



BSI Standards Publication

Nanomanufacturing — Key control characteristics

Part 4-3: Nano-enabled electrical energy storage — Contact and coating resistivity measurements for nanomaterials

National foreword

This Published Document is the UK implementation of IEC/TS 62607-4-3:2015.

The UK participation in its preparation was entrusted to Technical Committee NTI/1, Nanotechnologies.

A list of organizations represented on this committee can be obtained on request to its secretary.

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Published by BSI Standards Limited 2015

ISBN 978 0 580 86146 8

ICS 07.030

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This Published Document was published under the authority of the Standards Policy and Strategy Committee on 30 September 2015.

Amendments/corrigenda issued since publication

Date	Text affected
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TECHNICAL SPECIFICATION



**Nanomanufacturing – Key control characteristics –
Part 4-3: Nano-enabled electrical energy storage – Contact and coating
resistivity measurements for nanomaterials**

INTERNATIONAL
ELECTROTECHNICAL
COMMISSION

ICS 07.030

ISBN 978-2-8322-2851-7

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INTERNATIONAL ELECTROTECHNICAL COMMISSION

NANOMANUFACTURING – KEY CONTROL CHARACTERISTICS –**Part 4-3: Nano-enabled electrical energy storage –
Contact and coating resistivity measurements for nanomaterials**

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Technical Specifications are subject to review within three years of publication to decide whether they can be transformed into International Standards.

IEC 62607-4-3, which is a Technical Specification, has been prepared by IEC technical committee 113: Nanotechnology standardization for electrical and electronic products and systems.

The text of this Technical Specification is based on the following documents:

Enquiry draft	Report on voting
113/239/DTS	113/263A/RVC

Full information on the voting for the approval of this Technical Specification can be found in the report on voting indicated in the above table.

This publication has been drafted in accordance with the ISO/IEC Directives, Part 2.

A list of all parts in the IEC 62607 series, published under the general title *Nanomanufacturing – Key control characteristics*, can be found on the IEC website.

The committee has decided that the contents of this publication will remain unchanged until the stability date indicated on the IEC website under "<http://webstore.iec.ch>" in the data related to the specific publication. At this date, the publication will be

- transformed into an International Standard,
- reconfirmed,
- withdrawn,
- replaced by a revised edition, or
- amended.

A bilingual version of this publication may be issued at a later date.

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INTRODUCTION

The future utilization of renewable energy technologies including e-mobility for individual transportation significantly depends on the development of efficient systems for energy storage. From today's perspective, lithium-ion batteries, supercapacitors and their derivative concepts are regarded as the most promising innovative candidates.

A high energy density for the desired power and a long life time (recharge characteristics) are the two most important criteria for electrode materials. Because many electrochemically active materials such as metal oxides show an inherently lower and insufficient conductivity for the electron transport, composite materials with carbon nanomaterial content are used for optimization of the current flow in the electrodes of a battery. The electrochemical reactions and the ensuing energy density of the battery cells are influenced by the movement of electrons in a composite. Furthermore, the electronic contact resistivity between the electrode material and the metal collector is important to realize a low ohmic internal resistance of the battery or capacitor device.

This part of IEC 62607 provides standard methods to measure coating and contact resistivity of nano-enabled electrode materials and to evaluate the best combinations of the composite material recipes and fabrication technologies for carbon containing coatings of such nano-enabled electrodes. Following this method will allow comparison of the results of different research groups.

This standardized method is intended for comparing the contact and coating resistivity of composite materials with carbon nanomaterial content in the study stage, not for evaluating the electrode in end products.

The method is applicable for nano-enabled materials exhibiting function or performance only possible with nanotechnology, intentionally added to composite materials for measurable and significant improvement of the current flow in the electrodes of electrical energy storage devices.

In this context it is important to note that the percentage content of nanomaterial of the device in question has no direct relation to the applicability of this part of IEC 62607, because minute quantities of nanomaterial are frequently sufficient to improve the performance significantly.

The fraction of nanomaterials in electrodes, electrode coatings, separators or electrolyte is not of relevance for using this method.

NANOMANUFACTURING – KEY CONTROL CHARACTERISTICS –

Part 4-3: Nano-enabled electrical energy storage – Contact and coating resistivity measurements for nanomaterials

1 Scope

This part of IEC 62607 provides a standardized test method for the measurement of contact and coating resistivity of nano-enabled electrode materials. This method will enable a customer to:

- a) decide whether or not a coating composite material is usable, and
- b) select best combinations of coating composite material with fabrication technologies suitable for their application.

This part of IEC 62607 includes:

- definitions of terminology used in this part of IEC 62607,
- recommendations for sample preparation,
- outlines of the experimental procedures used to measure and calculate the contact and coating resistivity,
- methods of interpretation of results and discussion of data analysis, and
- a case study.

2 Normative references

The following documents, in whole or in part, are normatively referenced in this document and are indispensable for its application. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

ISO/TS 80004-1, *Nanotechnologies – Vocabulary – Part 1: Core terms*

3 Terms, definitions, acronyms and abbreviations

3.1 Terms and definitions

For the purposes of this document, the terms and definitions given in ISO/TS 80004-1 and the following apply.

3.1.1

electrode nanomaterial

material used in nano-enabled energy storage devices such as lithium-ion batteries or supercapacitors which contains a fraction of nanomaterial and exhibits function or performance made possible only with the application of nanotechnology

Note 1 to entry: Electrodes used in lithium-ion batteries or supercapacitors consist of mixed raw material powders (e.g. electrochemical active and carbon based nanomaterial powders) in a solvent with binder which forms a casting slurry. These slurries are coated by doctor blade process on thin metal collector foils, dried and subsequently calendar compressed to the final electrode. The electrode shows a multilayered layout, built up of (1) an aluminium or copper current collector and (2) the electrode material layer. This material layer consists of the active phase (cathode – lithium containing mixed oxides or phosphate, e.g. LCO, NCA, NCM, and LFP; anode, e.g. graphite and supercap – activated carbon), a conducting phase (e.g. carbon nanomaterials like CB, carbon nanotubes or fibres) and an organic binder (e.g. PVDF or SBR).

3.1.2 coating resistivity

resistance to the passage of an electric current through the electrode material layer

Note 1 to entry: It is expressed as electrical resistivity.

Note 2 to entry: The electric resistivity of the electrode material layer depends on several factors such as raw materials, the slurry processing step and the final electrode fabrication technology. Differences in the nanomaterial carbon content, the fabrication technology and the density or porosity of the layer can significantly influence its resistivity. It is possible to evaluate the resistivity by preparing a thin coating of electrode material on an isolator substrate. In the attached case study a sample design based on 5 cm² ceramic substrates is shown.

3.1.3 contact resistivity

electrical contact resistance between the metal current collector and the electrode material layer for a contact area of 1 cm²

Note 1 to entry: During the life time of a battery the contact resistance influences the degradation stability (e.g. rise in internal resistance due to delamination), capacity loss during cycling or heating and rise of the internal temperature of the cell. The contact resistivity depends on the microstructure of the interface between metal collector and electrode material layer. The material and the electrode processing steps such as choice and pre-treatment of the metal collector or the calendaring process have an important influence on the contact resistivity. It is possible to evaluate the contact resistivity by preparation of a thin coating of electrode material on an isolator substrate. The method is derived from a “transmission line method” (TLM) used for characterization of contact resistivity of metal-semiconductor interfaces in the field of photovoltaics [1]. In the attached case study a sample design based on 5 cm² ceramic substrates is shown. The measurement of coating resistivity is carried out using a 4-point probe method.

3.1.4 calendaring

process where the electrode foils pass under rollers at a high pressure

Note 1 to entry: Calendaring is an important step during the electrode manufacturing process, because by this method the final electrode microstructure and thickness is formed. Methods like rolling or lamination are used to densify the electrode material layer to a desired degree of thickness and porosity.

3.2 Acronyms and abbreviations

LCO	lithium cobalt oxide, LiCoO ₂
NCA	lithium nickel cobalt aluminium oxide, Li(Ni,Co,Al)O ₂
NCM	lithium nickel cobalt manganese oxide, LiNi _{1/3} Co _{1/3} Mn _{1/3} O ₂
LFP	lithium iron phosphate, LiFePO ₄
CB	carbon black
PVDF	polyvinylidene difluorite
SBR	styrene-butadiene rubber
EDLC	electrical double-layer capacitor
TLM	transmission line method

4 Sample preparation methods

4.1 General

The preparation of electrode nanomaterial samples consists of the following steps:

- mixing a casting slurry;
- assembly of metal collector strips on isolator carrier substrates;
- casting of the slurry on these carrier substrates; and
- drying and densification of the samples.

4.2 Reagents

4.2.1 Casting slurry

An electrode casting slurry is prepared in steps by dispensing and mixing different powders with solvent and binder. The choice of material recipe and the procedure of slurry preparation depend on the user and can be carried out similar to the industrial processes. The viscosity of the casting slurry should be in the range 0,5 Pa·s to 6 Pa·s (at low shearing rate 1/20 s). In this way, the slurry can be cast by doctor blade.

4.2.2 Isolator substrates

An isolator substrate serves as a carrier of the electrode coating. The substrate should be non-conductive, show a high accuracy in thickness homogeneity and flatness, a low roughness and a proper wettability with the casting slurry. Ceramic based thick film substrates like alumina with a thickness of (650 ± 5) mm, a flatness of < 10 mm per sample ($50 \text{ mm} \times 50 \text{ mm}$ substrate area) and a roughness $R_a < 1 \text{ } \mu\text{m}$ are recommended.

4.2.3 Metal collector strips and sample layout

Metal strips are cut out from the original current collector foil in the geometry of 2 mm width by 70 mm length. For the measurement of the coating resistivity four of these strips are bonded with glue based on cyanoacrylate in four-probe geometry (inner distance between metal strips contacts is 30 mm) on the isolator substrate. For the measurement of the contact resistivity 10 strips are bonded an equal distance (3 mm) from each other. Figure 1 shows the sample layouts. The choice of current collector material depends on the user and can be similar to industrial processes. Typical collector thicknesses are in the range 9 mm to 40 mm for aluminium and 10 mm to 20 mm for copper current collectors.

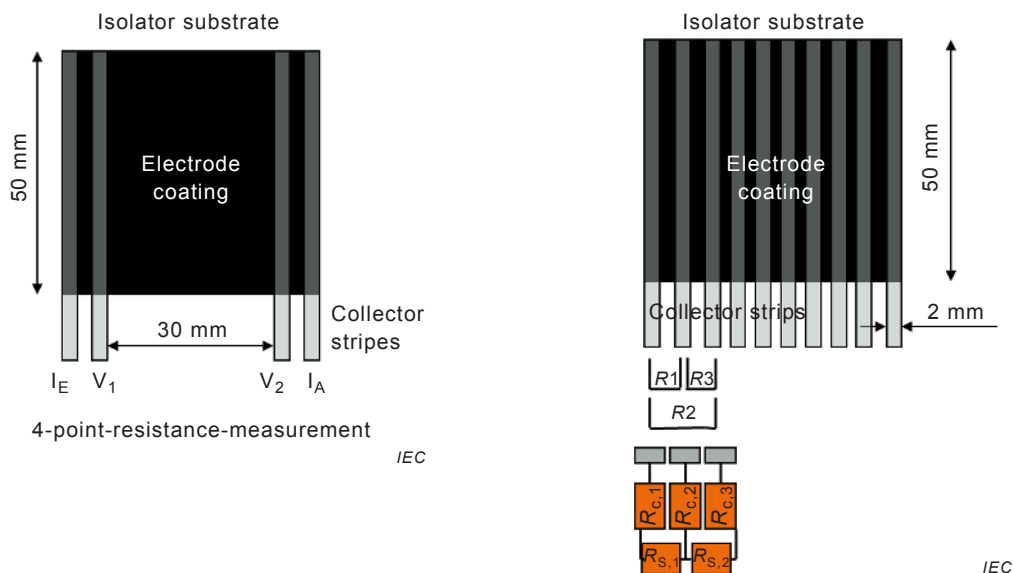


Figure 1 – Layout of the coating (left) and contact (right) resistivity measurement

4.3 Preparation of the electrode nanomaterial test samples

The slurry is cast by hand with a film applicator (doctor blade) on the isolator substrates which forms after drying the electrode layer. To set an accurate layer thickness the substrates are fixed on an aluminium carrier panel with cavities of the sample size of $50 \text{ mm} \times 50 \text{ mm}$. A doctor blade with a $500 \text{ } \mu\text{m}$ slot is used. To prepare a series of samples of the same type and quality it is possible to arrange several substrates on the carrier and to coat them with a single coating step.

Drying of the samples can be done at room or at elevated temperature with a customized temperature time profile in a drying oven. Afterwards the samples are ready for a first electronic characterization of the electrode state “as cast”.

The sample thickness is measured by a laser profilometer or a micrometer gauge (see detailed description in 5.2.2).

To characterize an electrode densification like calendaring it is possible to compress the samples by lamination under pressure and temperature. For an isostatic lamination the samples are sealed in lamination bags and laminated for example at 150 bar, 40 °C for 10 min. During this procedure the coating thickness shrinks and the layer densifies (“densified” state of the electrode) and is ready for subsequent electronic characterization.

To balance the shrinkage values and porosity of the samples with industrial electrodes processed by calendaring, it is recommended to adjust the laminating parameters on the individual electrode material system by measuring the thickness change during densification. Depending on the material recipe and sample preparation, the resulting electrode thickness change is in the range 10 % to 50 %.

5 Measurement of electric properties

5.1 General

Depending on the interest of the users, it is possible to characterize the prepared samples “as casted”, and “as densified”. The procedure to measure the coating and contact resistivity of such samples is described in 5.2 and 5.3 and is always the same.

NOTE In the state “as casted” the layer is already dried!

5.2 Coating resistivity

5.2.1 Demarcation of method

The coating resistivity of the electrode material layer shows a pure ohmic behaviour (linear correlation between voltage and current). The geometry of the electrical contact of the sample layout leads to a homogeneous current flow in the electrode coating (see Figure.A.3).

5.2.2 Measurement of the sample thickness

To calculate an electric resistivity it is important to measure the substrate and electrode thickness exactly. Prior to coating, the isolator substrate is measured by micrometer calliper. The coated sample is measured in the state of “as cast” and “as densified” with a laser profilometer. A minimum of three topographic line measurements across the sample are recommended to calculate a mean electrode coating thickness. The standard deviation of this thickness should lie below 10 % relative to the mean thickness.

5.2.3 Experimental procedures and measurement conditions

The sample is connected to a d.c. power supply source to set a constant current of 100 μ A between the outer contact strips (I_E-I_A) and the resulting voltage drop between the inner contact strips (V_1-V_2) is measured with voltage metering device (Figure A.3). The collector contact strips are connected by hand via needle test probes and banana plugs to the electrical devices. Due to variations in the sample quality (electrode thickness, amount of coating defects) it is recommended to test at least 10 samples of the same type. The coating resistivity is a mean value of these 10 samples, whereby the standard deviation of the resistivity should be below 10 % relative to the mean resistivity value.

5.3 Contact resistivity

5.3.1 Demarcation of method

The measurement of the contact resistivity works on the basis of the transmission line method (TLM) used to evaluate the contact resistivity of metal to semiconductor interfaces.

5.3.2 Experimental procedures and measurement conditions

The sample is connected to a d.c. power supply source to set a constant current of 100 μ A between alternating contact strips and the resulting voltage drop between these contact strips is measured with a voltage metering device. The contact strips are connected by hand via needle test probes and banana plugs to the electrical devices. Gradually the resistances between alternating positions of each of the ten contact strips are measured in the order of: $R1(n \text{ to } n + 1)$, $R2(n \text{ to } n + 2)$ and $R3(n + 1 \text{ to } n + 2)$ with $n = 1$ to 8. The following equations illustrate as an example of the scheme for evaluation of the contact resistance of the metal strip No. 2 of the sample (see Figure A.4):

$$R1 = R_{c,1} + R_{s,1} + R_{c,2}$$

$$R2 = R_{c,1} + R_{s,1} + R_{s,2} + R_{c,3}$$

$$R3 = R_{c,2} + R_{s,2} + R_{c,3}$$

$$R_{c,2} = (R1 + R3 - R2)/2 \text{ (absolute contact resistance of metal strip No. 2 in ohms)}$$

where

R_c is the contact resistance of the individual part of the sample;

R_s is the coating resistance of the individual part of the sample;

$R1$ to $R3$ are ohmic resistances [Ω] calculated by $R = U/I$.

Due to variations in the sample quality (electrode thickness, amount of coating defects and accuracy of the sample geometry) it is recommended to test at least five samples of the same type. The calculation of the contact resistivity follows a summation of different resistances which results in a contact resistivity of one of the ten collector strips. For each sample up to eight measured values can be generated successively.

6 Data analysis / interpretation of results

6.1 Coating resistivity

calculation: $\rho [\Omega \cdot \text{cm}] = R_{\text{Meas}} [\Omega] \times y [\text{mm}] \times S_d [\mu\text{m}] / (x [\text{mm}] \times 10^4)$

where

$$R_{\text{Meas}} = U / I;$$

ρ is the coating resistivity;

R_{Meas} is the coating resistance;

I is the preset current (100 μ A);

U is the measured voltage between the two inner strip contacts (Figure A.3 voltage between V_1 and V_2);

S_d is the coating thickness;

y is the sample length (50 mm);

x is the sample width between the two inner strip contacts (30 mm).

Calculation of a mean value of ten samples is recommended. The standard deviation should be below 10 %.

chart: coating resistivity vs. sample thickness (see A.2)

target value: coating resistivity

6.2 Contact resistivity

calculation: $r_c [\Omega \cdot \text{cm}^2] = R_c [\Omega] \times z [\text{cm}] \times y [\text{cm}]$

where

$R_c = (R_{n \text{ to } n+1} + R_{n \text{ to } n+2} - R_{n+1 \text{ to } n+2}) / 2$, and

$R = U / I$ of the individual measurement;

r_c is the specific contact resistivity;

n is the number of metal collector strips ($n = 1, \dots, 8$);

R_c is the contact resistance;

I is the preset current between two contact strips (100 μA);

U is the measured voltage between two contact strips;

z is the contact strip width (0,2 cm);

y is the contact strip length (equals sample length of 5 cm).

Each sample with ten metal strip contacts delivers eight results of contact resistivity. The calculation of a mean value of at least five samples is recommended (40 single measurements of contact resistivity). The standard deviation should be below 50 %.

chart: contact resistivity vs. sample thickness (see Figures A.4 to A.7)

target value: contact resistivity

Annex A (informative)

Case study

A.1 Sample preparation

See Figure A.1.



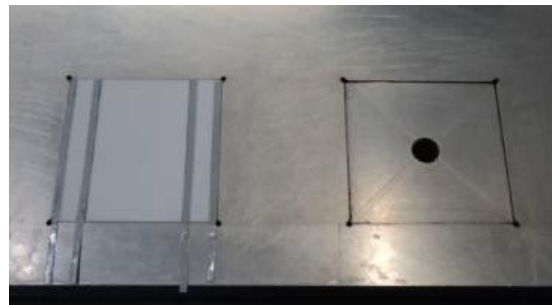
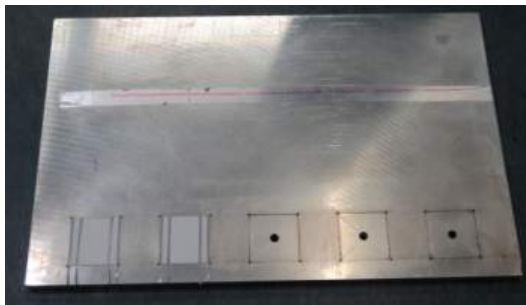
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a) Electrode casting slurry



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b) Alumina substrate with metal collector strips



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c) Aluminium carrier panel with cavities of the sample size

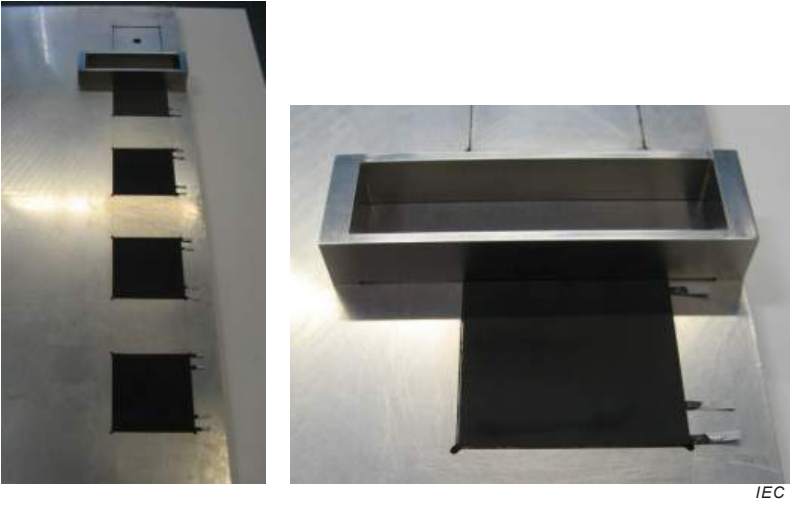
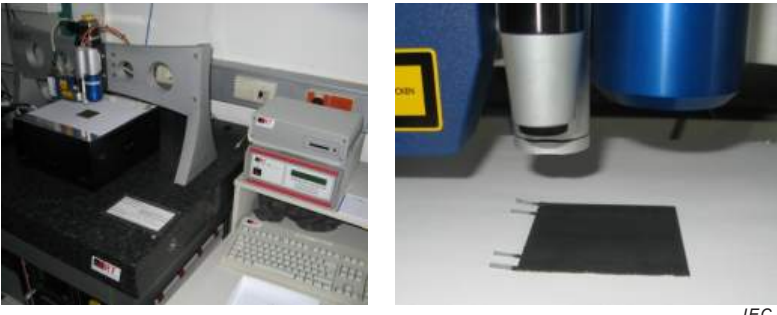

Figure A.1 – Sample preparation

Components which are required:

- 1) electrode casting slurry;
- 2) isolator substrates (5 cm × 5 cm);
- 3) metal collector strips (each 2 mm wide and 70 mm long);
- 4) aluminium carrier panel with substrate cavities.

The electrode casting slurry is prepared in a quantity of approximately 100 ml. The collector foil is cut into thin metal strips. These strips are bonded with superglue on the isolator substrates in a special layout for measurement of the coating or contact resistivity.

Construction steps are illustrated and described in Figure A.2.

Step		
a	 <p>The isolator substrates are fixed on the carrier panel within the cavities. The surface of the substrates and the carrier panel are afterwards on equal height. The electrode casting slurry is filled into a film applicator (doctor blade). This film applicator is moved along the carrier panel above the isolator substrates whereupon the electrode coating takes place. The coated substrates are left to rest for drying at room temperature or set into a drying oven.</p>	
b	 <p>The sample thickness is characterized at three different positions by laser profilometer (line scan across the sample). By measurement of the initial substrate thickness (without coating) it is possible to calculate the final electrode coating thickness.</p>	
c	 <p>The compression of the electrode is done in an isostatic laminator. The substrates are sealed within a lamination bag. Afterwards they were placed into the laminator and put under pressure and temperature (for example 150 bar, 40 °C, 10 min).</p>	

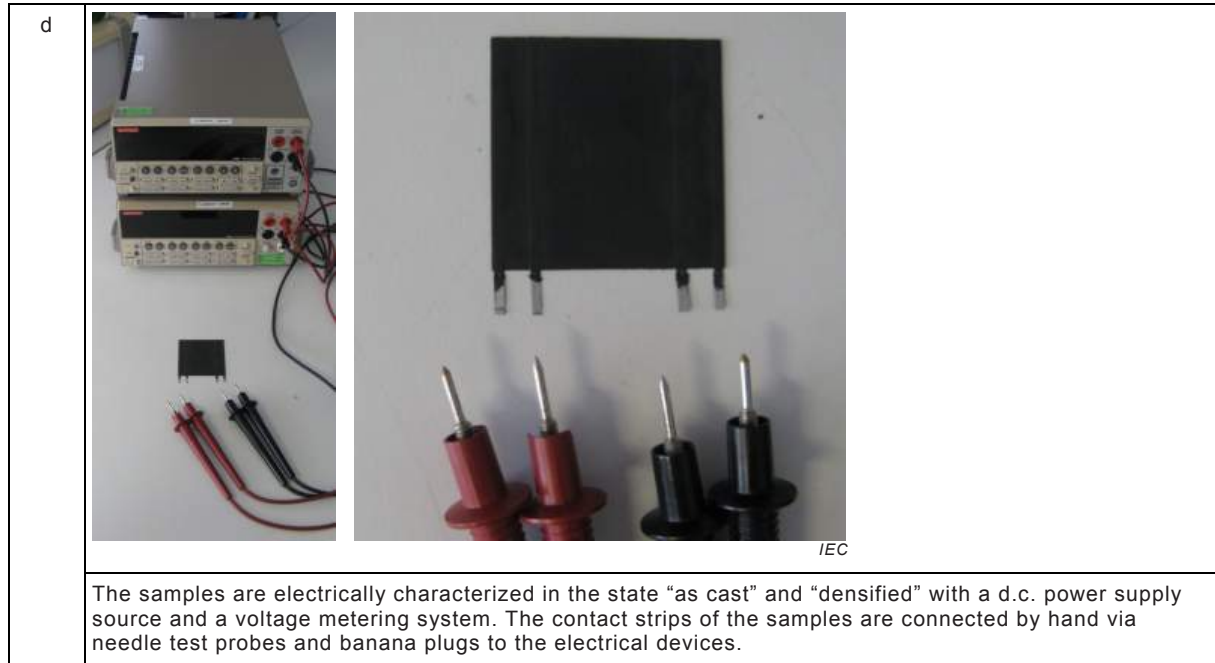


Figure A.2 – Construction steps

A.2 Results for a supercap EDLC-electrode and a lithium-ion battery NCM-cathode

A.2.1 Linear correlation between current and voltage of the electrode coating resistance of a supercap electrode (ohmic behaviour)

See Figure A.3.

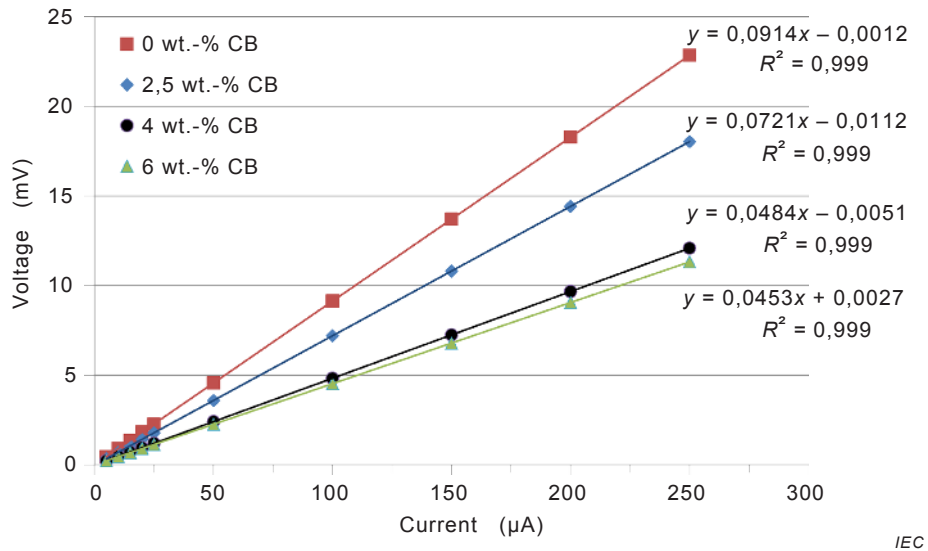


Figure A.3 – Correlation between current and voltage of the coating resistance of various supercap EDLC-electrodes (variation in amount of carbon black additive in the electrode recipe)

A.2.2 Results for coating resistivity

See Figures A.4 and A.5.

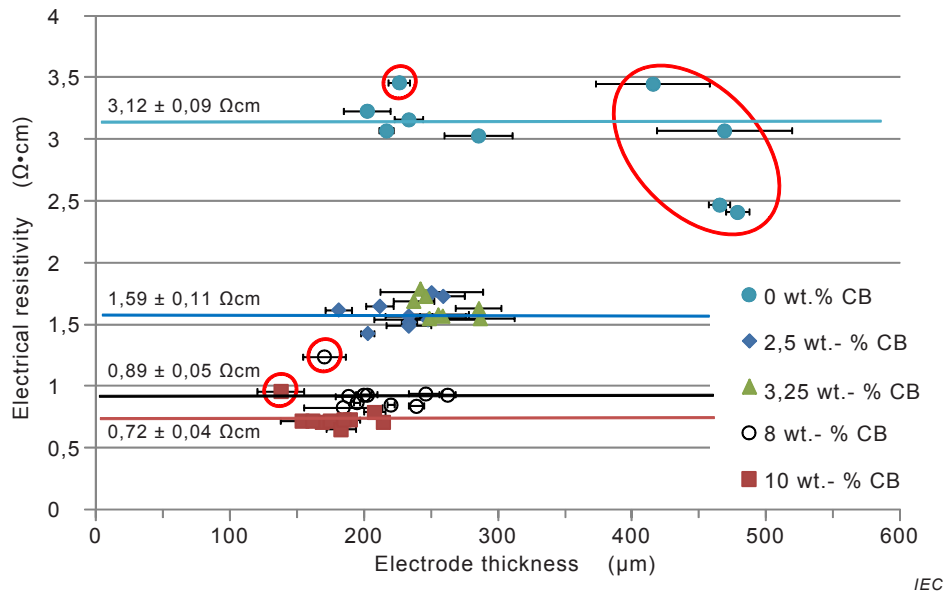


Figure A.4 – Coating resistivity of supercap electrodes with variation in the amount of carbon black in the electrode composite recipe and sample thickness

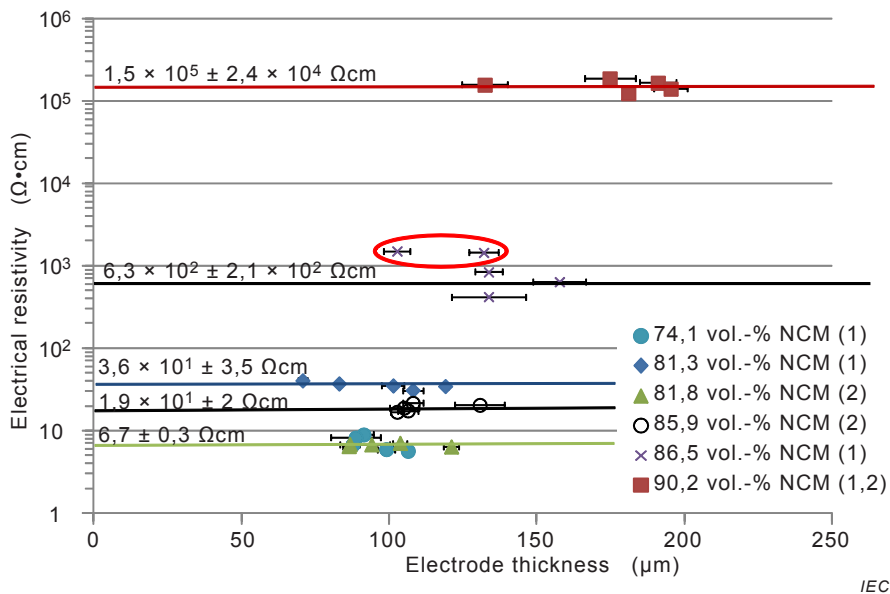


Figure A.5 – Coating resistivity of NCM-based lithium-ion battery cathode with variation in the amount of NCM, binder to carbon black value and sample thickness

A.2.3 Results of measurement of contact resistivity

See Figures A.6 and A.7.

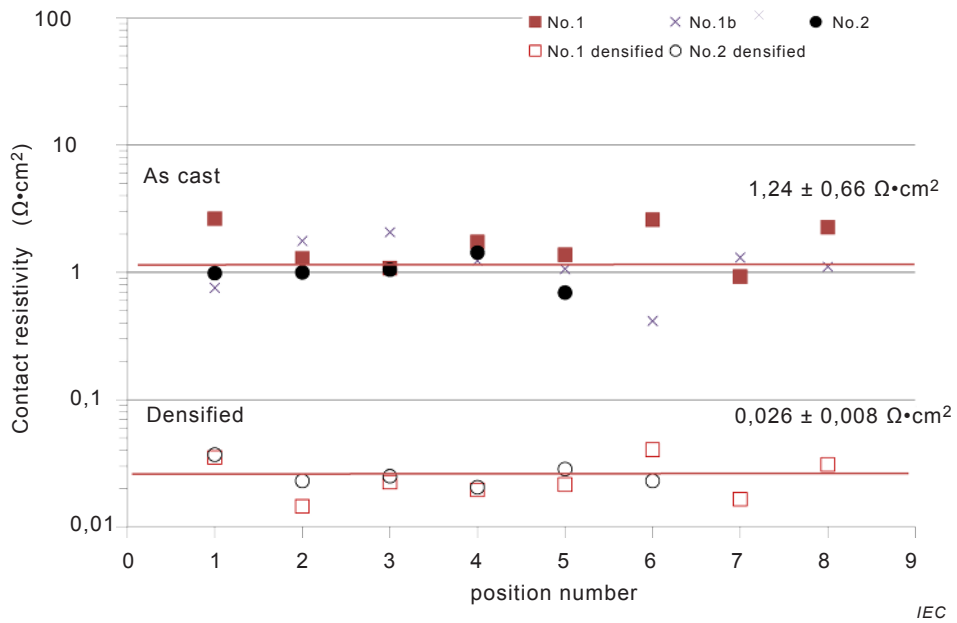


Figure A.6 – Contact resistivity of a supercap electrode in the state “as cast” and “densified”

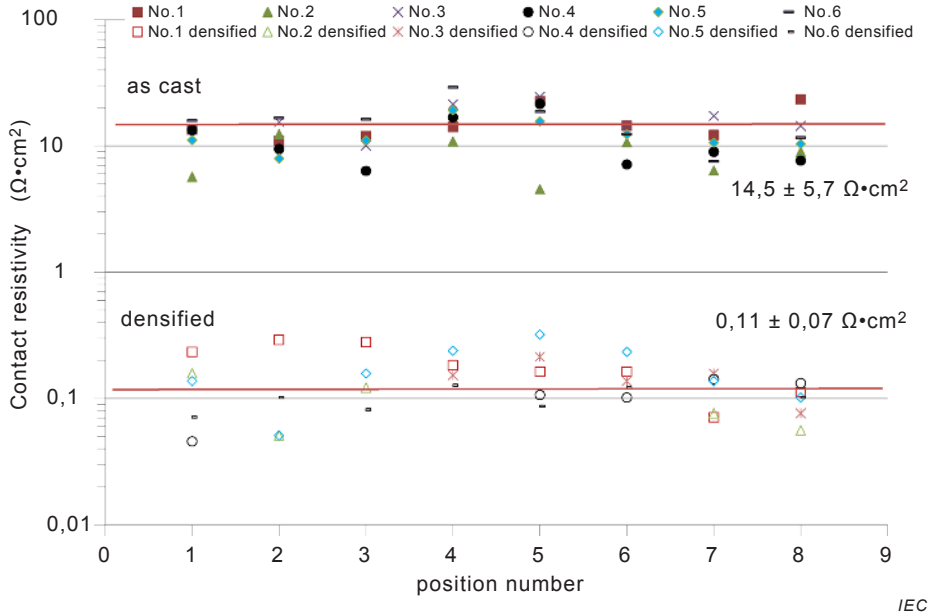


Figure A.7 – Contact resistivity of a NCM-based lithium-ion battery cathode (81,3 vol.-% NCM) in the state “as cast” and “as densified”

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