Structure and external covers.

ISO 7967-2: 1987, Reciprocating internal combustion engines — Vocabulary of components and systems — Part 2: Main running gear.

ISO 7967-3: 1987, Reciprocating internal combustion engines — Vocabulary of components and systems — Part 3: Valves, camshaft drive and actuating mechanisms.

ISO 7967-4: 1988, Reciprocating internal combustion engines — Vocabulary of components and systems — Part 4: Pressure charging and air/exhaust gas ducting systems.

ISO 7967-5: 1992, Reciprocating internal combustion engines — Vocabulary of components and systems — Part 5: Cooling systems.

ISO 7967-8: 1990, Reciprocating internal combustion engines — Vocabulary of components and systems — Part 8: Starting systems.

ASTM D 240-87, Standard test method for heat of combustion of liquid hydrocarbon fuels by bomb calorimeter.

ASTM D 3338-88, Standard test method for estimation of heat of combustion of aviation fuels.

¹⁾ To be published. (Revision of ISO 3675: 1976.)

3 Definitions

For the purposes of this International Standard, the definitions given in ISO 2710, ISO 7967-1, ISO 7967-2, ISO 7967-3, ISO 7967-4, ISO 7967-5 and ISO 7967-8, and the following definitions apply.

- **3.1** net power: Power obtained on a test bed at the end of the crankshaft or its equivalent 1) at the corresponding engine speed with the equipment and auxiliaries listed in table 1.
- **3.2 standard production equipment:** Any equipment provided by the manufacturer for a particular engine application.

4 Accuracy of measuring equipment and instruments

4.1 Torque

The dynamometer torque-measuring system shall have an accuracy within \pm 1 % in the range of scale values required for the test.

4.2 Engine speed (rotational frequency)

The engine speed (rotational frequency) measuring system shall have an accuracy of \pm 0,5 %.

4.3 Fuel flow

The fuel flow measuring system shall have an accuracy of \pm 1 %,

4.4 Fuel temperature

The fuel temperature measuring system shall have an accuracy of \pm 2 K.

4.5 Air temperature

The air temperature measuring system shall have an accuracy of ± 2 K.

4.6 Barometric pressure

The barometric pressure measuring system shall have an accuracy of \pm 100 Pa².

4.7 Back pressure in exhaust system

The system used to measure the back pressure in the exhaust system shall have an accuracy of \pm 200 Pa. The measurement shall be made subject to footnote 1b) of table 1.

4.8 Depression in inlet system

The system used to measure the depression in the inlet system shall have an accuracy of ± 50 Pa. The measurement shall be made subject to footnote 1a) of table 1.

4.9 Absolute pressure in inlet duct

The system used to measure the absolute pressure in the inlet duct shall have an accuracy of ± 2 % of the measured pressure.

¹⁾ If the power measurement can only be carried out with a mounted gear-box, the losses in the gear-box should be added to the measured power to give the engine power.

²⁾ $1 \text{ Pa} = 1 \text{ N/m}^2$

Table 1 — Installation of equipment and auxiliaries during test

No.	Auxiliaries		Fitted for net power test
1	Inlet system Inlet manifold Crankcase emission control system Control devices for dual induction inlet manifold system Air flow meter Air inlet ductwork 1a) Air filter 1a) Inlet silencer 1a) Speed-limiting device 1a)		Yes, standard production equipment
2	Induction heating device of inlet manifold		Yes, standard production equipment. If possible, to be set in the most favourable position
3	Exhaust system Exhaust purifier Exhaust manifold Pressure-charging devices Connecting pipes 1b) Silencer 1b) Tail pipe 1b) Exhaust brake 2)		Yes, standard production equipment
4	Fuel supply pump ³⁾		Yes, standard production equipment
5	Carburation equipment Carburettor Electronic control system, air-flow meter, etc. (if fitted) Equipment for gaseous fuel engines Pressure reducer Evaporator Mixer	$\left. \left. \right \right $	Yes, standard production equipment
6	Fuel injection equipment [Spark-ignition and compression-ignition (diesel)] Prefilter Filter Pump High-pressure pipe Injector Air inlet valve (if fitted) 4) Electronic control system, etc. (if fitted) Governor/control system — automatic full-load stop for the control depending on atmospheric conditions		Yes, standard production equipment
7	Liquid cooling equipment Radiator Fan ⁵⁾ , ⁶⁾ Fan cowl Water pump Thermostat ⁷⁾	$\left. \right\}$	Yes, ⁵⁾ standard production equipment
8	Air cooling Cowl Fan or blower ^{5),6)} Temperature regulating device	}	Yes, standard production equipment

Table 1 - Installation of equipment and auxiliaries during test (concluded)

No.	Auxiliaries	Fitted for net power test
9	Electrical or electronic ignition equipment Generator ⁸⁾ Spark distribution system Coil or coils Wiring Spark-plugs Electronic control system including knock sensor/spark-retard system ¹¹⁾	Yes, standard production equipment
10	Pressure-charging equipment (if fitted) Compressor driven either directly by the engine, and/or by the exhaust gases Boost control ¹²⁾ Charge-air-cooler ^{5), 6), 9)} Coolant pump or fan (engine-driven) Coolant flow control devices (if fitted)	Yes, standard production equipment
11	Auxiliary test bed fan	Yes, if necessary
12	Anti-pollution devices 10)	Yes, standard production equipment

- 1a) Except in the case where there is a risk of the system having a noticeable influence upon engine power, an equivalent system may be used. In this case, a check should be made to ascertain that inlet depression does not differ by more than 100 Pa from the limit specified by the manufacturer for a clean air filter.
- 1b) Except in the case where there is a risk of the system having a noticeable influence upon engine power, an equivalent system may be used. In this case, a check should be made to ascertain that the back-pressure in the engine exhaust system does not differ by more than 1 000 Pa from that specified by the manufacturer.
- 2) If an exhaust brake is incorporated in the engine, the throttle valve shall be fixed fully open.
- 3) The fuel feed pressure may be adjusted, if necessary, to reproduce the inlet pump pressure conditions consistent with the particular engine application (particularly where a "fuel return" system, e.g. to tank or filter, is used).
- 4) The air inlet valve is the control valve for the pneumatic governor of the injection pump. The governor of the fuel injection equipment may contain other devices which may affect the amount of fuel injected.
- 5) The radiator, fan, fan cowl, water pump and thermostat shall be located on the test bed in the same relative positions that they will occupy on the vehicle. The cooling liquid circulation shall be operated by the engine water pump only.

Cooling of the liquid may be produced either by the engine radiator or by an external circuit, provided that the pressure loss of this circuit and the pressure at the pump inlet remain substantially the same as those of the engine cooling system. The radiator shutter, if incorporated, shall be in the open position.

Where the fan, radiator and cowl system cannot conveniently be fitted to the engine, the power absorbed by the fan when separately mounted in its correct position in relation to the radiator and cowl (if used), shall be determined at the speeds corresponding to the engine speeds used for measurement of the engine power either by calculation from standard characteristics or by practical tests. This power corrected to the standard atmospheric conditions defined in 6.2 shall be deducted from the corrected power.

- 6) Where a disconnectable or progressive fan or blower is incorporated, the test shall be made with the disconnectable fan or blower disconnected or with the progressive fan running at maximum slip.
- 7) The thermostat may be fixed in the fully open position.
- 8) Minimum power of the generator: the power of the generator shall be limited to that necessary for the operation of accessories which are indispensable for engine operation. If the connection of a battery is necessary, a fully charged battery in good order shall be used.
- 9) Charge-air-cooled engines shall be tested complete with charge-air-cooling whether liquid- or air-cooled, but, if the engine manufacturer prefers, a test bed system may replace the air-cooled cooler. In either case the measurement of power at each speed shall be made with the pressure drop and temperature drop of the engine air across the charge air cooler in the test bed the same as those specified by the manufacturer for the system on the complete vehicle.

If a test bed system is used on a compression-ignition engine without a wastegate, or with the wastegate not operating, the correction factor given in 6.3.2.1 b) is to be used. If a wastegate is both fitted and operating, then the correction factor in 6.3.2.1 a) is to be used.

- 10) They may include for example EGR system, catalytic convertor, thermal reactor, secondary air supply system and fuel evaporation protecting system.
- 11) The spark advance shall be representative of in-use conditions established with the minimum octane fuel recommended by the manufacturer.
- 12) For engines equipped with variable boost as a function of charge or inlet air temperature, octane rating and/or engine speed, the boost pressure shall be representative of in-vehicle conditions established with the minimum octane fuel as recommended by the manufacturer.

5 Tests

5.1 Auxiliaries

5.1.1 Auxiliaries to be fitted

During the test auxiliaries necessary to make engine acceptable for service in the intended application (as listed in table 1) shall be installed on the test bed as far as possible in the same position as in the intended application.

5.1.2 Auxiliaries to be removed

Certain vehicle accessories necessary only for the operation of the vehicle, and which may be mounted on the engine, shall be removed for the test. The following non-exhaustive list is given as an example:

- air compressor for brakes;
- power steering pump;
- suspension compressor;
- air-conditioning system.

Where accessories cannot be removed, the power absorbed by them in the unloaded condition may be determined and added to the measured engine power.

5.1.3 Compression-ignition engine starting auxiliaries

For auxiliaries used to start compression-ignition engines, the two following cases shall be considered:

- a) Electrical starting. The generator is fitted and supplies, where necessary, the auxiliaries indispensable to the operation of the engine.
- b) Starting other than electrical. If there are any electrically operated accessories indispensable to the operation of the engine, the generator is fitted to supply these accessories. Otherwise, it is removed.

In either case, the system for producing and accumulating the energy necessary for starting is fitted and operates in the unloaded condition.

5.2 Setting conditions

The setting conditions for the test for determination of net power are indicated in table 2.

Table 2 — Setting conditions

1	Setting of carburettor(s)	
2	Setting of injection pump delivery system	In accordance with the manufacturer's produc-
3	Ignition or injection timing (timing curve)	tion specifications and used without further
4	Governor setting	alteration for the particular
5	Anti-pollution devices	application.
6	Boost control	

5.3 Test conditions

- **5.3.1** The net power test shall consist of a run at full throttle for spark-ignition engines and at the fixed full-load fuel injection pump setting for compression-ignition engines, the engine being equipped as specified in table 1.
- **5.3.2** Performance data shall be obtained under stabilized operating conditions, with an adequate fresh air supply to the engine.

Engines shall have been run-in, started and warmed up in accordance with the manufacturer's recommendations. Combustion chambers may contain deposits, but in limited quantity. Test conditions such as inlet air temperature shall be selected as near to reference conditions (see 6.2) as possible in order to minimize the correction factor.

5.3.3 The temperature of the inlet air to the engine (ambient air), shall be measured within 0,15 m upstream of the air inlet ductwork.

The thermometer or thermocouple shall be shielded from radiant heat and located directly in the airstream. It shall also be shielded from fuel sprayback. A sufficient number of locations shall be used to give a representative average inlet temperature.

- **5.3.4** The inlet depression shall be measured downstream of the entry ducts, air filter, inlet silencer, speed-limiting device (if they are fitted) or their equivalents.
- **5.3.5** The absolute pressure at the entry to the engine, downstream of the compressor and heat exchanger if they are fitted, shall be measured in the inlet manifold and at any other point where pressure has to be measured to calculate correction factors.
- **5.3.6** The exhaust back pressure shall be measured at a point at least three pipe diameters from the outlet flange(s) of the exhaust manifold(s) and downstream of the turbocharger(s), if fitted. The location shall be specified.
- **5.3.7** No data shall be taken until torque, speed and temperature have been maintained substantially constant for at least 1 min.
- **5.3.8** The engine speed during a run or reading shall not deviate from the selected speed by more than \pm 1 % or \pm 10 min⁻¹, whichever is greater.
- **5.3.9** Observed brake load, fuel flow and inlet air temperature data shall be taken virtually simultaneously and shall, in each case, be the average of two stabilized consecutive readings which do not vary more than 2 % for the brake load and fuel consumption. The second reading shall be determined without any adjustment of the engine, approximately 1 min after the first.

5.3.10 The coolant temperature at the engine outlet shall be kept within \pm 5 K of the upper thermostatically controlled temperature specified by the manufacturer. If no temperature is so specified, the temperature shall be 353 K \pm 5 K.

For air-cooled engines, the temperature at a point indicated by the manufacturer shall be kept within $_{20}^{0}$ K of the maximum value specified by the manufacturer in the reference conditions.

5.3.11 Fuel temperatures shall be as follows:

- a) For spark-ignition engines, the fuel temperature shall be measured as near as possible to the inlet of the carburettor or assembly of fuel injectors. Fuel temperature shall be maintained within \pm 5 K of the temperature specified by the manufacturer. However, the minimum test fuel temperature allowed shall be the ambient air temperature. If the test fuel temperature is not specified by the manufacturer, it shall be 298 K \pm 5 K.
- b) For compression-ignition engines, the fuel temperature shall be measured at the inlet to the fuel-injection pump. At the manufacturer's request the fuel temperature measurement can be made at another point in the pump representative of the engine operating condition. Fuel temperature shall be maintained within $\pm 3~\rm K$ of the temperature specified by the manufacturer. In all cases, the minimum allowable fuel temperature at the pump entrance is 303 K. If the test fuel temperature is not specified by the manufacturer, it shall be 313 K $\pm 3~\rm K$.
- **5.3.12** The lubricant temperature shall be measured at the oil gallery inlet or the oil cooler outlet if fitted, unless some other measuring location is specified by the manufacturer. The temperature shall be maintained within the limits specified by the manufacturer.
- **5.3.13** An auxiliary regulation system may be used if necessary to maintain temperature within limits specified in 5.3.10, 5.3.11 and 5.3.12.
- **5.3.14** It is recommended that a reference fuel is used; a non-exhaustive list of such fuels includes:

CEC RF-01-A-801)

CEC RF-08-A-85

CEC RF-03-A-84

JIS K 22022)

JIS K 2204

40 CFR, Part 86.113-873) for spark-ignition engines

40 CFR, Part 86.1313-87 for compression-ignition engines

A commercially available fuel may be used, providing its characteristics are specified in 8.3 and that it does not contain any supplementary smoke-suppressant or additive.

5.4 Test procedure

Measurements shall be taken at a sufficient number of engine speeds to define the power curve completely between the lowest and the highest engine speeds recommended by the manufacturer. This range of speeds shall include the revolution speed at which the engine produces its maximum power.

5.5 Data to be recorded

Data to be recorded shall be those indicated in clause 8.

6 Power correction factors

6.1 Definition of factor α for power correction

This is factor by which the observed power shall be multiplied to determine the engine power at the reference atmospheric conditions specified in 6.2. The corrected power (i.e. power at reference conditions), $P_{\rm ref}$, is given by

$$P_{\text{ref}} = \alpha P_{\text{v}}$$

where

 α is the correction factor (α_a being the correction factor for spark-ignition engines and α_c the correction factor for compression-ignition engines);

 $P_{\rm v}$ is the measured (observed) power.

6.2 Atmospheric conditions

6.2.1 Reference atmospheric conditions

The reference atmospheric conditions shall be as given in 6,2,1,1 and 6,2,1,2,

6.2.1.1 Temperature

The reference temperature, $T_{\rm ref}$, is 298 K (25 °C).

¹⁾ Co-ordinating European Council for the Development of Performance Tests for Lubricants and Engine Fuels.

²⁾ Japan Industrial Standard.

³⁾ Title 40, Code of Federal Regulations, USA.

6.2.1.2 Dry pressure

The reference dry pressure, $p_{\rm d, ref}$, is 99 kPa.

NOTE — The dry pressure is based on a total pressure of 100 kPa and a vapour pressure of 1 kPa.

6.2.2 Test atmospheric conditions

The test atmospheric conditions shall be within the values given in 6.2.2.1 and 6.2.2.2 during the test.

6.2.2.1 Temperature, T

- for spark-ignition engines

for compression-ignition engines

283 K
$$< T < 313$$
 K

6.2.2.2 Dry pressure, p_d

For all engines

80 kPa
$$< p_{\rm d} <$$
 110 kPa

6.3 Determination of power correction factors

The test may be carried out in air-conditioned test rooms where the atmospheric conditions are controlled to equal the reference conditions.

Where an influencing parameter is controlled by an automatic device, no power correction for that parameter shall be applied, provided that the relevant parameter is within the relevant range of the device. This applies in particular to

- a) automatic air temperature controls where the device is still operating at 25 °C;
- b) automatic boost control, independent of atmospheric pressure, when the atmospheric pressure is such that the boost control is working;
- automatic fuel control where the governor adjusts the fuel flow for constant power output (by compensating for the influence of ambient pressure and temperature).

However, in the case of a), if the automatic air temperature device is fully closed at full load at 25 °C (no heated air added to the intake air), the test shall be carried out with the device fully closed, and the normal correction factor applied. In the case of c), the fuel flow for compression-ignition engines shall be corrected by the reciprocal of the power correction factor.

6.3.1 Naturally aspirated and pressure-charged spark-ignition engines — Factor $\alpha_{\rm a}$

The correction factor, $\alpha_{\rm a}$, for spark-ignition engines shall be as calculated from the formula

$$\alpha_{\rm a} = \left(\frac{99}{p_{\rm d}}\right)^{1.2} \left(\frac{T}{298}\right)^{0.6}$$

where

 T_{\parallel} is the absolute temperature, in kelvins, at the engine air inlet:

 $p_{\rm d}$ is the dry atmospheric pressure, in kilopascals, i.e. the total barometric pressure minus the water vapour pressure.

This formula applies to carburettored engines and to other engines where the management system is designed to maintain a relatively constant fuel/air ratio as ambient conditions change. For other engine types see 6.3.3.

This formula only applies if

$$0.93 \le \alpha_{\rm a} \le 1.07$$

If these limits are exceeded, the corrected value obtained shall be given, and the test conditions (temperature and pressure) precisely stated in the test report.

6.3.2 Compression-ignition engines — Factor α_c

The power correction factor, $\alpha_{\rm c}$, for compression-ignition engines at constant fuel delivery setting is obtained by applying the formula

$$\alpha_{\rm c} = (f_{\rm a})^{f_{\rm m}}$$

where

 f_a is the atmospheric factor (see 6.3.2.1);

 $f_{\rm m}$ is the characteristic parameter for each type of engine and adjustment (see 6.3.2.2).

6.3.2.1 Atmospheric factor, f_a

The atmospheric factor, f_a , which indicates the effect of environmental conditions (pressure, temperature and humidity) on the air drawn in by the engine shall be as calculated from the formula in a), b) or c):

a) naturally aspirated engines, mechanically pressurecharged engines and turbocharged engines with wastegates operating: 1)

$$f_{\mathsf{a}} = \left(\frac{99}{p_{\mathsf{d}}}\right) \left(\frac{T}{298}\right)^{0.7}$$

¹⁾ For engine speeds when the wastegate of a turbocharged engine is not operating, formula a) or b) is used, depending on the type of charge cooling, if any.

b) turbocharged engines without charge air cooling or with charge cooling by air/air cooler:

$$f_{\rm a} = \left(\frac{99}{p_{\rm d}}\right)^{0.7} \left(\frac{T}{298}\right)^{1.2}$$

c) turbocharged engines with charge air cooling by engine coolant:

$$f_{\rm a} = \left(\frac{99}{p_{\rm d}}\right)^{0.7} \left(\frac{T}{298}\right)^{0.7}$$

where T and p_d are as defined in 6.3.1.

6.3.2.2 Engine factor, $f_{\rm m}$

Within the limits established for $\alpha_{\rm c}$ in 6.3.2, the engine factor, $f_{\rm m}$, is a function of the corrected fuel delivery parameter, $q_{\rm c}$, and is calculated from the formula

$$f_{\rm m} = 0.036 \, q_{\rm c} - 1.14$$

where

$$q_{\rm c} = \frac{q}{r}$$

in which

q is the fuel delivery parameter, in milligrams per cycle per litre of engine swept volume [mg/($l \cdot cycle$)], and is equal to

$$\frac{(Z) \times (\text{fuel flow in g/s})}{(\text{displacement in I}) \times (\text{engine speed in min}^{-1})}$$

where

 $Z = 120\ 000$ for 4-stroke cycle engines and $Z = 60\ 000$ for 2-stroke cycle engines;

r is the ratio between the absolute static pressure at the outlet of the pressure charger, or charge air cooler if fitted, and the ambient pressure (r = 1 for naturally aspirated engines).

The formula for the engine factor, $f_{\rm m}$, is only valid for a $q_{\rm c}$ value between 37,2 mg/(I·cycle) < $q_{\rm c}$ < 65 mg/(I·cycle). For values less than 37,2 mg/(I·cycle), a constant value of 0,2 shall be taken for $f_{\rm m}$, while for $q_{\rm c}$ values greater than 65 mg/(I·cycle), a constant value of 1,2 shall be taken for $f_{\rm m}$ (see figure 1).

6.3.2.3 Limitation in use of correction formula

This correction formula only applies if

$$0.9 < \alpha_{\rm c} < 1.1$$

If these limits are exceeded, the corrected value obtained shall be given, and the test conditions (temperature and pressure) precisely stated in the test report.

6.3.3 Other types of engine

For engines not covered by 6.3.1 and 6.3.2, a correction factor equal to 1 shall be applied when the ambient air density does not vary by more than \pm 2 % from the density at the reference conditions (298 K and 99 kPa). When the ambient air density is beyond these limits, no correction shall be applied, but the test conditions shall be stated in the test report.

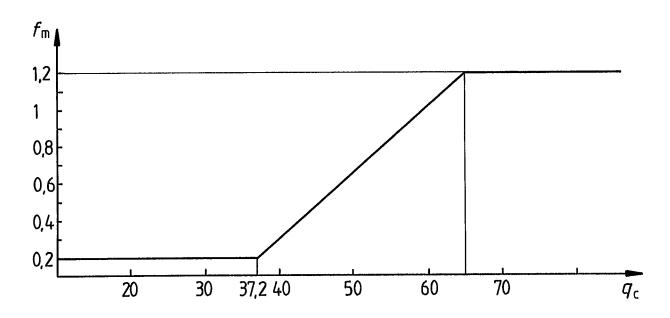


Figure 1 — Engine factor, $f_{
m m}$, as a function of corrected fuel delivery parameter, $q_{
m c}$

7 Measurement of and correction for smoke value for compression-ignition engines

The smoke value shall be measured and recorded at every test point. The opacimeter used, and its installation, shall meet the requirements of ISO 3173.

7.1 Correction factor for light absorption coefficient of smoke

This is the factor by which the light absorption coefficient of smoke, $S_{\rm r}$, expressed in absolute units of metres to the power minus one, shall be multiplied to determine the engine light absorption coefficient of smoke at the reference atmospheric conditions specified in 6.2.1:

$$S_{\rm r} = \alpha_{\rm s} S$$

where

 α_s is the correction factor (see 7.2);

 ${\it S}$ is the measured light absorption coefficient of smoke, in reciprocal metres (observed smoke).

7.2 Determination of correction factor for light absorption coefficient of smoke

The correction factor, $\alpha_{\rm s}$, for compression-ignition engines under a constant fuel delivery setting is obtained from the following formula

$$\alpha_{\rm s} = 1 - 5 (f_{\rm a} - 1)$$

where f_a is the atmospheric factor (see 6.3.2.1).

7.3 Limits of application

This correction factor only applies when, for approval purposes,

$$0.92 \le f_{\rm a} \le 1.08$$

283 K
$$\leq T \leq$$
 313 K

80 kPa
$$\leq p_{\rm d} \leq$$
 110 kPa

8	Test	report
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(State '	'none''	where	inappl	icable	, or	delete)	ł
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8.1 Compression-ignition engines — Essential charact	ceristics ¹⁾
8.1.1 Description of engine	
Make :	
Туре:	
Cycle: four-stroke/two-stroke ²⁾	
Bore:mm	
Stroke:mm	
Number of cylinders :	
Layout of cylinders :	Firing order:
Engine swept volume: litres	
Compression ratio ³⁾ :	
Cooling system	
• •	
a) Liquid	
Nature of liquid:	
Circulating pumps: yes/no ²⁾	
Characteristics or make(s) :	Type(s) :
Drive ratio:	
Thermostat: setting:	
Radiator: drawing(s) or make(s):	Type(s) :
Relief valve:	
Fan: characteristics or make(s):	Type(s) :
Fan drive system:	
Drive ratio:	
Fan cowl :	

¹⁾ In the case of non-conventional engines and systems, particulars equivalent to those referred to here shall be supplied by the manufacturer.

²⁾ Delete where inapplicable.

³⁾ Specify the tolerance.

b)	Air		
	Blower: characteristics or make(s):	Туре(s) :	
	Drive ratio:		
	Air ducting (standard production) :		
	Temperature regulation system: yes/no 1)		
	Brief description:		
c)	Temperatures specified by the manufacturer		
	Liquid cooling		
	Maximum temperature at outlet		κ
	Air cooling		
	Reference point (description):		
	Maximum temperature at reference point:		К
	Maximum exhaust temperature :		κ
	Fuel temperature : min. :	max.:	к
	Lubricant temperature : K		
Press	sure charger: with/without 1)		
	Description of the system :		
	Make :	Туре :	
	Compressor system: Make :	Туре:	
	Charge-air-cooling system: Make:	Туре:	
Inlet	system		
	Description and diagrams of air inlets and their accessories (heat	ing device, inlet silencer, etc.)	
	Inlet manifold:	Description:	
	Air filter:	Make :	Туре:
	Inlet silencer:	Make :	Туре :

¹⁾ Delete where inapplicable.

8.1.2	Additional smoke control devices (if any, and if not covered by another heading)
Descr	iption and diagrams :
8.1.3	Fuel feed system
Fuel f	eed ;
Fe	ed pump
	Pressure: kPa ¹⁾ or characteristic diagram ²⁾ :
ln)	ection system :
	Pump
	Make(s):
	Type(s):
	Delivery: mm ³ per stroke ¹⁾ at pump speed of min-1 ^{1), 3)} at full injection, or characteristic diagram ²⁾
	Quote the method used: on engine/on pump bench ²⁾
	Injection advance 1):
	Injection advance curve :
	Timing:
	Injection piping
	Length: mm
	Internal diameter:mm
	Injector(s)
	Make(s):
	Type(s):
	Opening pressure : kPa 1) or characteristic diagram 2)
	Governor
	Make(s):
	Type(s):
	Speed at which cut-off starts under full load:min-1
	Maximum no-load speed : min ⁻¹

¹⁾ Specify the tolerance.

²⁾ Delete where inapplicable.

³⁾ $1 \min^{-1} = 1 \text{ r/min}$

8.1.8 Other engine-driven equipment (Enumeration and brief description if necessary):
Characteristics or make(s) :
Generator/alternator ¹⁾
8.1.7 Electrical equipment
Drawing(s) or make(s) :
Oil cooler: with/without 1)
Percentage:
Mixture with fuel
Type :
Make ;
Circulating pump
Feed system (circulation by pump, injection inlet mixing with fuel, etc.) :
Position of lubricant reservoir:
Description of system :
8.1.6 Lubrication system
manufacturer, or indication of the maximum back-pressure at maximum power specified by the manufacturer 1):
Description of other parts of the exhaust equipment if the test is made with the complete exhaust equipment provided by the
Description of exhaust manifold :
8.1.5 Exhaust system
Reference and/or setting ranges 1)
Maximum lift of valves and angles of opening and closing in relation to dead centres :
8.1.4 Valve timing
Description:
Type(s):
Make(s) :
Cold-start system
Idling speed: min-1

¹⁾ Delete where inapplicable.

8.2 Spark-ignition engines — Essential characteristics 1)	
8.2.1 Description of engine	
Make :	
Type:	
Cycle: four-stroke/two-stroke ²⁾	
Bore:mm	
Stroke :	
Number of cylinders :	
Layout of cylinders :	Firing order:
Engine swept volume : litres	
Compression ratio 3):	
Cooling system	
a) Liquid	
Nature of liquid:	
Circulating pump: yes/no ²⁾	
Characteristics or make(s) :	Type(s):
Drive ratio:	
Thermostat: setting:	
Radiator: drawing(s) or make(s):	Type(s) :
Relief valve: pressure setting:	
Fan: characteristics or make(s):	Type(s) :
Fan drive system:	
Drive ratio:	
Fan cowl:	

¹⁾ In the case of non-conventional engines and systems, particulars equivalent to those referred to here shall be supplied by the manufacturer.

²⁾ Delete where inapplicable.

³⁾ Specify the tolerance.

b)	Air	
	Blower: characteristics or make(s) :	Type(s):
	Drive ratio :	
	Air ducting (standard production):	
	Temperature regulating system : yes/no 1)	
	Brief description :	
c)	Temperatures specified by the manufacturer	
	Liquid cooling	
	Maximum temperature at engine outlet:	κ
	Air cooling	
	Reference point (description) :	
	Maximum temperature at reference point:	κ
	Fuel temperature : min. :	max.: K
	Lubricant temperature: min.: K	max.: K
Press	sure charger: with/without1)	
Desci	ription of the system :	
Make	· · · · · · · · · · · · · · · · · · ·	Type :
Comp	pressor system : make :	Туре:
Charg	ge-air-cooling system : make :	Type:
Inlet	system	
Desci		, heating device, additional air inlets, etc.):
Inlet r	manifold:	Description:
Air fil		Type:
		Type:
	Additional anti-pollution devices (if any, and if not cover	
Desc	ription and diagrams :	
8.2.3	Fuel feed system	
Fuel	feed	
В	y carburettor(s) 1):	Number :

¹⁾ Delete where inapplicable.

Make :
Type:
Adjustments
Jets:
Venturis:
Float-chamber level:
Mass of float:
Float needle:
Manual/automatic choke 1)
Closure setting 2):
Feed pump
Pressure: kPa ²⁾ or characteristic diagram ¹⁾ :
By fuel injection 1)
Make(s):
Type(s):
Description (general):
Calibration: kPa ²⁾ or characteristic diagram ¹⁾ :
8.2.4 Valve timing
Maximum lift of valves and angles of opening and closing in relation to dead centres :
Reference and/or setting ranges 1):
8.2.5 Ignition systems
Ignition distributor
Knock sensor: yes/no ¹⁾
Strategy: retard only or advance/retard 1)
Make :
Type:
Ignition advance curve ²⁾ :
Ignition timing ²⁾ :
Contact-point gap ²⁾ and dwell-angle ¹⁾ :
Spark-plugs
Make:

¹⁾ Delete where inapplicable.

²⁾ Specify the tolerance.

Туре:
Spark-gap setting:
Ignition coil
Make :
Туре:
Ignition condenser
Make :
Туре:
Radio interference suppression equipment
Make :
Туре:
8.2.6 Exhaust system
Description and diagrams :
Description and diagrams
8.2.7 Lubrication system
Description of system
Position of lubricant reservoir:
Feed system (circulation by pump, injection into inlet, mixing with fuel, etc.):
Circulating pump 1)
Make:
Туре:
Mixture with fuel 1)
Percentage:
Oil cooler: with/without ¹⁾
Drawing(s) or make(s) :
8.2.8 Electrical equipment
Generator/alternator ¹⁾
Characteristics or make(s) :
8.2.9 Other auxiliaries fitted to engine (Enumeration and brief description if necessary):

¹⁾ Delete where inapplicable.

8.3 Test conditions for measuring engine net power
Trade-name or -mark of the engine :
Type and identification number of engine :
Test conditions
Pressures measured at maximum power:
Total barometric pressure : kPa
Water vapour pressure: kPa
Exhaust back-pressure: kPa
Location of exhaust back-pressure measurement point :
Inlet depression :
Absolute pressure in the inlet ductwork :
Temperatures measured at maximum power
a) of the inlet air :
b) at the engine intercooler outlet:
c) of the cooling fluid
— at the engine cooling fluid outlet: K
— at the reference point in the case of air cooling: K
d) of the lubricating oil :
at measurement point :
e) of the fuel
— at the carburettor inlet/fuel injection system inlet 1):
— in the fuel flow-measuring device :
Characteristics of the dynamometer
Make : Model : Model :
Туре:
Rating:
Characteristics of the opacimeter
Make : Model :
Type:
Fuel flow-measuring apparatus: gravimetric/volumetric1)

¹⁾ Delete where inapplicable.

Fuel

For spark-ignition engines operating on liquid fuel	
Make and type:	
Specification:	
Research Octane Number (RON):	64) ¹⁾
Motor Octane Number (MON):	63) ¹⁾
Percentage and type of oxygenates :	
Density:	75) ¹⁾
Lower calorific value, measured :	40) ²⁾
or lower calorific value, estimated:kJ/kg (in accordance with ASTM D 33	38) ²⁾
For spark-ignition engines operating on gaseous fuel	
Make:	
Specification:	· • • •
Storage pressure :	kPa
Utilization pressure :	kPa
Lower calorific value: k	J/kg
For compression-ignition engines operating on gaseous fuel	
Feed systems: gas:	.
Specification of gas used:	
Fuel oil/gas proportion:	.
Lower calorific value :	:J/kg
For compression-ignition engines operating on liquid fuel	
Make:	
Specification of fuel used:	
Cetane number: (in accordance with ISO 51	165) ^{1]}
Viscosity:mm²/s at 40 °C (in accordance with ISO 31	104) ¹
Density:	375) ¹
Lower calorific value, measured:kJ/kg (in accordance with ASTM D 2	240) ²⁾
or lower calorific value, estimated:kJ/kg (in accordance with ASTM D 33	338) ²

¹⁾ ASTM standards also exist.

²⁾ Delete where inapplicable.

_ubricant				
Make :				
Specification:				
SAE viscosity:				
3.4 Statement of results as function of engine speed 1)				
	····			
	ine speed, min ⁻¹			
Results			_	
Measured torque, N·m				
Measured power, kW				
Measured fuel flow ²⁾ , g/s		<u> </u>		
Measured smoke, m ⁻¹				
Barometric pressure, kPa				
Water vapour pressure, kPa				
Inlet air temperature, K				
	No. 1			
Power to be added for auxiliaries in excess of table (see 8.1.8 and 8.2.9), kW	No. 2			
	No. 3			
Power correction factor				
Corrected fuel flow ²⁾ , g/s				
Corrected brake power, kW (with/without ³⁾ fan or blower)				
Power of fan or blower, kW (to be subtracted if fan or blower is not fitted)				
Net power, kW				
Net torque, N·m				
Specific fuel consumption, g/(kW·h) ⁴⁾				
Smoke correction factor				
Corrected smoke, m ⁻¹				
Cooling liquid temperature at outlet, K				
Lubricating oil temperature at measuring point, K				
Air temperature after pressure-charger, K ³⁾		2 2 3 2 3 2 3 2 3 2 3 2 3 2 3 2 3 2 3 2		
Fuel temperature at injection pump inlet, K				
Air temperature after charge air cooler, K ³⁾				
Pressure after pressure-charger, kPa ³⁾	- 1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1			
Pressure after charge air cooler, kPa				
The characteristic curves of the net power and net torque, of the specific fuel ca function of the engine speed.	onsumption and of	the exhaust smoke va	lues shall be drawn as	
2) For spark-ignition engines, the corrected fuel flow is the measured fuel flow corrected fuel flow is added only for calculation purposes. For compression-ignition flow, except for constant power engines [see 6.3 c)].	v multiplied by the n engines, the corre	power correction fa acted fuel flow is equa	ictor. The concept of il to the measured fuel	
3) Delete where inapplicable.				

Calculated with corrected net power and corrected fuel flow.

9 Verification of engine performance

9.1 Designation

When the performance (power curves, torque and specific fuel consumption) of an engine are determined according to this International Standard, reference shall be made to the method used by stating "determined in accordance with ISO 1585".

9.2 Notation

9.2.1 Declared net power and corresponding engine speed (range)

The declared net power and corresponding engine speed (range) are that power and engine speed (range) which the manufacturer indicates in his sales literature for an engine type.

Qualify declared "net power and engine speed (range)" by the word "ISO".

EXAMPLE

ISO net power: kW at min⁻¹ (in accordance with ISO 1585).

9.2.2 Declared net torque and corresponding engine speed (range)

The declared net torque and corresponding engine speed (range) are that torque and corresponding engine speed (range) which the manufacturer indicates in his sales literature for an engine type.

Qualify declared "net torque and engine speed (range)" by the word "ISO".

EXAMPLE

9.2.3 Declared specific fuel consumption and corresponding engine speed (range)

The declared specific fuel consumption and the corresponding engine speed (range) are those specific fuel consumption and corresponding engine speed (range) which the manufacturer indicates in his sales literature for an engine type.

Qualify declared "specific fuel consumption and engine speed (range)" by the word "ISO".

EXAMPLE

ISO specific fuel consumption: $g/(kW \cdot h)$ at min^{-1} (in accordance with ISO 1585).

9.3 Tolerances

9.3.1 Declared values

9.3.1.1 Power

9.3.1.1.1 Declared single maximum power engine speed, n_p

At least at one engine speed which is in the range of $n_p \pm 2$ %, the corrected power shall be not less than (100 -a) % (see figure 2) of the declared power. 1)

At no engine speed shall the corrected power be more than (100 + a) % (see figure 2) of the declared power. 1), 2)

In no case shall the corrected power differ from the declared power at a given engine speed by more than d%.1

9.3.1.1.2 Declared maximum power engine speed range, $(n_{p_1}-n_{p_2})$

Within the engine speed range $(n_{p_1} + 2 \%)$ to $(n_{p_2} - 2 \%)$, the corrected power shall be not less than (100 - a) % (see figure 3) of the declared power. 1)

At no engine speed shall the corrected power be more than (100 + a) % (see figure 3) of the declared power. 1), 2)

In no case shall the corrected power differ from the declared power at a given engine speed by more than d%.1

9.3.1.2 Torque

9.3.1.2.1 Declared single maximum torque engine speed, n_T

At least at one speed, which is in the range of $n_T \pm 2$ %, the corrected torque shall be not less than (100 - b) % (see figure 4) of the declared maximum torque. 1)

At no engine speed shall the corrected torque be more than (100 + b) % (see figure 4) of the declared maximum torque. 1),3)

In no case shall the corrected torque differ from the declared torque at a given engine speed by more than d%.1

¹⁾ See 9.3.1.4.

²⁾ In normal cases near the declared maximum power engine speed, it is recommended that measurements be made in steps no smaller than 3 % of the declared maximum power engine speed or 3 % of the maximum engine speed, n_{p_2} , of the power range as appropriate.

³⁾ In normal cases near the declared maximum torque engine speed, it is recommended that measurements be made in steps no smaller than 3 % of the declared maximum torque engine speed or 3 % of the maximum engine speed, n_{T_2} , of the torque range as appropriate.

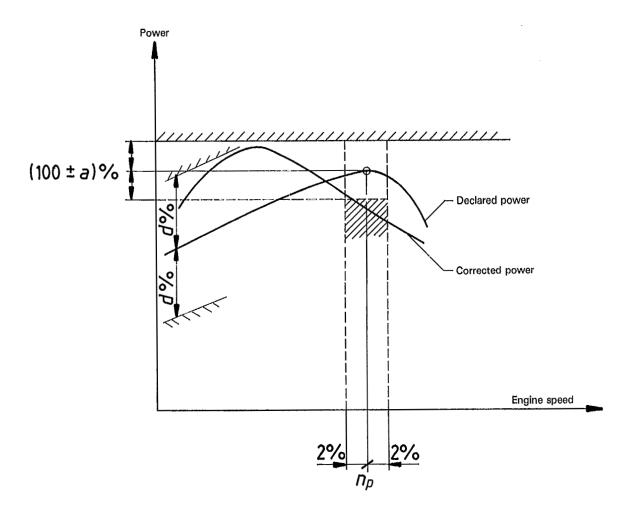


Figure 2 — Declared single engine speed maximum power graph

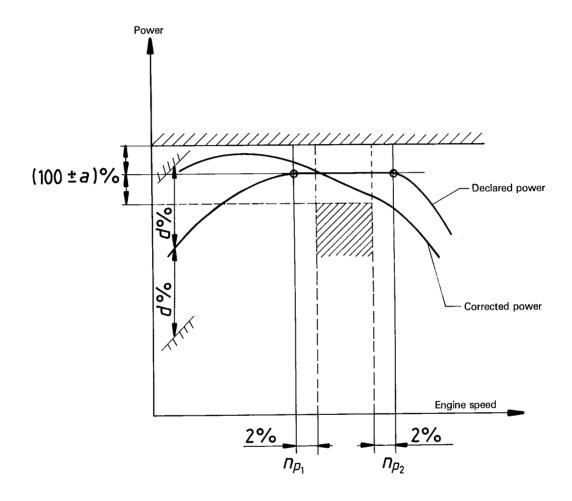


Figure 3 — Declared engine speed range maximum power graph

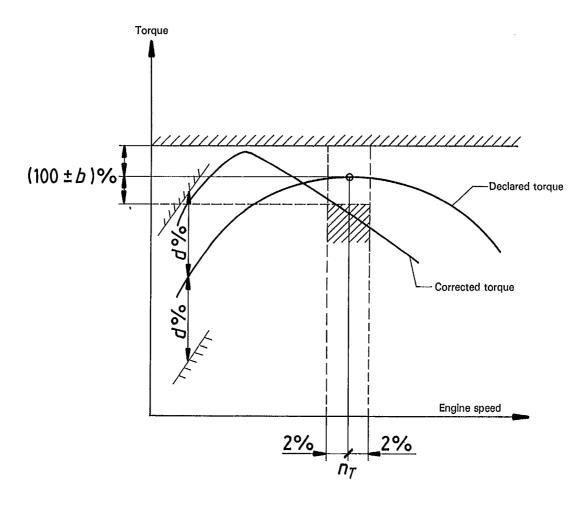


Figure 4 — Declared single engine speed maximum torque graph

9.3.1.2.2 Declared maximum torque engine speed range, ($n_{T_1} - n_{T_2}$)

Within the engine speed range $(n_{T_1}+2\%)$ to $(n_{T_2}-2\%)$ the corrected torque shall be not less than (100-b)% (see figure 5) of the declared maximum torque. 1)

At no engine speed shall the corrected torque be more than (100 + b) % (see figure 5) of the declared maximum torque. 1), 2)

In no case shall the corrected torque differ from the declared torque at a given engine speed by more than d%.1

9.3.1.3 Specific fuel consumption

A declared specific fuel consumption at a declared engine speed (range) is assumed to be verified, if the specific fuel consumption calculated during test is not more than c % greater than the declared specific fuel consumption. 1)

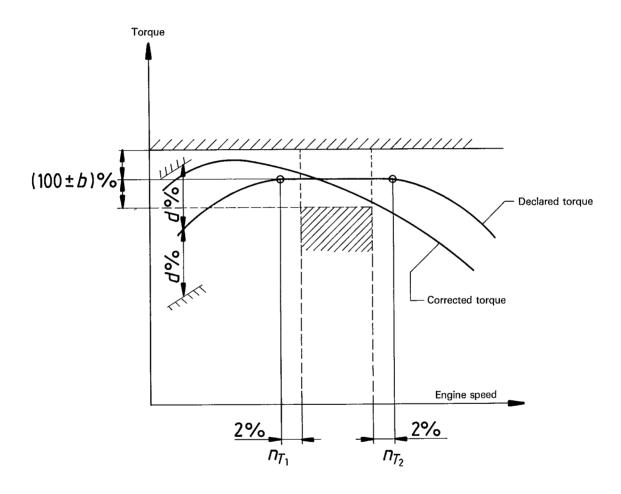


Figure 5 — Declared engine speed range maximum torque graph

¹⁾ See 9.3.1.4.

²⁾ In normal cases near the declared maximum torque engine speed, it is recommended that measurements be made in steps no smaller than 3 % of the declared maximum torque engine speed or 3 % of the maximum engine speed, n_{T_2} , of the torque range as appropriate.

9.3.1.4 Numerical tolerances

The numerical tolerances are given in table 3.

Table 3 — Numerical tolerances

	а	b	с	d
Verification of declared values	2 %	4 %	2 %	4 %
Production conformity tests 1)	5 %	6 %	4 %	6 %

¹⁾ For production conformity tests, the tolerance of compressionignition engine fuel temperatures may be relaxed to \pm 5 K.

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