

PD ISO/TS 17920:2015



BSI Standards Publication

Fibre ropes for offshore stationkeeping — Aramid

bsi.

...making excellence a habit.™

National foreword

This Published Document is the UK implementation of ISO/TS 17920:2015.

The UK participation in its preparation was entrusted to Technical Committee TCI/77, Ropes and cordage and fishing nets.

A list of organizations represented on this committee can be obtained on request to its secretary.

This publication does not purport to include all the necessary provisions of a contract. Users are responsible for its correct application.

© The British Standards Institution 2015. Published by BSI Standards Limited 2015

ISBN 978 0 580 78727 0

ICS 59.080.50

Compliance with a British Standard cannot confer immunity from legal obligations.

This Published Document was published under the authority of the Standards Policy and Strategy Committee on 31 August 2015.

Amendments issued since publication

Date	Text affected
------	---------------

TECHNICAL
SPECIFICATION

PD ISO/TS 17920:2015

ISO/TS
17920

First edition
2015-08-01

**Fibre ropes for offshore
stationkeeping — Aramid**

*Cordages en fibres pour le maintien en position des structures
marines — Aramide*



Reference number
ISO/TS 17920:2015(E)

© ISO 2015



COPYRIGHT PROTECTED DOCUMENT

© ISO 2015, Published in Switzerland

All rights reserved. Unless otherwise specified, no part of this publication may be reproduced or utilized otherwise in any form or by any means, electronic or mechanical, including photocopying, or posting on the internet or an intranet, without prior written permission. Permission can be requested from either ISO at the address below or ISO's member body in the country of the requester.

ISO copyright office
Ch. de Blandonnet 8 • CP 401
CH-1214 Vernier, Geneva, Switzerland
Tel. +41 22 749 01 11
Fax +41 22 749 09 47
copyright@iso.org
www.iso.org

Contents

Page

Foreword	v
1 Scope	1
2 Normative references	1
3 Terms and definitions	1
4 Materials	2
4.1 Rope core material.....	2
4.2 Rope cover material.....	2
4.3 Other materials.....	2
5 Requirements — Rope properties	2
5.1 Minimum breaking strength.....	2
5.2 Minimum core tenacity.....	3
5.3 Axial compression fatigue properties.....	3
5.4 Particle ingress protection.....	3
5.5 Cyclic loading performance.....	3
6 Requirements — Rope layout and construction	3
6.1 General.....	3
6.2 Type of construction.....	3
6.3 Rope core.....	3
6.4 Protective cover.....	4
6.5 Terminations.....	4
6.6 Length of rope.....	4
7 Rope testing	5
7.1 Type testing.....	5
7.1.1 General.....	5
7.1.2 Sampling.....	5
7.1.3 Breaking strength, core tenacity and stiffness tests.....	5
7.1.4 Axial compression fatigue properties test.....	6
7.1.5 Torque properties tests.....	6
7.1.6 Linear density test.....	6
7.1.7 Cyclic loading (endurance) test.....	6
7.1.8 Protective cover thickness.....	6
7.1.9 Particle ingress protection.....	6
7.2 Testing of current production.....	6
7.2.1 Sampling and testing.....	6
7.2.2 Length measurement.....	7
8 Report	7
8.1 Prototype rope.....	7
8.2 Current production.....	7
9 Certification	7
10 Marking, labelling, and packaging	8
10.1 Marking.....	8
10.2 Labelling.....	8
10.3 Packaging.....	8
Annex A (normative) Fibre qualification and testing	9
Annex B (normative) Rope testing	12
Annex C (normative) Axial compression fatigue properties test	21
Annex D (informative) Guidance for rope handling care	23
Annex E (informative) Certificate of conformity — Aramid ropes for offshore stationkeeping	34

Annex F (informative) Commentary	35
Bibliography	41

Foreword

ISO (the International Organization for Standardization) is a worldwide federation of national standards bodies (ISO member bodies). The work of preparing International Standards is normally carried out through ISO technical committees. Each member body interested in a subject for which a technical committee has been established has the right to be represented on that committee. International organizations, governmental and non-governmental, in liaison with ISO, also take part in the work. ISO collaborates closely with the International Electrotechnical Commission (IEC) on all matters of electrotechnical standardization.

The procedures used to develop this document and those intended for its further maintenance are described in the ISO/IEC Directives, Part 1. In particular the different approval criteria needed for the different types of ISO documents should be noted. This document was drafted in accordance with the editorial rules of the ISO/IEC Directives, Part 2 (see www.iso.org/directives).

Attention is drawn to the possibility that some of the elements of this document may be the subject of patent rights. ISO shall not be held responsible for identifying any or all such patent rights. Details of any patent rights identified during the development of the document will be in the Introduction and/or on the ISO list of patent declarations received (see www.iso.org/patents).

Any trade name used in this document is information given for the convenience of users and does not constitute an endorsement.

For an explanation on the meaning of ISO specific terms and expressions related to conformity assessment, as well as information about ISO's adherence to the WTO principles in the Technical Barriers to Trade (TBT) see the following URL: [Foreword - Supplementary information](#)

The committee responsible for this document is ISO/TC 38, *Textiles*.

Fibre ropes for offshore stationkeeping — Aramid

1 Scope

This Technical Specification specifies the main characteristics and test methods of new aramid fibre ropes used for offshore stationkeeping.

2 Normative references

The following documents, in whole or in part, are normatively referenced in this document and are indispensable for its application. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

ISO 139, *Textiles — Standard atmospheres for conditioning and testing*

ISO 1968, *Fibre ropes and cordage — Vocabulary*

ISO 2060, *Textiles — Yarn from packages — Determination of linear density (mass per unit length) by the skein method*

ISO 7500-1, *Metallic materials — Verification of static uniaxial testing machines — Part 1: Tension/compression testing machines — Verification and calibration of the force-measuring system*

ISO 18692, *Fibre ropes for offshore stationkeeping — Polyester*

ASTM D1907, *Test Method for Linear Density of Yarn (Yarn Number) by the Skein Method*

ASTM D1776, *Practice for Conditioning and Testing Textiles*

ASTM D6611, *Standard Test Method for wet and dry Yarn-on-Yarn Abrasion resistance*

ASTM D7269, *Test Methods for Tensile Testing of Aramid Yarns*

CI 1503, *Test method for yarn-on-yarn abrasion*

3 Terms and definitions

For the purposes of this document, the terms and definitions given in ISO 1968, ISO 18692, and the following apply.

3.1

aramid

long-chain synthetic polyamide in which at least 85% of the amide linkages are attached directly to two aromatic rings

[SOURCE: ISO 1968, 3.3.1, modified]

3.2

axial compression fatigue

failure mode for fibre rope such as *aramid* (3.1) under low tension or compression

4 Materials

4.1 Rope core material

The aramid fibre used in the core of the rope shall have an average tenacity of not less than 1,8 N/tex and in accordance with [Annex A](#). Qualification and testing requirements are given in [Annex A](#).

4.2 Rope cover material

Where polyester yarn is used in the protective cover, its minimum tenacity shall be 0,73 N/tex.

4.3 Other materials

Other materials employed in rope assembly shall be identified in the rope design/manufacturing specification.

For each material, the following shall be specified, as applicable:

- a) base material;
- b) size (linear density, mass per unit area, ...);
- c) relevant mechanical properties (tenacity, stiffness, ...).

5 Requirements — Rope properties

5.1 Minimum breaking strength

The minimum breaking strength (MBS) of the rope (spliced) when tested according to [Annex B](#) shall conform to [Table 1](#).

Table 1 — Minimum breaking strength (MBS)

Reference number ^a	Minimum breaking strength kN
80	2 500
90	3 100
100	3 900
106	4 400
112	5 000
118	5 600
125	6 300
132	7 000
140	7 800
150	8 700
160	10 000
170	11 200
180	12 500

^a The reference number corresponds to the approximate outer diameter of the rope, in millimetres (mm). Actual diameters may vary for a given reference number.

Table 1 (continued)

Reference number ^a	Minimum breaking strength kN
190	14 000
200	15 500
212	17 500
224	19 500
^a The reference number corresponds to the approximate outer diameter of the rope, in millimetres (mm). Actual diameters may vary for a given reference number.	

5.2 Minimum core tenacity

The minimum tenacity of the aramid rope core shall be 0,90 N/tex measured according to [Annex B](#). All samples tested shall comply with the minimum value specified herein.

5.3 Axial compression fatigue properties

The rope shall have demonstrated 95 % retention of MBS following the axial compression fatigue test method in [Annex C](#).

5.4 Particle ingress protection

If specified, the rope shall be constructed with a protection of the core against the ingress of particles having a size greater than 20 µm (microns) or as agreed between involved parties. Testing of the protection shall be performed in accordance with [Annex B](#).

5.5 Cyclic loading performance

The rope shall have demonstrated performance under cycling loading following the requirements of [7.1.7](#) and [B.5](#).

6 Requirements — Rope layout and construction

6.1 General

The typical section of a rope shall comprise a rope core providing intended strength and stiffness and a cover.

6.2 Type of construction

The rope shall be of one of the following types of construction:

- torque-neutral construction (type TF);
- torque-matched construction (type TM).

The type of rope shall be specified by the purchaser.

NOTE Torque-neutral ropes are intended for use in mooring systems together with chain or torque-neutral spiral strand wire ropes. Torque-matched ropes are intended for use in mooring systems together with six-strand wire ropes or other non torque-neutral wire ropes. Typical constructions are illustrated in [Figure F.3](#) and [Figure F.4](#).

6.3 Rope core

6.3.1 The total number of yarns in the rope shall be at least the number specified in the rope design specification.

6.3.2 Splices are not allowed in the rope core nor in sub-ropes except for those at the end terminations. Strands shall be uninterrupted over the length of the rope with no splice or strand interchange.

NOTE Yarns may be joined if necessary.

6.4 Protective cover

6.4.1 A protective cover shall be provided around the rope core to protect the rope core from mechanical damages during handling and in service.

The protection shall be water-permeable.

6.4.2 A polyester braided protective cover shall have a minimum thickness, t , with

- $t = 7,0$ mm, for a reference number RN above 100, and
- $t = 0,07 \times \text{RN}$, but not less than 4 mm, for a reference number RN less than 100.

Strand interchanges, i.e. the overlapping continuation of an interrupted strand with another identical strand following the same path, are permitted if they are properly staggered.

6.4.3 If an alternative protective cover is used, it shall demonstrate a level of protection equal to that of a polyester braided cover.

6.4.4 A braided cover shall include coloured strands forming a pattern so that rope twist during installation or in service can be identified. There shall be a minimum of one "S" coloured strand and one "Z" coloured strand to form a cross on the rope.

An alternative protective cover shall be fitted with an axial stripe of contrasting colour or other means to identify rope twist during installation or in service.

6.5 Terminations

The terminations shall be made of an eye splice plus abrasion protection materials.

NOTE There can be other terminations provided that they do not jeopardize the rope performance.

The dimensions and arrangement of the eye shall match the diameter and groove shape of the thimble (or other interface piece) to be used for end connections and shall be the same as for the rope prototype testing.

In the splice area, the integrity and the continuity of rope cover and particle-ingress protection, if fitted, shall be preserved or restored.

The eye and the splice area shall be further covered by an abrasion protection coating such as polyurethane. Each termination shall be made according to the manufacturing practice as described in the termination specification.

6.6 Length of rope

The bedded-in lengths of the rope sections shall be calculated in accordance with [7.2.2](#) under 20 % of MBS unless otherwise agreed on the purchase order or contract.

The calculated length of supplied rope shall be within ± 1 % of the specified length.

For each supplied rope, the actual length at the reeling tension or during manufacture shall be reported as an indicative value.

Adequate extra length shall be manufactured in order to prepare the samples for testing which are considered to be part of the delivery.

7 Rope testing

7.1 Type testing

7.1.1 General

Prototype tests shall demonstrate that ropes certified by the manufacturer as complying with the requirements laid down in this Technical Specification possess the properties specified in this Technical Specification. The purpose of these tests is to verify the design, material, and method of manufacture of each size of finished rope including protective cover and terminations.

All ropes to be prototype tested shall comply with all the other requirements laid down in this Technical Specification. The tests specified below shall be carried out on a prototype rope for each size of rope, unless otherwise noted in this Clause.

Any change in the design, material, method of manufacture, including protective cover and terminations which may lead to a modification of the properties as defined in [Clause 5](#), shall require that the prototype tests specified in this Technical Specification be carried out on the modified rope.

7.1.2 Sampling

The number of rope samples to be tested is given in [Table 2](#).

Table 2 — Number of samples for testing

Test	Number of samples
Breaking strength, core tenacity, and stiffness	3
Axial compression fatigue	1 ^a
Torque properties	1 ^b
Linear density	1
Cyclic loading endurance	1 ^c
^a See 7.1.4 . ^b See 7.1.5 . ^c See 7.1.7 .	

7.1.3 Breaking strength, core tenacity and stiffness tests

7.1.3.1 Three samples shall be tested according to the procedure specified in [Annex B](#) and each shall be capable of meeting the requirements of [5.1](#) (minimum breaking strength) and of [5.2](#) (minimum core tenacity).

7.1.3.2 The rope core tenacity and stiffness at the end of bedding-in shall be calculated according to the methods defined in [Annex B](#).

7.1.3.3 Measurement of the stiffness at other load levels shall be performed within the same tests.

These measurements are, however, not required when results are available for another qualified rope of the same design, material and method of manufacture with a reference number of not less than 90, and when the stiffness at end of bedding-in does not differ by more than 10 %.

NOTE 1 These measurements are performed for design purposes only. There are no acceptance criteria on these parameters.

NOTE 2 These measurements can also be performed on a separate rope sample (see [Annex B](#)).

7.1.4 Axial compression fatigue properties test

One sample shall be tested for axial compression fatigue properties.

This test need not be performed when data is available from the previous qualification test of another rope with the same design, material and method of manufacture of rope core, and a size not less than reference number 90.

7.1.5 Torque properties tests

Where applicable, torque properties tests shall be performed according to the procedure specified in ISO 18692. These tests are, however, not required when results are available for another qualified rope of the same design, material, method of manufacture, and termination with a reference number of not less than 90.

7.1.6 Linear density test

The linear density shall be calculated from the measured weight and elongation according to the method defined in [Annex B](#).

7.1.7 Cyclic loading (endurance) test

7.1.7.1 One sample shall be tested for cyclic loading. However, cyclic loading (endurance) tests performed with one size of qualified rope having the same design, material, and method of manufacture including protective cover and terminations is enough to qualify all sizes with an MBS between 50 % and 200 % of the size tested. The test for cyclic loading (endurance) is not required if such data is available.

7.1.7.2 The cyclic loading (endurance) test shall be performed according to the procedure specified in [B.5](#). A load range shall be selected by the manufacturer and the rope shall withstand, without breaking, at least the number of cycles for that load range as given in [Figure B.2](#).

The residual strength of the rope shall be at least 80 % of its MBF.

7.1.8 Protective cover thickness

The thickness of the protective cover shall be verified.

The thickness of a braided cover shall be measured as twice the thickness of cover strands under the maximum braiding tension.

7.1.9 Particle ingress protection

See [5.4](#) and [Annex B](#).

7.2 Testing of current production

7.2.1 Sampling and testing

When the ropes are already certified by the manufacturer as complying with the requirements laid down in this Technical Specification, the rope tests including breaking strength and core tenacity, as well as protective cover thickness verification, shall be performed on one sample taken from the manufacturing process for each type and size of rope.

7.2.2 Length measurement

The bedded-in length of each supplied rope section (other than short sections) shall be calculated from the linear density, ρ_l , by Formula (1):

$$L = \frac{(m_T - m_S) \cdot 1000}{\rho_{l,20}} \quad (1)$$

where

- L is the length of the rope in metres (m);
- m_T is the mass of the total rope length in kilograms (kg);
- m_S is the mass of the materials used to form the eyes and the splices in kilograms (kg);
- $\rho_{l,20}$ is the linear density of the rope, in ktex, obtained from the prototype test in accordance with [7.1.6](#).

The length of short rope sections (i.e. sections of less than 20 m) shall be measured at a load of 2 % of MBS as the length between the centres of termination fittings (i.e. same as L_u on [Figure B.1](#)).

8 Report

8.1 Prototype rope

A complete and detailed report of the prototype rope manufacturing shall be supplied including the fibre manufacturer, the fibre type and finish, and all rope characteristics that can influence the mechanical properties like design, material specifications, and method of manufacture, including protective cover and terminations, with sketches or pictures.

A complete and detailed report of type tests with sketches or pictures of the test set-up shall also be provided.

8.2 Current production

The manufacturing report of supplied ropes shall be provided. A complete and detailed report of rope tests with sketches and pictures of the test set-up shall also be provided.

9 Certification

The certificate of approval and control issued by an RCS (recognized classification society) shall be presented together with the ropes in order to ensure that testing and fabrication are in accordance with the approved specifications.

The rope manufacturer shall issue or obtain a rope certificate including at least the following information:

- a) reference number;
- b) type of construction;
- c) linear density;
- d) MBS;
- e) individual identification number;
- f) length at a specified load;
- g) length at the reeling handling tension.

NOTE A suggestion for a certificate of conformity can be found in [Annex E](#).

10 Marking, labelling, and packaging

10.1 Marking

A tape of at least 3 mm wide printed with a reference identifying the manufacturer shall be incorporated into the rope. The maximum distance between two consecutive markings shall be 0,5 m.

10.2 Labelling

An identification plaque or alternative means shall be installed close to the splice with the following information as a minimum:

- a) purchase identification;
- b) individual identification number;
- c) reference to this Technical Specification;
- d) type of construction (TF or TM) in accordance with [6.2](#);
- e) rope MBS;
- f) rope length at a specified load according to [7.2.2](#).

10.3 Packaging

If the assembly is packed on a spool or a reel, these shall be suitable for the applicable transportation means and of appropriate construction in terms of strength.

The packaging shall be marked with the manufacturer's trademark and with the lot identification number.

NOTE The ropes may be delivered in steel reels or in containers. Alternative packaging designs may be provided with the prior approval of the purchaser.

Annex A **(normative)**

Fibre qualification and testing

A.1 General

This Annex specifies the requirements for fibre qualification and testing.

A.2 Fibre specification

A.2.1 General information

A fibre specification shall include at least the information defined below:

- a) identification and general properties of fibre;
- b) detailed specification of physical and mechanical properties.

NOTE General properties of material can be found in the material safety data sheet.

A.2.2 Identification and general properties

The following information shall be provided in the fibre specification:

- a) producer of fibres;
- b) fibre designation;
- c) fibre material;
- d) number of filaments;
- e) nominal size (linear density);
- f) average tenacity;
- g) finish designation;
- h) finish content.

A.2.3 Physical and mechanical properties

The following information shall be provided in the fibre specification including tolerances on specified properties:

- a) linear density;
- b) dry breaking strength;
- c) dry elongation to break;
- d) dry elongation at a specified load level;
- e) effect of hydrolysis in seawater (reduction of strength with time).

These properties shall be documented by results of tests in accordance with [A.4](#).

A.3 Fibre test certificate

For each delivery, the fibre manufacturer shall issue a raw material certificate including at least the following information:

- a) fibre designation;
- b) merge number/batch identification;
- c) size (linear density);
- d) dry breaking strength;
- e) dry elongation to break;
- f) test result of finish level on fibre (see [A.4.2](#) below).

For acceptance testing, the above properties shall be obtained from testing on a representative number of samples taken from the delivery, not less than once every 5,000 kg.

For each property, the number of tests, the mean value, and the standard deviation or range shall be reported.

A.4 Fibre testing

A.4.1 Fibre linear density and strength

The fibre linear density shall be determined and recorded according to ASTM D1907 or ISO 2060.

The fibre strength and elongation shall be determined based on five specimen of basic yarn samples. The following samples shall be preconditioned according to ASTM D1776:

- 45 °C ± 5 °C and relative humidity of 15 % ± 5 % during 4 h.

Subsequently, conditioned according to ISO 139 or ASTM D1776:

- standard atmosphere 20 °C ± 2 °C and relative humidity 65 % ± 5 %;
- optional atmosphere 24 °C ± 2 °C and relative humidity 55 % ± 5 %.

The conditioning time shall be 14 h at least.

After conditioning, the specimen shall be loaded to break according to ASTM D7269. The average yarn breaking strength and elongation shall be calculated and recorded. The used test methods shall be documented with the results.

A.4.2 Yarn-on-yarn abrasion performance

A.4.2.1 Qualification testing (efficiency)

A.4.2.1.1 Qualification testing for efficiency of finish shall be performed on wet yarns. Tests shall be done in accordance with CI 1503 or ASTM D6611. The results shall be kept for reference.

NOTE The number or wraps used in the tests may be one.

A.4.2.1.2 Tests shall be performed at least at three load levels including one in each of the following ranges:

- a) 20 mN/tex to 30 mN/tex;
- b) 35 mN/tex to 45 mN/tex;

c) 55 mN/tex to 60 mN/tex.

A minimum of eight yarns shall be tested for each level.

A.4.2.1.3 The results at each load level shall be derived and reported in accordance with the procedure in CI 1503 or in ASTM D6611.

Based on these results, acceptance levels for further production tests shall be chosen by the fibre manufacturer.

A.4.2.2 Qualification testing (persistence)

The persistence of the marine finish in a marine environment shall be demonstrated.

The assessment method shall be duly documented by the fibre producer.

NOTE Yarn-on-yarn abrasion tests after artificial ageing may be used.

A.4.2.3 Testing of current production

The effectiveness of the application of the marine finish during fibre production shall be verified by yarn-on-yarn abrasion tests or another documented testing method.

When a yarn-on-yarn abrasion test is used, the testing shall be performed at least at one load level on a minimum of four yarns at each test with an acceptance level according to [A.4.2.1.3](#).

Any other testing method shall be duly documented by the fibre producer.

A.4.3 Hydrolysis properties of aramid fibres

The material shall have a residual strength of at least 90 % of its nominal value (new fibre) after immersion for three weeks in 80 °C seawater.

NOTE 1 Water can be either natural or artificial seawater (e.g. ASTM D1141) and can be used for testing.

NOTE 2 Accelerated test based on a factor 1 000 in time over a -60 °C increased temperature [e.g. see ISO 9080 to simulate the conditions of a mooring line (20 years in seawater at 4 °C to 20 °C)].

Annex B (normative)

Rope testing

B.1 General

This Annex specifies the requirements for full-size testing of rope samples and it addresses the following tests:

- a) strength and stiffness;
- b) linear density;
- c) cyclic loading endurance;
- d) particle ingress resistance.

NOTE 1 For the requirements for axial compression fatigue testing, see [Annex C](#).

NOTE 2 Requirements for testing of the torque properties whenever applicable can be found in ISO 18692:2007, B.6.

B.2 Testing conditions

B.2.1 Rope samples

The rope tests including strength, cyclic loading endurance, and torque measurement shall be performed on samples with terminations that are identical to the supplied ropes. The strength and cyclic loading tests shall be performed with fixed end conditions (without a swivel).

Termination fittings shall be provided with the same type of material and the same profile and dimensions (radius, groove shape) as the thimbles for the supplied rope.

B.2.2 Ambient conditions

In all tests, the ambient temperature and humidity shall be recorded.

The water used for soaking, wetting, and immersing shall be fresh water with no additives.

During the cyclic loading endurance test (see [B.5](#)), the rope shall be wetted by a water spray or immersed and the temperature shall be controlled in order to avoid over-heating.

The temperature of the out-flowing water should not exceed 30 °C.

B.2.3 Testing machine

The testing machine shall be of at least class 2 according to ISO 7500-1 and it shall be of such a type that load (or cross-head displacement) can be controlled at all time during both extension and retraction.

For the breaking test (step 10 in [B.3.1](#)), the use of a test machine with a fixed cross-head speed is acceptable provided that time to failure is at least 2 min.

B.2.4 Load and elongation measurements

Load shall be measured by a strain gauge system and continuously recorded during each test.

NOTE In the loading sequences specified below, loads are given as a percentage of the specified MBS of the rope.

The measurements of the gauge length elongation of the rope core shall be performed with a system of adequate sensitivity for the intended sequences taking into account the very small elongation of an aramid rope under such conditions. Extensometer or video image processing may be used.

The cover and the filter shall be cut for fastening of extensometer ends or for marking of core (in case of measurement by video image processing).

B.3 Strength and stiffness test

B.3.1 Test procedure

The following rope test procedure applies to verify the rope MBS, the minimum core specific strength, and the stiffness. The test shall be performed according to the steps below.

- Step 1: The sample shall be soaked for at least 4 h in fresh water.
- Step 2: The sample shall be installed in the test machine.
- Step 3: A load of 2 % of MBS shall be applied.
- Step 4: The rope shall be marked at each end at a distance of three times the rope diameter from the last tuck of splices (see [Figure B.1](#)).
- Step 5: The extensometer shall be installed in a section of the rope undisturbed by the termination between these marks.
- Step 6: A tension of 50 % of the rope MBS shall be applied at a rate of 10 % MBS per minute and held for 30 min.
- Step 7: The tension shall be reduced to 10 % of the rope MBS at a rate of 10 % MBS per minute.
- Step 8: A cycling tension between 10 % and 30 % of the rope MBS shall be applied 100 times, without interruption at a frequency between 0,03 Hz and 0,1 Hz (bedding-in and measurement of dynamic stiffness after bedding-in).
- Step 9: When applicable, a cycling tension between specified limits shall be applied for a specified number of cycles (dynamic or static stiffness measurements, see [B.3.5](#)) and without interruption, otherwise this step is omitted;
- Step 10: The sample shall be unloaded, the extensometer removed, and the rope pulled to failure at a loading rate of approximately 20 % MBS per minute.

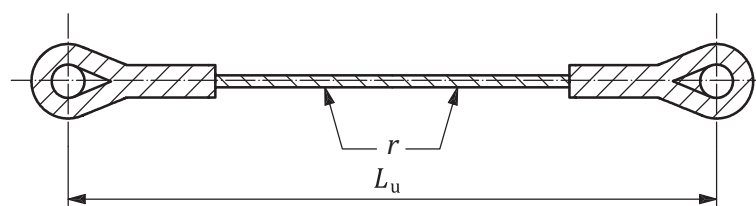


Figure B.1 — Marks “r” on the rope sample

B.3.2 Breaking strength

The tension at break of the rope sample shall be recorded.

All samples tested shall meet the MBS.

If the breaking load of one sample is lower than the MBS, two other samples shall be prepared and tested.

The rope is considered to comply with the breaking strength requirement in this Technical Specification only if the results of both the subsequent two tests meet the MBS.

B.3.3 Load-elongation measurements

The rope test shall include the measurement of the following:

- a) load versus total elongation (stroke), four plots as below:
 - 1) steps 5 to 7;
 - 2) step 8;
 - 3) step 9 (when performed);
 - 4) step 10;
- b) gauge length (extensometer) elongation (for the prototype rope), three plots as below:
 - 1) load versus elongation encompassing steps 5 to 7;
 - 2) load versus elongation for the last three full cycles at least in step 8;
 - 3) load versus elongation for the last three full cycles at least, in step 9 (when performed);
- c) continuous record of load and elongation versus time during the three cycles of the quasi-static stiffness measurement (when performed).

NOTE Step numbers refer to [B.3.1](#).

B.3.4 Dynamic stiffness at end of bedding-in

The dynamic stiffness at end of bedding-in (step 8 of [B.3.1](#)) shall be obtained from the load and gauge length elongation measurements and shall be calculated according to [B.3.6.2](#).

B.3.5 Quasi-static stiffness and dynamic stiffness

B.3.5.1 The quasi-static stiffness and the dynamic stiffness at other load levels shall be obtained from load and gauge length elongation measurements in step 9 in [B.3.1](#), and calculated according to [B.3.6.3](#) and [B.3.6.4](#).

NOTE Additional measurements of dynamic stiffness may be performed when agreed between the purchaser and the manufacturer (see [Annex F](#)).

B.3.5.2 For the measurement of the quasi-static stiffness, the following cycling shall be applied in three full cycles without interruption:

- a) slowly load the rope from 10 % of the rope MBS to 30 % of the rope MBS in a period of time between 2 min and 6 min;
- b) hold the load at 30 % of the rope MBS for 30 min from the start time of a) above;
- c) slowly unload the rope from 30 % of the rope MBS to 10 % of the rope MBS in a period of time between 2 min and 6 min;
- d) hold the load at 10 % of the rope MBS for 30 min from the start time of c) above.

This cycling shall be performed during step 9 of [B.3.1](#) above on one sample before the cycling for the dynamic stiffness.

NOTE Other load levels may be considered when agreed between involved parties (see [Annex F](#)).

B.3.5.3 For the measurement of the dynamic stiffness, the following cycling shall be applied during step 9 of [B.3.1](#) at a frequency between 0,03 Hz and 0,1 Hz:

- step 9a: On one sample: 100 cycles between 20 % and 30 % of the rope MBS;
- step 9b: On a second sample: 200 cycles between 30 % and 40 % of the rope MBS;
- step 9c: On a third sample: 300 cycles between 40 % and 50 % of the rope MBS.

In the case of an interruption within a set of cycling, this set of cycling shall be repeated.

If the interruption leads to unloading of the rope, the step 8 shall be performed again before re-running the interrupted set of cycling.

B.3.5.4 Alternatively to the above, measurements may be performed as follows.

- a) All measurements are performed on the same sample, quasi-static stiffness, then dynamic stiffness as steps 9a, 9b, and 9c (see [B.3.5.3](#)) in ascending order of load. Then, the cycling may be limited to 100 cycles at each level.
- b) These measurements are performed on a separate rope sample in either wet or dry condition according to the steps below:
 - 1) the sample shall be installed in test machine;
 - 2) steps 3 to 8 of [B.3.1](#) including measurement of the dynamic stiffness at the end of bedding-in;
 - 3) step 9 of [B.3.1](#) with cycling as per [B.3.5.2](#) for the measurement of the quasi-static stiffness;
 - 4) steps 9a, 9b, and 9c of [B.3.5.3](#) with cycling for the measurement of the dynamic stiffness.

B.3.6 Calculation of mechanical properties

B.3.6.1 Core tenacity

The rope core tenacity shall be calculated according to Formula (B.1):

$$t = \frac{F_{BS}}{\rho_{1,c0}} \quad (B.1)$$

where

- t is the rope core tenacity, expressed in newtons per tex (N/tex);
- F_{BS} is the actual breaking strength of the rope, expressed in newtons (N), obtained in step 10 of [B.3.1](#);
- $\rho_{1,c0}$ is the linear density of the rope core, expressed in tex at 2 % of MBS, as measured during the linear density test (see [B.4](#)).

B.3.6.2 Dynamic stiffness at end of bedding-in

The dynamic stiffness at end of bedding-in is calculated from the load-elongation measurement at the end of step 8 of [B.3.1](#).

The dynamic stiffness is calculated according to Formula (B.2):

$$K_{rb} = \frac{\frac{F_{30} - F_{10}}{L_{30} - L_{10}}}{\frac{F_{MBS}}{L_{10}}} \quad (\text{B.2})$$

where

K_{rb} is the dynamic stiffness after bedding-in;

$F_{30} - F_{10}$ is the recorded variation of load over the 100th cycle;

F_{MBS} is the specified minimum breaking strength of the rope;

$\frac{L_{30} - L_{10}}{L_{10}}$ is the elongation (strain variation) between F_{10} and F_{30} over the 100th cycle.

NOTE Alternatively, the stiffness can be obtained from the average slope of the load-elongation plot over the last three full cycles.

B.3.6.3 Dynamic stiffness

When required, the dynamic stiffness is calculated according to Formula (B.3) from load-elongation measurements of step 9a, 9b, or 9c of [B.3.5.3](#):

$$K_{rd,X \rightarrow Y} = \frac{\frac{F_Y - F_X}{L_Y - L_X}}{\frac{F_{MBS}}{L_X}} \quad (\text{B.3})$$

where

$K_{rd,X \rightarrow Y}$ is the dynamic stiffness under cycling between load X and Y;

$F_Y - F_X$ is the recorded variation of load over the last cycle;

$\frac{L_Y - L_X}{L_X}$ is the elongation between F_X and F_Y over the last cycle.

NOTE Alternatively, the stiffness can be obtained from the average slope of the load-elongation plot over the last three full cycles.

B.3.6.4 Quasi-static stiffness

When required, the quasi-static stiffness is calculated according to Formula (B.4) from load-elongation measurements:

$$K_{rs,X \rightarrow Y;1h} = \frac{\frac{F_Y - F_X}{L_Y - L_X}}{L_X} \quad (\text{B.4})$$

where

$K_{rs,X \rightarrow Y;1h}$ is the quasi-static stiffness under cycling between loads X and Y, over a period of 1 h;

$F_Y - F_X$ is the recorded variation of load over the last cycle;

$\frac{L_Y - L_X}{L_X}$ is the recorded elongation between F_X and F_Y over the last cycle.

NOTE 1 Alternatively, the quasi-static stiffness can be obtained by averaging the results over the last two cycles.

NOTE 2 The quasi-static stiffness for longer cycling periods can be obtained by extrapolation from the records of load and elongation versus time (see [Annex E](#)).

B.4 Linear density

B.4.1 Test procedure

The linear density is calculated from a dry sample of rope with at least 2 m free length (out of splice area as for marks "r" in [B.3.1](#)) taken from the manufacturing process according to the following procedure, unless otherwise agreed on purchase order or contract.

- a) The sample shall be installed in the test machine.
- b) A suitable fastening shall be provided in order to ensure no slippage between the cover and the core.
- c) The sample shall be submitted to a tension of 2 % of MBS and a length of about 2 m marked as a reference length, L_{R0} .
- d) The tension shall be increased to 20 % of the rope MBS at a rate of 10 % of MBS per minute.
- e) A cycling tension between 15 % and 25 % of the rope MBS shall be applied 100 times at a frequency between 0,03 Hz and 0,1 Hz.
- f) After cycling, the tension shall be maintained at 20 % of the rope MBS and the reference length, L_{R20} , shall be measured immediately after this tension is reached;
- g) The tension shall be lowered to 2 % of MBS and the reference length, L_{R2} , shall be measured again immediately after the 2 % tension is reached;
- h) After unloading, the sample shall be cut upon the reference length marks. The cut sections shall be flat and perpendicular to the rope longitudinal axis.
- i) The mass of the segment shall be measured and recorded.
- j) After removing the cover, the mass of the core segment shall also be measured and recorded.

NOTE The linear density includes the dry weight of the coating applied.

B.4.2 Calculation of linear densities

The linear densities shall be calculated according to Formula (B.5):

$$\rho_{1,0} = \frac{m_R}{L_{R0}} \quad \rho_{1,20} = \frac{m_R}{L_{R20}} \quad \rho_{1,2} = \frac{m_R}{L_{R2}} \quad \rho_{1,c0} = \frac{m_{RC}}{L_{R0}} \quad (\text{B.5})$$

where

$\rho_{1,0}$ is the linear density of the rope, expressed in ktex, as manufactured under 2 % of MBS;

$\rho_{1,20}$ is the linear density of the rope, expressed in ktex, after the rope has been cycled and under 20 % of MBS;

$\rho_{1,2}$ is the linear density of the rope, expressed in ktex, under 2 % of MBS after being mechanically worked to the above procedure;

$\rho_{1,c0}$ is the linear density of the rope core, expressed in ktex, as manufactured under 2 % of MBS;

m_R is the mass of the reference length, expressed in grams;

m_{RC} is the mass of the reference length of rope core, expressed in grams;

L_{R0} is the length of the reference length, expressed in metres, as manufactured under 2 % of MBS;

L_{R20} is the length of the reference length, expressed in metres, after the rope has been cycled and under a tension of 20 % of MBS;

L_{R2} is the length of the reference length, expressed in metres, under 2 % of MBS after being mechanically worked to the above procedure.

B.5 Cyclic loading endurance test

B.5.1 Planning

A load range, R , between 40 % and 50 % of MBS shall be selected by the manufacturer.

The corresponding minimum number of cycles shall be obtained from [Figure B.2](#).

The mean load, F_{mean} during test shall be such that the maximum load, F_{max} , is within 52 % and 55 % of MBS.

NOTE 1 The levels for cycling are then:

$$F_{\text{min}} = F_{\text{mean}} - \frac{R}{2}$$

and

$$F_{\text{max}} = F_{\text{mean}} + \frac{R}{2} \quad (\text{B.6})$$

NOTE 2 The number of cycles, N , in [Figure B.2](#) is given by Formula (B.7):

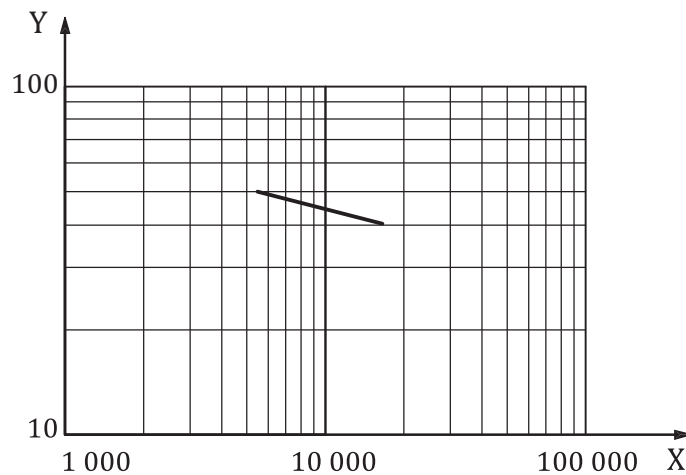
$$N.R^{5,05} = 166 \quad (B.7)$$

where

R is the load range divided by the MBS;

$N = 17\,000$ for $R = 0,4$;

$N = 5\,500$ for $R = 0,5$.



Key

X endurance (number of cycles), N

Y load range, R (% of MBS)

Figure B.2 — Minimum requirement for cyclic loading test

B.5.2 Test procedure

The cyclic loading test shall be performed as follows:

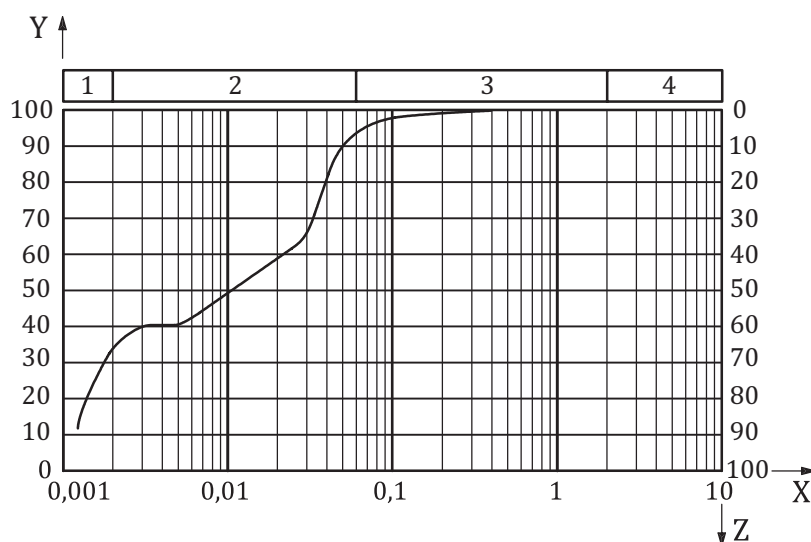
- a) the sample shall be soaked for at least 4 h in fresh water;
- b) the sample shall be installed in the test machine;
- c) a load of 2 % of the MBS shall be applied;
- d) a tension of 50 % of the rope MBS shall be applied at a rate of about 10 % of MBS per minute and held for 30 min;
- e) the tension shall be reduced to 30 % of the rope MBS at a rate of about 10 % of MBS per minute;
- f) cyclic loading between the selected levels F_{\min} and F_{\max} shall be applied for at least the specified number of cycles at a frequency between 0,01 Hz and 0,2 Hz (see [B.2.2](#));
- g) unload the sample and pull the rope to failure at a loading rate of approximately 20 % of MBS per minute.

The residual strength of the rope shall be at least 80 % of its MBF.

B.6 Particle ingress resistance

One sample shall be tested as follows:

- a) a specimen from a new rope with useful length of at least two times the rope diameter shall be selected;
- b) the specimen ends shall be sealed with a waterproof compound;
- c) the specimen shall be placed into a hyperbaric chamber and it shall be immersed in tap water with a sufficient volume to cover it. It shall be kept for 60 min at atmospheric pressure;
- d) an amount of soil shall be added at a proportion of 25 % of water weight.
- e) a pressure of 10 MPa shall be applied during a period of 72 h. During this period, the soil shall not be allowed to settle and it shall be kept suspended in water;
- f) after this period, the pressure shall be removed and the rope core shall be examined by a scanning electron microscope (SEM) to determine the efficiency of the filter in avoiding soil particle ingress with a size equal to, or greater than, the one stipulated.



Key

- 1 clay $\leq 2 \mu\text{m}$
- 2 silt $> 2 \mu\text{m}$ and $\leq 63 \mu\text{m}$
- 3 sand $> 63 \mu\text{m}$ and $\leq 2 \text{mm}$
- 4 gravel $> 2 \text{mm}$ and $\leq 63 \text{mm}$
- X particle size (mm)
- Y passing percentage (%)
- Z retained percentage (%)

Figure B.3 — Grading of soil for particle ingress resistance test

Annex C (normative)

Axial compression fatigue properties test

C.1 General

This Annex specifies the requirements for axial compression fatigue properties test of aramid ropes for offshore station keeping.

C.2 Testing conditions

C.2.1 Rope samples

The axial compression fatigue tests shall be performed on one sample of the full-size rope. Terminations of samples shall be identical to those used in supplied ropes.

Termination fittings shall be provided with the same type of material and the same profile and dimensions (radius, groove shape) as the thimbles for the supplied rope.

C.2.2 Ambient conditions

The axial compression fatigue test shall be performed under ambient conditions similar as those described for cyclic loading endurance test (see [B.2.2](#)).

C.2.3 Testing machine and measurement

The testing machine and the measurement system shall be in accordance with the provisions of [B.2.3](#) and [B.2.4](#). The machine shall be capable of accurately controlling the trough load at 1 % of MBS.

C.3 Testing

C.3.1 Test procedure

The axial compression fatigue test shall be performed according to the steps below:

- a) the sample shall be soaked for at least 4 h in fresh water
- b) the test piece shall be installed in the test machine;
- c) a load of 2 % of MBS shall be applied;
- d) the extensometer shall be installed in a section of the rope undisturbed by the termination;
- e) a tension of 50 % of the rope MBS shall be applied at a rate of 10 % MBS per minute and held for 30 min;
- f) the tension shall be reduced to 20 % of the rope MBS at a rate of 10 % MBS per minute;
- g) a cycling tension between 10 % and 30 % of the rope MBS shall be applied 300 times at a frequency between 0,03 and 0,1 Hz;
- h) a cycling tension between 1 % and 20 % of the rope MBS shall be applied 2 000 times at a frequency between 0,03 and 0,1 Hz;

- i) unload the sample and pull the rope to failure at a loading rate of approximately 20 % of MBS per minute.

C.3.2 Recorded data

The following data shall be recorded:

- type and length of the sample, linear density, and MBS;
- applied cyclic tension load;
- residual strength and as % of MBS.

Annex D (informative)

Guidance for rope handling care

NOTE Extracted from ISO 18692.

D.1 General considerations

Whenever fibre ropes for offshore stationkeeping are being handled, avoid the following:

- a) contact between rope and sharp edges (attention to vessel's drum area and stern roller);

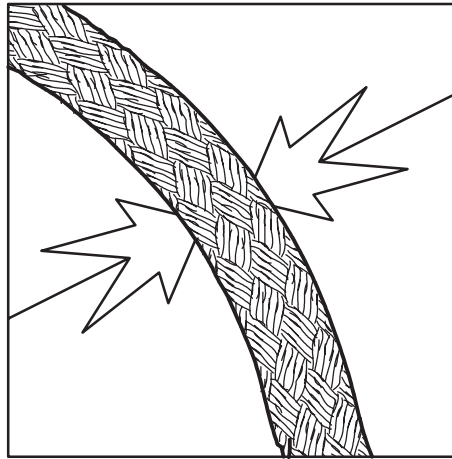


Figure D.1

- b) excessive abrasion between rope and rough surfaces (attention to vessel's deck and stern roller);

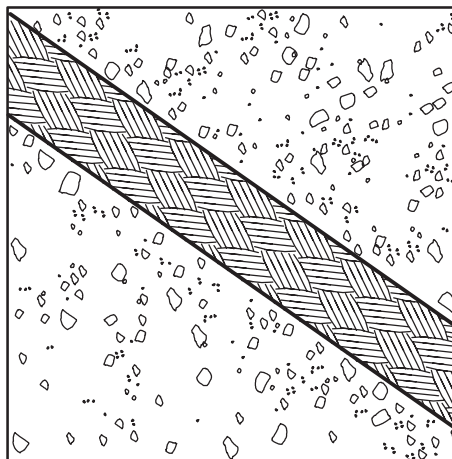


Figure D.2

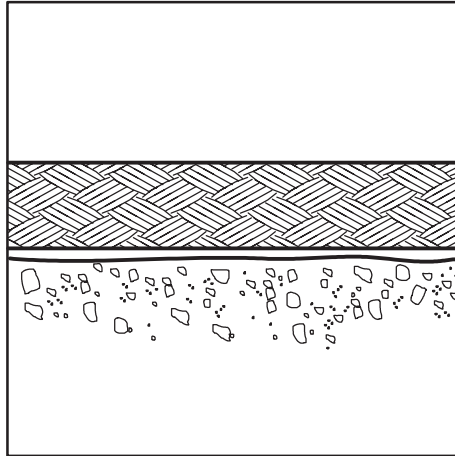


Figure D.3

c) working or handling with sharp tools (knives, blades, steel cables);

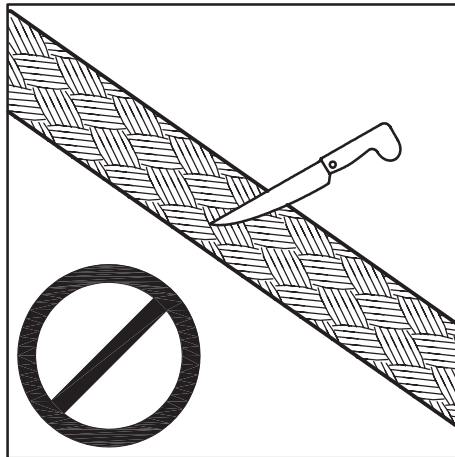


Figure D.4

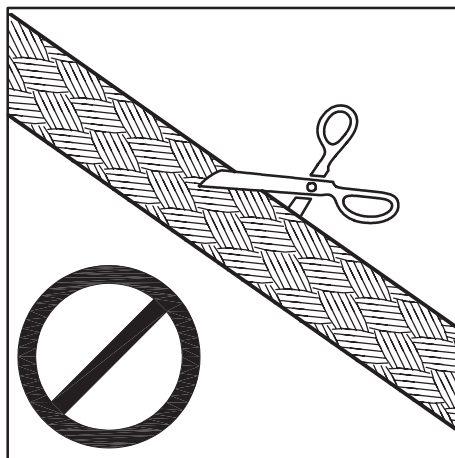


Figure D.5

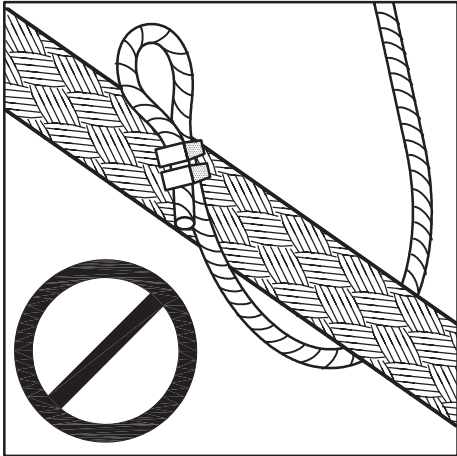


Figure D.6

d) excessive dirt in the rope and work area (oil, mud, scraps);

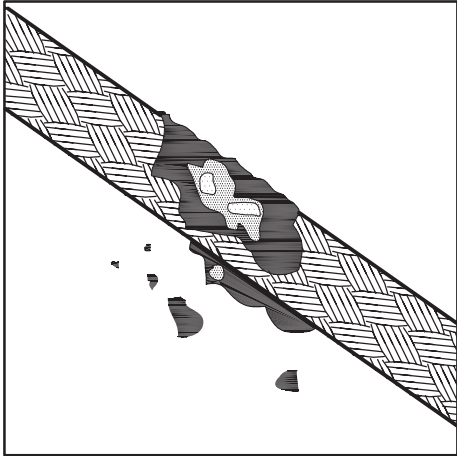


Figure D.7

e) excessive twist or bending in the rope;

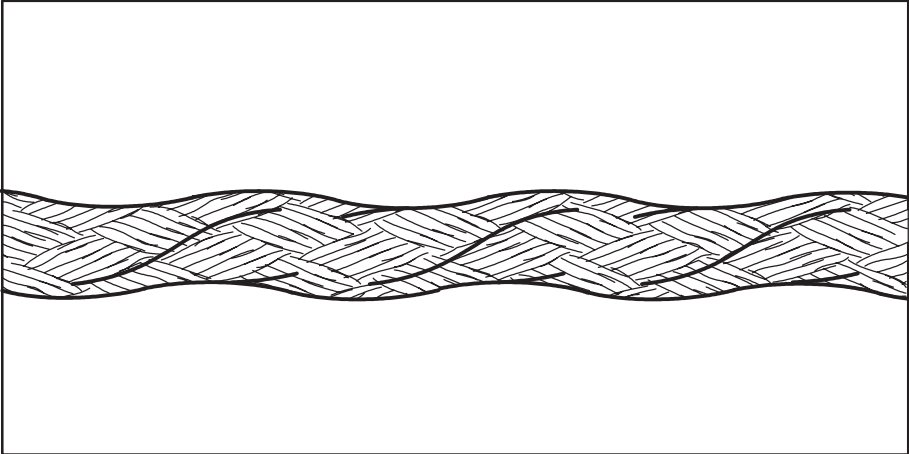


Figure D.8

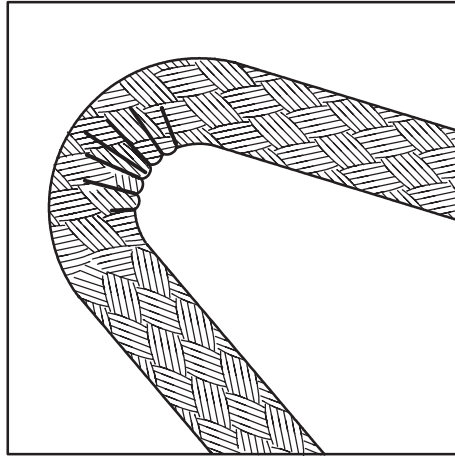


Figure D.9

f) contact with chemicals and prolonged exposure to sunlight.

D.2 Presentation of rope on reels

Fibre ropes for offshore stationkeeping will normally be supplied wound onto steel reels.

Protective packaging material will be wound around the main body of the rope to provide protection during transportation.

Packaging material should be carefully removed without cutting or damaging the rope. Strapping around the packaging may be under high tension and may snap back when cut, so extra care should be taken.

Insert segments will likely be provided in packing crates of considerable dimension. Crates may be handled with a forklift truck of suitable dimension and working load provided the fork positions enable safe lifting. Alternatively, the crates may be lifted by a slinging arrangement provided the slings are connected to the underside of the crate and are positioned to enable equal load distribution and safe lifting. Lifting slings which risk to damage the crate, thereby risking the segments packed inside are not permitted.

D.3 Reel lifting and handling

When using a crane, reels should be lifted using a specified lifting arrangement.

When lifting reels, the initial load application and final set-down should be conducted as slowly and softly as possible to prevent the imposition of undue acceleration and deceleration forces.

Reels should not be rolled on the floor when loaded with rope. When empty, reels should not be rolled unless it is absolutely essential and only on flat clear ground and where methods to fully control rolling are applied.

Reels should not be twisted or moved sideways while standing on the ground. Forklift trucks should not be used to lift reels in either the full or empty condition.

Where reel cradles are provided, the reel should not be disconnected from the cradle until just prior to installation into the rope spooling mechanism. The use of the cradle will prevent reel rolling, minimize instability, and ensure correct reel orientation when in storage.

D.4 Reel storage and maintenance

The ropes should be stored on reels on flat ground in reel cradles, where supplied, or else suitably chocked to prevent any unexpected movement. They should not be stacked on top of each other. The reels should be covered if stored outside to avoid prolonged exposure to sunlight, prevent plant growth

on the ropes, and to prevent abrasive particles from being deposited into the cover. These measures will ensure that the rope cover is maintained in as good a condition as possible.

Steel spools and other fittings should not be connected to the rope when stored on a reel to avoid chafing the rope cover.

D.5 Installation

D.5.1 Deployment overboard

- a) When a new rope is in contact with the vessel's deck and stern roller, spraying water directly on the rope will help to avoid damage caused by external abrasion and reduce rope internal abrasion between fibres.

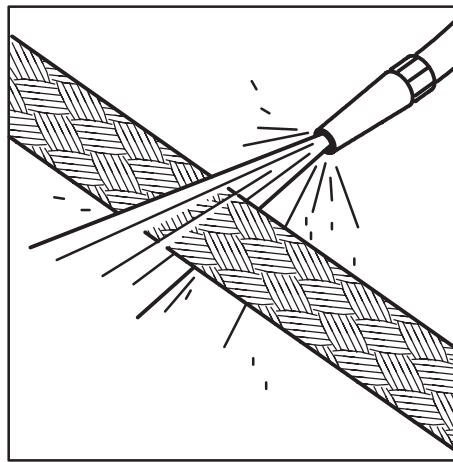


Figure D.10

- b) When installing the thimble, avoid excessive opening of the rope eye which can damage or crack the polyurethane coating.

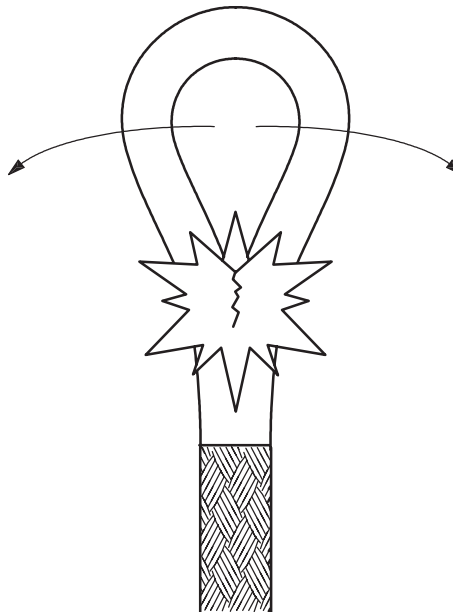


Figure D.11

- c) Avoid proximity with works involving fire, corrosive chemical products, or excessive heat. If unavoidable, protect the rope.

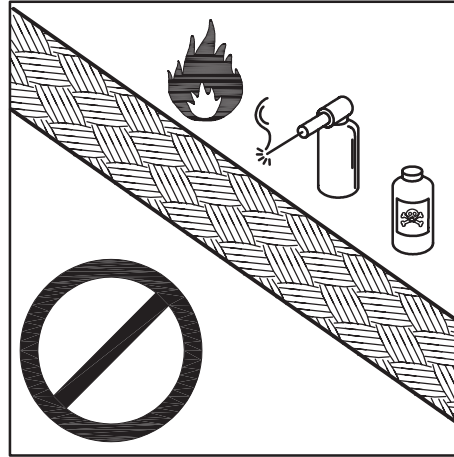


Figure D.12

- d) Avoid contact of the rope with the seabed.

D.5.2 Line tensions and re-reeling

The maximum line tension during deployment should be calculated and designed not to exceed 10 % of MBS. The deployment of heavy anchors and long lengths of chain may be required. It is recommended that the rope does not support the complete weight of these and they are either pre-deployed or a second line is used. In the latter case, care should be taken to avoid the second line causing damage to the rope both during the deployment and after disconnection. This second work line should ideally be a torque-balanced fibre rope.

The standard reels that ropes are normally transported on will not withstand line tensions over a few tonnes. It is recommended that the ropes be transferred to a winch drum on an anchor-handling vessel or to a purpose-built deployment reel. The lines can then be deployed directly from the winch or from the deployment reel through a dedicated deployment winch. Any temporary connection to the eye during re-reeling should be made using a fibre rope or webbing sling. The load in any connecting rope should be kept to a minimum to avoid cutting into the bearing point of the eye.

To reduce the chances of burying on a drum and possible damage caused to the cover by relative movement of the rope against the layer below, the deployment tension should be designed to be as low as possible. Applying tension during re-reeling onto a winch or storage drum will help avoid burying, along with a good traverse mechanism. As a guide, lines re-reeled at low tension and deployed with a line tension below 5 % of MBS do not experience problems with burying.

D.5.3 Equipment condition

All surfaces with which the rope will come into contact should be smooth and free from sharp edges. Relative movement between the rope and any equipment that it will contact during deployment should be avoided. Special care should be taken to avoid contact between the polyurethane eyes of the rope and metal parts such as winch frameworks.

D.5.4 Rollers and rope bending

Occasional bending and running over rollers is allowable during deployment. The rope should not be repeatedly cycled around rollers for prolonged periods of time. The rope should also not be left for prolonged periods around bends under dynamic loading conditions.

Drums, sheaves, and rollers should rotate freely.

The minimum storage D/d ratio is given by the barrel diameter of the transport reels. Insert lengths may utilize a lesser D/d ratio when packed in the original shipment.

D.5.5 Pre-tensioning and hook-up

In order to test the anchors and to remove initial constructional stretch from the tethers, a tensioning programme may be used. It may also be necessary to retension the lines from time to time during the early life of the mooring system and after its first storm loading in order to remove further constructional extension from the rope. Line tensions should continue to be monitored and retensioning should be completed when necessary.

When applying high tensions to the rope during deployment or hook-up, the rope and terminations should be clear of any bends or obstructions. The rope should be completely outboard of the deployment vessel and fully submerged in the seawater.

D.6 Identifying damage

D.6.1 Damage to the rope cover

Small external damages such as dirt and minor abrasion are very common. The objective of the rope cover and filter is to protect the inner cores. The cover and filter are not considered for calculations of rope performance regarding, for example, breaking strength and stiffness.

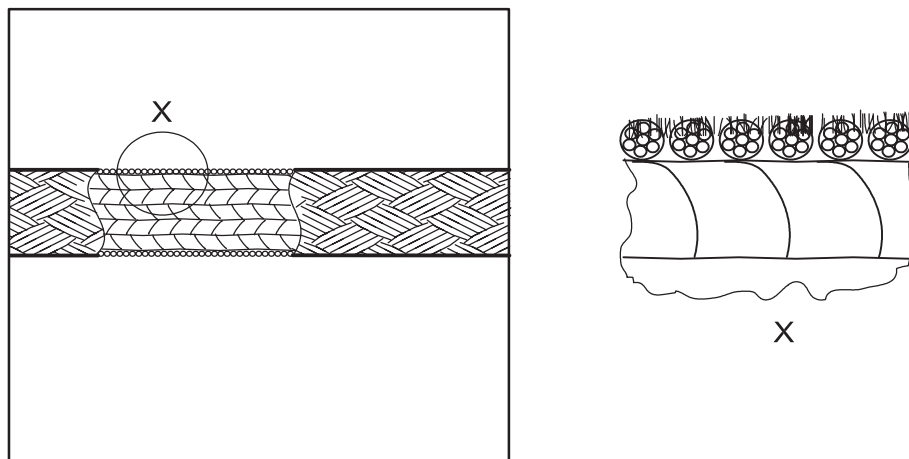


Figure D.13

External damages can be visually identified as the following.

- a) Excess dirt which does not represent major damage. The objective of the cover is to protect the rope cores. In this case, wash the area with fresh water.

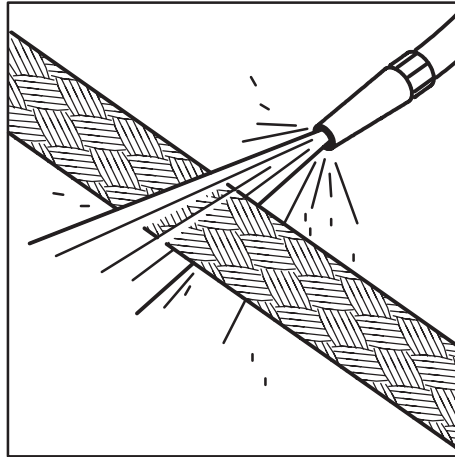


Figure D.14

- b) Cuts in the rope cover exposing the cores. In this case, if the exposed area of the core does not show any signs of cuts or dirt, cover the area with small diameter cords in a spiral array and secure them with reinforced adhesive tape, otherwise the rope should be rejected.

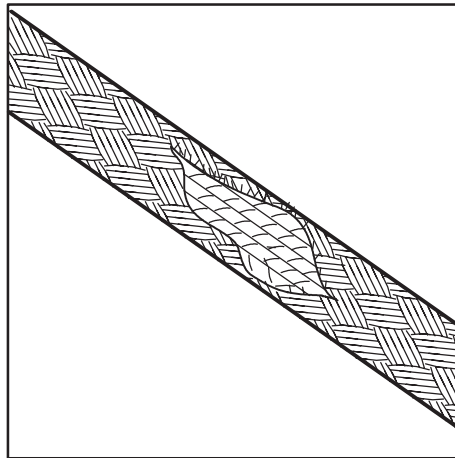


Figure D.15

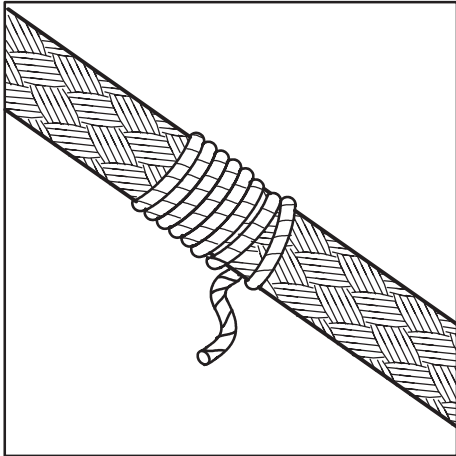


Figure D.16

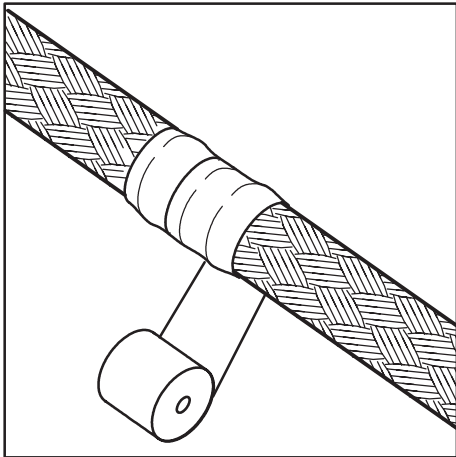


Figure D.17

c) Threadbare cover caused by abrasion without a cut. In this case, cover the area with reinforced adhesive tape.

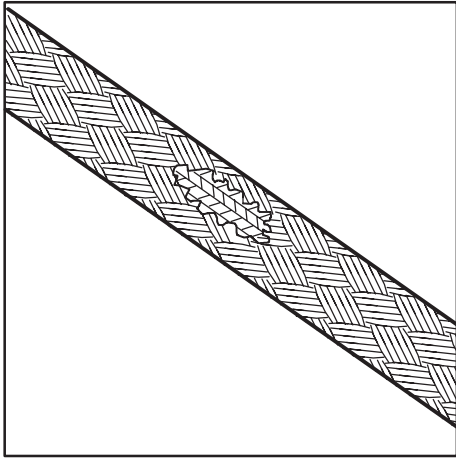


Figure D.18

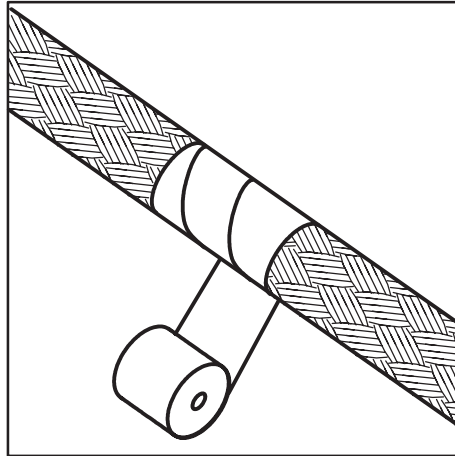


Figure D.19

D.6.2 Damage to the rope core

Ropes with damaged cores should be rejected.

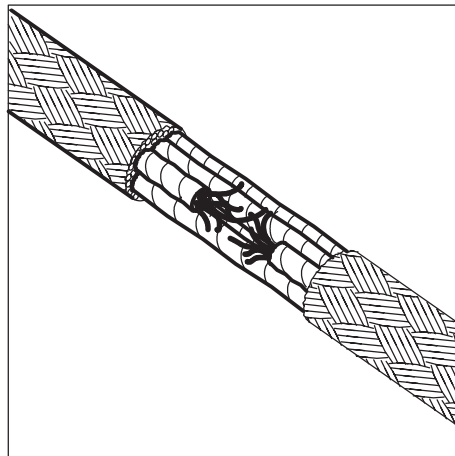


Figure D.20

It should be noted that only major internal damage can be identified visually. Excessive nonlinearity in the rope surface may represent internal damage.

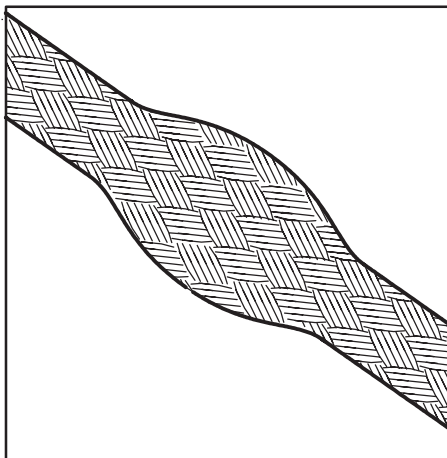


Figure D.21

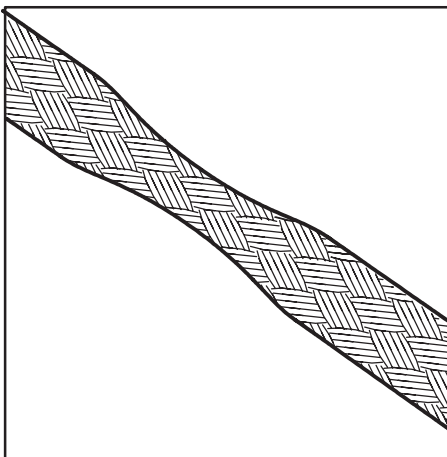


Figure D.22

Annex E (informative)

Certificate of conformity — Aramid ropes for offshore stationkeeping

Certificate number: _____

Purchaser		
Purchaser order number	:	
Production order	:	
ROPE IDENTIFICATION		
Designation	:	
Reference document	:	ISO/TS 17920
Core material	:	Aramid
Cover material	:	
Reference number	:	
Type of construction	:	Torque-neutral (type TF) – Torque-matched (type TM)*
Linear density (ktex)	:	
Minimum breaking strength (kN)	:	
RCS/Type approval certificate number	:	
	:	

*specify

Item	Rope individual identification number	Nominal length (at ...% of MBS) (m)	Actual length (at ...% of MBS) (m)	Rope length at reeling handling tension (m)	Rope net mass (kg)**	Packaging number
1						
2						
3						
...						

**including termination and fitting

Place:

Date:

Quality Control Supervisor

Annex F (informative)

Commentary

F.1 General

Reference is made to the corresponding clauses of this Technical Specification and its annexes.

F.2 [Clause 1](#) — Scope

This Technical Specification covers aramid fibre ropes intended for use as components of anchoring lines forming the stationkeeping system of permanent or mobile offshore floating structures or for use in a similar application.

The design of stationkeeping systems of offshore floating structures and the criteria for the application of fibre ropes in such systems are covered in ISO 19901-7.

In such systems, fibre ropes are typically permanently immersed and freely spanning between end terminations. Contact with the seabed is avoided and can normally happen only in an accidental situation (e.g. during the handling of lines for installation).

In this Technical Specification for aramid ropes and in the present commentary, reference is made to ISO 18692.

F.3 [5.3](#) — Axial compression fatigue properties

F.3.1 Axial compression fatigue of aramid fibres

The main characteristics of aramid fibre that make it attractive for mooring applications are its high strength, high modulus, and low creep properties. However, compared to PET fibres, aramid fibre is more susceptible to damage from axial compression fatigue. In a rope, this effect will appear when subjected to tension-tension cycles in the low load range. This susceptibility contributed to the premature failure of the first aramid fibre mooring rope deployed in 1983 (see Reference [\[15\]](#) and Reference [\[14\]](#)). However, in the same period, aramid fibre ropes were successfully used (see Reference [\[13\]](#)) indicating that the actual risk from compression fatigue on a rope level depends on the actual rope design and handling.

Studies and design improvements to address axial compression fatigue issues had resulted in several successful trials or use of aramid fibre mooring rope (see References [\[9\]](#), [\[10\]](#), and [\[12\]](#)). Care should be taken to properly design and test aramid fibre ropes for axial compression fatigue performance in order to ensure endurance of the rope in station keeping use.

F.3.2 Technical considerations

To avoid failures due to improper design of a rope, it is important to understand and distinguish the factors that play a role in causing compression fatigue. Compression fatigue should be separated in the following effects:

- a) tension-tension fatigue due to cycling at low loads;

Cycling at low loads in general gives more damage to materials than cycling the same range at a higher load. With aramids, this effect is more explicit than with, e.g. PET, but the principle is similar. The cause

of this fatigue effect is partly from the fact that aramids are less abrasion-resistant. During the low load cycling, the movement in a rope is relatively high causing abrasion.

b) compression of filaments due to length differences, e.g. in the splice area.

When aramid filaments are compressed for more than a 0,5 % strain (up to 1 %), a weak spot will be created which is generally referred to as a kink-band. The effect of such kink-band with regards to the strength of the filament is only significant when the fibre is repetitively compressed more than 0,5 % for at least several hundreds of cycles. When the fibre is subjected to 0,5 % or less compressive strain, studies have showed that no strength loss is found even after several hundred thousands of cycles (see Reference [14]).

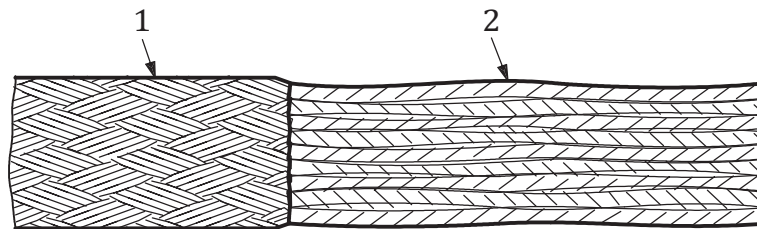
Especially when filaments are locked into their position, this effect will appear. This affects the splice area (and ropes with large length differences within the rope also causing low strength efficiency).

The risk from the axial compression fatigue can be minimized by the following methods:

- a) improve rope design to minimize local compression especially in the splice areas;
- b) establish proper rope minimum tension criteria and analysis procedure;
- c) conduct rope axial compression fatigue test to demonstrate adequate resistance to failure.

F.4 6.2 — Type of construction

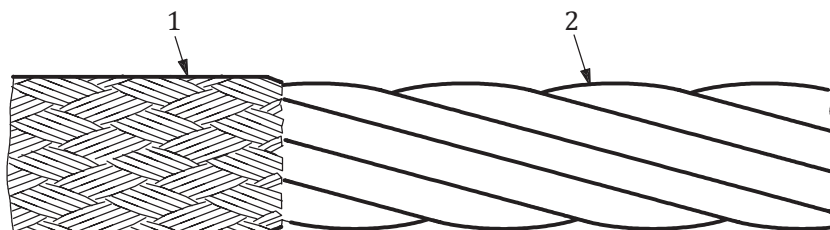
Typical constructions of ropes are illustrated in [Figure F.1](#) and [Figure F.2](#).



Key

- 1 cover
- 2 sub-ropes

Figure F.1 — Typical torque-neutral parallel construction rope with cover and sub-ropes (type TF)



Key

- 1 cover
- 2 rope core

Figure F.2 — Typical torque-matched wire rope construction rope with cover (type TM)

Depending on the rope construction, the rope may be torque-neutral or designed to accommodate a given torque (torque-matched construction). Torque-matched fibre ropes are intended for use in series with wire ropes. These constructions are specifically designed to reduce torsional fatigue in the wire rope.

F.5 [6.6](#) — Length of rope

The length of rope is defined as the installed length at a typical mean tension as simulated by the loading and the bedding-in sequence of the typical elongation and linear density test defined in [B.4](#) (see [F.10](#)).

F.6 [7.1.3](#) and [B.3.2](#) — Breaking strength

The purpose of the test is to verify the breaking strength of the rope against the specified MBS. The testing of three samples provides a margin that is quantifiable. Adjusting the breaking strength upward or downward from the test results is not to be considered.

The test sequence includes an initial loading and a bedding-in sequence. Further, load-elongation measurements that may be performed in between are not deemed to affect significantly the condition of the rope with respect to the break test.

F.7 [7.1.3](#) and [B.3](#) — Dynamic stiffness at end of bedding-in and quasi-static stiffness

The load-elongation properties of fibre ropes under cyclic loading have been investigated in several research and development projects and models have been proposed to quantify the dependence of stiffness on testing parameters (see, e.g. Reference [\[11\]](#)).

Depending on the construction particulars, a rope of a given strength could exhibit a wide range of stiffness under given conditions. The dynamic stiffness at the end of the standard bedding-in sequence has been found to provide a pertinent indication of the degree of stiffness of a given rope. Then, only a limited amount of testing performed on one rope size only is necessary to verify the rope behaviour and adjust models if needed (see [F.10](#)).

F.8 [7.1.4](#) and [C.3](#) — Axial compression fatigue test

The test conditions specified in [C.3.1](#) are intended to demonstrate adequate performance of the rope for service conditions with a minimum tension of 2 % of MBS in the leeward lines at any time during operation (design environmental conditions) and during installation (prelaid buoyed line).

F.9 [7.1.6](#) and [B.5](#) — Cyclic loading endurance test

The endurance of polyester ropes at moderate load ranges typical of mooring system response has been quantified by systematic cyclic loading tests on small size ropes (see ISO 18692:2007, E.7) and found far above that of a steel wire rope.

For aramid ropes, only very limited data are available indicating, however, that the endurance of aramid ropes with adequate finish and proper manufacture may be expected to be in the same order as that of (spiral strand) steel wire ropes provided that axial compression fatigue (see [F.3](#)) is avoided.

The purpose of cyclic loading endurance testing in [B.5](#) is therefore to evidence that a particular rope has the expected endurance and also does not present risks of premature failure due to inadequate design or manufacturing.

F.10 7.2.2 and B.4.2 — Length measurement and calculation of linear densities

The objective of the linear density test is to provide data to determine/verify the as-installed length of supplied rope segments. For this purpose, the linear density of the rope after a typical installation sequence is determined.

Other methods of measuring the length of a rope could be used in conjunction with the method specified in this Technical Specification, but would require a suitable calibration to ensure an accuracy that is consistent with specified length tolerances.

F.11 B.3.5 — Quasi-static stiffness and dynamic stiffness

The axial stiffness of a rope is defined in this Technical Specification as the ratio of rope load to strain variations between the lower (trough) and upper (peak) stresses imposed during testing normalized by the rope minimum breaking strength.

$$Kr = [\Delta F / MBS] / (\Delta\lambda / \lambda) \tag{F.1}$$

The reduced stiffness, *Kr*, is dimensionless (%/%).

For further background, see ISO 18692:2007, E.9.

The quasi-static stiffness, i.e. the stiffness under quasi-static cycling, is defined as a secant stiffness between the end points of successive half-cycles. The results of a 1 h cycling can be extrapolated to more representative durations, e.g. 24 h or 7 d as noted in Reference [11]. For the longer durations, the effect of rope creep over such duration (averaged over *in situ* rope length) should be accounted for, in addition.

The dynamic stiffness is representative of the near-linear behaviour observed under cycling at frequencies that are typical of vessel slow drift motions and wave actions. A load range smaller than 10 % would be desirable in some cases, but may lead to difficulties in the measurement of small elongations.

F.12 5.4 and 7.1.9 — Particle ingress protection

The intent of the particle ingress protection is to prevent risks of damaging the rope core in the case of accidental contacts with the seabed (see ISO 19901-7).

F.13 B.3 to B.5

Testing sequences specified in B.3 to B.5 are shown for illustration in Figure F.3 to Figure F.7.

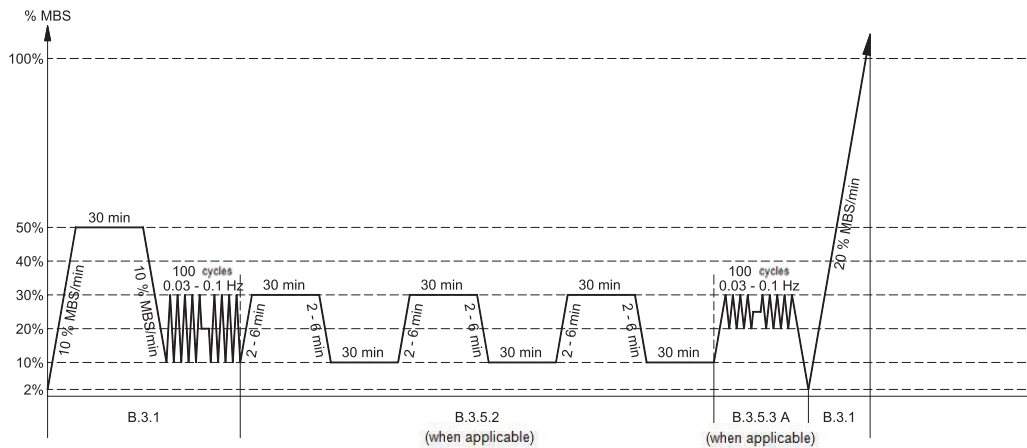


Figure F.3 — Quasi-static stiffness, dynamic stiffness, and breaking test sequence, B.3, sample a

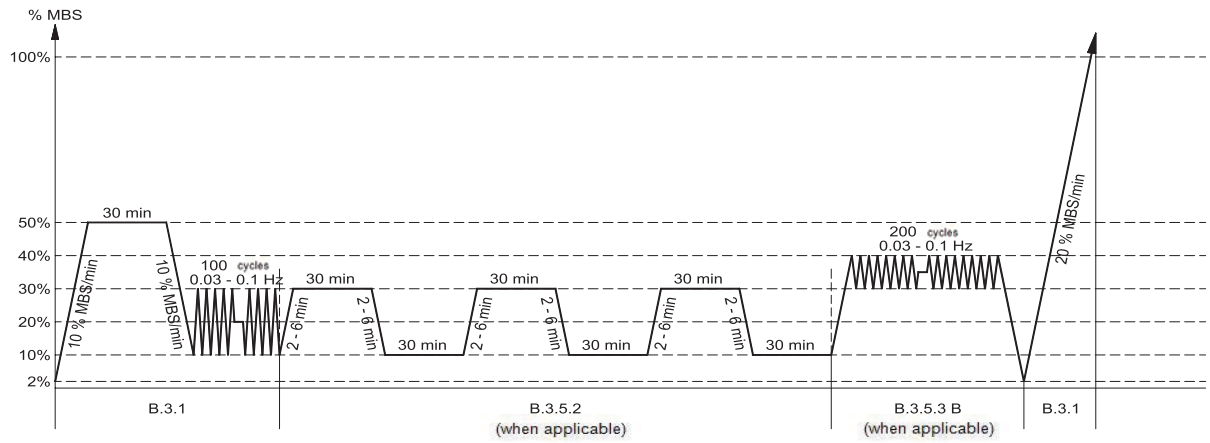


Figure F.4 — Quasi-static stiffness, dynamic stiffness, and breaking test sequence, [B.3](#), sample b

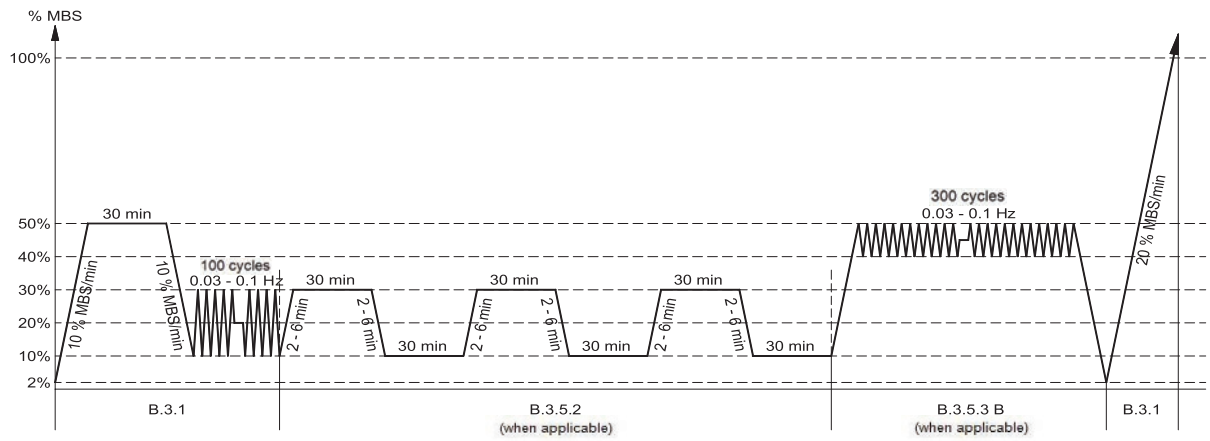
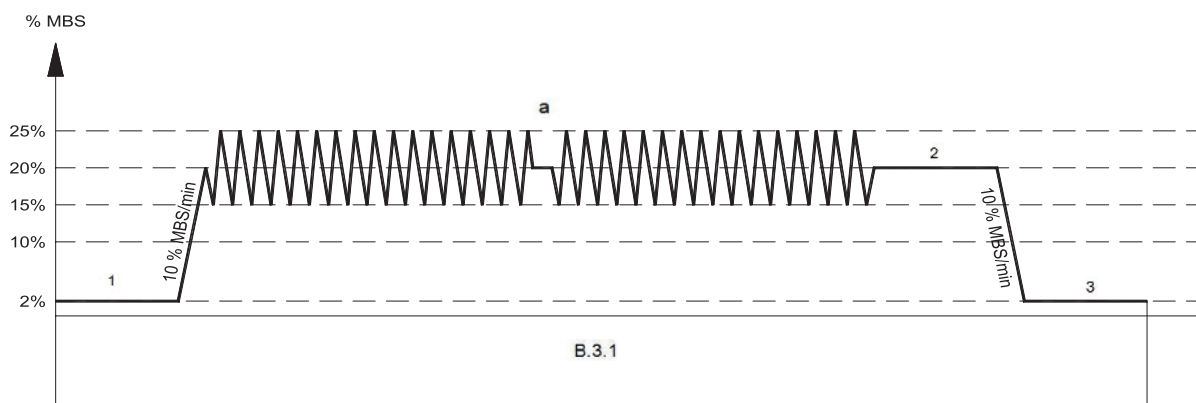


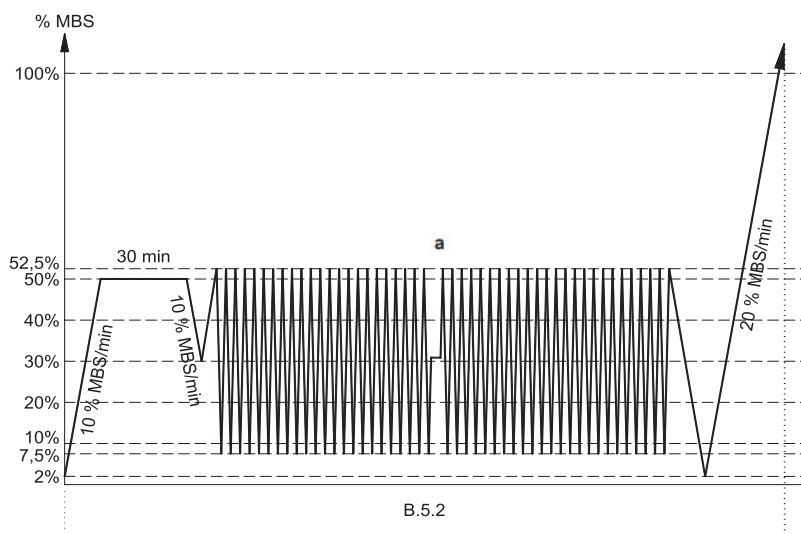
Figure F.5 — Quasi-static stiffness, dynamic stiffness, and breaking test sequence, [B.3](#), sample c



Key

- 1 mark 1, L_{R0} (2 m)
- 2 mark 2, L_{R20}
- 3 mark 3, L_{R2}
- a 100 cycles; between 0,03 Hz and 0,1 Hz.

Figure F.6 — Linear density test sequence, [B.4](#)



Key

- a 9 362 cycles; between 0,01 Hz and 0,1 Hz.

Figure F.7 — Cyclic loading endurance test sequence, [B.5](#) (example with a cycling range, R , of 45 %)

Bibliography

- [1] ISO 2062, *Textiles — Yarns from packages — Determination of single-end breaking force and elongation at break using constant rate of extension (CRE) tester*
- [2] ISO 9080, *Plastics piping and ducting systems — Determination of the long-term hydrostatic strength of thermoplastics materials in pipe form by extrapolation*
- [3] ISO 9554, *Fibre ropes — General specifications*
- [4] ISO 19901-7, *Petroleum and natural gas industries — Specific requirements for offshore structures — Part 7: Stationkeeping systems for floating offshore structures and mobile offshore units*
- [5] ISO/TS 14909, *Fibre ropes for offshore stationkeeping — High modulus polyethylene (HMPE)*
- [6] ASTM D1141, *Standard Practice for the Preparation of Substitute Ocean Water*
- [7] ASTM D2256, *Test Method for Tensile Properties of Yarns by the Single-Strand Method*
- [8] ASTM D885, *Test Methods for Tire Cords, Tire Cord Fabrics, and Industrial Filament Yarns Made from Manufactured Organic-Base Fibers*
- [9] ASSAYAG M.I., & CASTRO G. Minami, K., Assayag, S., Campos Basin: A Real Scale Lab for Deepwater Technology Development, OTC 8492, 1997
- [10] CHI C.H., LUNDHILD E.M., VESELIS T., HUNTLEY M.B. Enabling ultra-deepwater mooring with aramid fiber rope technology, OTC 20074, 2009
- [11] FRANÇOIS M., DAVIES P., Grosjean F., Legerstee F.: Modelling Fiber Rope load elongation properties - Polyester and other fibers, OTC 20846, 2010
- [12] KORALEK A.S., & BARDEN D.K. Performance of a Lightweight Aramid Mooring Line, OTC 5381, 1987
- [13] MCKENNA H.A., HEARLE J.W.S., O'HEAR N. Handbook of fibre rope technology. Woodhead Publishing, Cambridge, England, 2004, pp. 366.
- [14] RIEWALD P.G. Performance Analysis of an Aramid Mooring Line, OTC 5187, 1986
- [15] RIEWALD P.G., WALDEN R.G., WHITEHILL A.S., KORALEK A.S. Design and Deployment Parameters Affecting the Survivability of Stranded Aramid Fiber Ropes in the Marine Industry. IEEE Oceans, 1986

British Standards Institution (BSI)

BSI is the national body responsible for preparing British Standards and other standards-related publications, information and services.

BSI is incorporated by Royal Charter. British Standards and other standardization products are published by BSI Standards Limited.

About us

We bring together business, industry, government, consumers, innovators and others to shape their combined experience and expertise into standards-based solutions.

The knowledge embodied in our standards has been carefully assembled in a dependable format and refined through our open consultation process. Organizations of all sizes and across all sectors choose standards to help them achieve their goals.

Information on standards

We can provide you with the knowledge that your organization needs to succeed. Find out more about British Standards by visiting our website at bsigroup.com/standards or contacting our Customer Services team or Knowledge Centre.

Buying standards

You can buy and download PDF versions of BSI publications, including British and adopted European and international standards, through our website at bsigroup.com/shop, where hard copies can also be purchased.

If you need international and foreign standards from other Standards Development Organizations, hard copies can be ordered from our Customer Services team.

Subscriptions

Our range of subscription services are designed to make using standards easier for you. For further information on our subscription products go to bsigroup.com/subscriptions.

With **British Standards Online (BSOL)** you'll have instant access to over 55,000 British and adopted European and international standards from your desktop. It's available 24/7 and is refreshed daily so you'll always be up to date.

You can keep in touch with standards developments and receive substantial discounts on the purchase price of standards, both in single copy and subscription format, by becoming a **BSI Subscribing Member**.

PLUS is an updating service exclusive to BSI Subscribing Members. You will automatically receive the latest hard copy of your standards when they're revised or replaced.

To find out more about becoming a BSI Subscribing Member and the benefits of membership, please visit bsigroup.com/shop.

With a **Multi-User Network Licence (MUNL)** you are able to host standards publications on your intranet. Licences can cover as few or as many users as you wish. With updates supplied as soon as they're available, you can be sure your documentation is current. For further information, email bsmusales@bsigroup.com.

BSI Group Headquarters

389 Chiswick High Road London W4 4AL UK

Revisions

Our British Standards and other publications are updated by amendment or revision.

We continually improve the quality of our products and services to benefit your business. If you find an inaccuracy or ambiguity within a British Standard or other BSI publication please inform the Knowledge Centre.

Copyright

All the data, software and documentation set out in all British Standards and other BSI publications are the property of and copyrighted by BSI, or some person or entity that owns copyright in the information used (such as the international standardization bodies) and has formally licensed such information to BSI for commercial publication and use. Except as permitted under the Copyright, Designs and Patents Act 1988 no extract may be reproduced, stored in a retrieval system or transmitted in any form or by any means – electronic, photocopying, recording or otherwise – without prior written permission from BSI. Details and advice can be obtained from the Copyright & Licensing Department.

Useful Contacts:

Customer Services

Tel: +44 845 086 9001

Email (orders): orders@bsigroup.com

Email (enquiries): cservices@bsigroup.com

Subscriptions

Tel: +44 845 086 9001

Email: subscriptions@bsigroup.com

Knowledge Centre

Tel: +44 20 8996 7004

Email: knowledgecentre@bsigroup.com

Copyright & Licensing

Tel: +44 20 8996 7070

Email: copyright@bsigroup.com



...making excellence a habit.™