

Specification for

# Pressure vessel details (dimensions) —

Part 4: Standardized pressure vessels

UDC 621.772.4:621.642:66.023

## Cooperating organizations

The Pressure Vessel Standards Committee, under whose direction this British Standard was prepared, consists of representatives from the following Government departments and industrial and professional organizations:

Associated Offices Technical Committee\*  
 Association of Shell Boilermakers  
 British Chemical Engineering Contractors' Association\*  
 British Compressed Gases Association  
 British Gas Corporation\*  
 British Insurance (Atomic Energy) Committee  
 British Steel Industry\*  
 CBMPE\*  
 Chemical Industries Association\*  
 Department of Trade (Marine Division)  
 Electricity Supply Industry in England and Wales\*  
 Engineering Equipment Users' Association\*  
 Health and Safety Executive  
 Institution of Chemical Engineers  
 Institution of Gas Engineers\*  
 Institution of Mechanical Engineers\*  
 Lloyd's Register of Shipping\*  
 Oil Companies Materials Association\*  
 Process Plant Association\*  
 The Welding Institute  
 United Kingdom Atomic Energy Authority  
 University of Manchester — Institute of Science and Technology  
 Water-tube Boilermakers' Association

The organizations marked with an asterisk in the above list, together with the following, were directly represented on the committee entrusted with the preparation of this British Standard:

Association of Consulting Engineers  
 Association of Hydraulic Equipment Manufacturers  
 British Valve Manufacturers' Association  
 National Association of Drop Forgers and Stampers

This British Standard, having been prepared under the direction of the Pressure Vessel Standards Committee, was published under the authority of the Executive Board on 31 August 1977

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The following BSI references relate to the work on this standard:  
 Committee reference PVE/II  
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# Foreword

This British Standard has been prepared under the direction of the Pressure Vessel Standards Committee to cover the dimensions of pressure vessel details. It has been arranged in Parts as follows:

- *Part 1: Davits for branch covers;*
- *Part 2: Saddle supports for horizontal cylindrical pressure vessels (in course of preparation);*
- *Part 3: Dimensional tolerances for pressure vessels (currently Draft for Development DD 42);*
- *Part 4: Standardized pressure vessels.*

This Part replaces BS 3161 and is confined to unfired cylindrical pressure vessels for horizontal and vertical use in the chemical and allied industries. Only one of the shapes of domed ends previously shown in BS 1966 is specified; this is the torispherical 2 : 1 radius/height ratio in terms of the inner profile (domed ends with 6 % and 10 % knuckle radii are not currently included).

It is intended that the module system adopted for the shell cylinder lengths will lead to economies in the manufacture of carbon steel and carbon manganese steel vessels by reducing the number of plate sizes used and minimizing the equipment required for fabrication.

This Part covers dimensions and pressure ratings for basic unpierced vessels thereby providing an aid to selection of standardized vessels and is intended for use in conjunction with BS 5500 “*Unfired fusion welded pressure vessels*”.

A British Standard does not purport to include all the necessary provisions of a contract. Users of British Standards are responsible for their correct application.

**Compliance with a British Standard does not of itself confer immunity from legal obligations.**

## Summary of pages

This document comprises a front cover, an inside front cover, pages i and ii, pages 1 to 12, an inside back cover and a back cover.

This standard has been updated (see copyright date) and may have had amendments incorporated. This will be indicated in the amendment table on the inside front cover.

## 1 Scope

This Part of this British Standard specifies requirements for cylindrical vessels with torispherical domed ends. The lengths and thicknesses of the shell cylinders are based on standard carbon and carbon manganese steel plates. Permissible internal pressures for the domed ends and shell cylinders, not taking account of openings, can be calculated using the dimensions and pressure coefficients stated in this standard together with the relevant stress values obtained from BS 5500.

The overall design of vessels, their fabrication and testing shall be in accordance with BS 5500.

For vessels that are outside the range of sizes covered, it is recommended that shell cylinder lengths should be derived using the modular method described in 5.2.1.

## 2 References

The titles of the publications referred to in this standard are listed on the inside back cover.

## 3 Terms and symbols

For the purposes of this British Standard the terms and symbols illustrated in Figure 1 apply.

## 4 Shapes

**4.1** Standard diameters and lengths of shell cylinders shall be as shown in Table 1 and Table 2 together with the nominal volumes contained within the vessels and their aspect ratios (length : diameter). Table 1 facilitates the selection of a standardized vessel for a required capacity, diameter and aspect ratio.

**4.2** Domed ends shall be torispherical as defined in Table 4 in terms of inner profile.

## 5 Dimensions

**5.1 General.** Linear dimensions are specified in millimetres, volumes in cubic metres.

Diameters of vessels are based on metric inside diameters and, in order to enable manufacturers to utilize existing "inch size" forming tools for the domed ends, a variation of  $\pm 12$  mm is permissible on diameters up to and including 1 300 mm. This is a temporary measure and manufacturers are strongly recommended to adopt nominal sizes when re-tooling.

### 5.2 Shell cylinders

**5.2.1 Modular lengths.** A standardized range of modular lengths shall be as given in Table 1 and Table 2. These lengths are based on the use of a single standard width of plate, purchased 2 500 mm wide. Shell cylinder lengths are built up in modular form using full plate widths where possible and fractions of these where necessary. Allowance is made for edge preparation, resulting in fabrication strakes of 2 480 mm (full plate), 1 860 mm ( $\frac{3}{4}$  plate), 1 235 mm ( $\frac{1}{2}$  plate) and 610 mm ( $\frac{1}{4}$  plate). The use of alternative widths to achieve the overall shell cylinder lengths is not, however, precluded.

**5.2.2 Thicknesses.** Shell cylinder thicknesses  $e_{\text{cyl}}$ , which include 1.5 mm corrosion allowance, associated with each diameter shall be as given in Table 3.

### 5.3 Domed ends

**5.3.1 Profile.** The dimensions of the inner profile shall be as given in Table 4.

It is permissible to use any values of crown and knuckle radii between the stated limits provided that the head height is as specified. Appropriate values may be selected using Appendix A. For practical purposes the profiles headed "ellipsoidal" are indistinguishable from ellipsoids of vessel radius/height ratio 2 : 1, which are also acceptable.

In the manufacture of domed ends where advantage is taken of the permissible variation of  $\pm 12$  mm on the nominal diameter (see 5.1) the inside crown radius shall be between  $0.75D_i$  and  $0.95D_i$ , the inside knuckle radius shall be between  $0.125D_i$  and  $0.1805D_i$  and the inside height shall be not less than  $0.25D_i$  where  $D_i$  is equal to the inside diameter, as manufactured, of the end concerned.

**5.3.2 Lengths of straight flanges.** The straight flanges shall be 50 mm long for vessels up to and including 1 700 mm diameter and 65 mm long for vessels above 1 700 mm diameter.

**5.3.3 Thicknesses.** Minimum thicknesses  $e_{\text{end}}$ , which include 1.5 mm corrosion allowance, associated with each diameter shall be as given in Table 3. These have been calculated to match the corresponding thickness  $e_{\text{cyl}}$  of the shell cylinder on the basis of equivalent strength. It is the responsibility of the manufacturer to select a suitable plate thickness to ensure that, after forming, the thickness shall at no point in the profile be less than  $e_{\text{end}}$  and that the thickness of the straight flange when prepared for welding shall be not less than the thickness  $e_{\text{cyl}}$  of the shell cylinder.

**5.4 Dimensional tolerances.** These shall be in accordance with BS 5500 except that the tolerance on the circumference (4.2.4.1.1 of BS 5500:1976) shall be increased by  $\pm 38$  mm for diameters up to and including 1 300 mm (see 5.1).

General dimensional tolerances for completed vessels shall be in accordance with DD 42.

## 6 Internal pressure rating of basic unpierced vessels

**6.1 Procedure.** To determine the shell cylinder and domed end thicknesses for a given pressure and stress, calculate the ratio  $p \div f$  to find the value of the pressure coefficient,  $k$ .

$$k = \frac{p}{f}$$

where

$p$  is the maximum permissible gauge pressure (in bar<sup>a</sup>) for vessel (including static head where significant).

$f$  is the maximum allowable design stress in material (in N/mm<sup>2</sup>).

<sup>a</sup> 1 bar = 10<sup>5</sup> N/m<sup>2</sup> = 100 kPa.

Enter Table 3 at the appropriate diameter and find a value of  $k$  equal to or greater than the calculated value.

Read off  $e_{\text{cyl}}$  and  $e_{\text{end}}$  for the thicknesses of the shell cylinder and the domed end respectively.

**6.2 Derivation of pressure coefficient  $k$**  (see Table 3). Coefficients are based on calculations to BS 5500:1976 as follows:

Shell cylinders, 3.5.1.2 a)

Unpierced ends, 3.5.2.3

The calculations include a corrosion allowance of 1.5 mm. In the case of vessels up to and including 1 300 mm diameter calculations are made for diameters inclusive of tolerance and variation (see 5.1).

## 7 Other requirements

Irrespective of the category of vessel, if the ends are made from more than one plate, the welds within each end shall be completely radiographed or examined ultrasonically before the end is formed. After forming, the knuckle region of these welds shall be examined by radiography or ultrasonic means.

The following information shall be supplied by the vessel fabricator when ordering ends.

- a) Inside diameter.
- b) Minimum thickness ( $e_{\text{end}}$ ).
- c) End preparation of the straight flange and the associated shell cylinder thickness ( $e_{\text{cyl}}$ ).
- d) The material specified in accordance with the appropriate British Standard.
- e) Any heat treatment requirements.
- f) Any further inspection requirements.
- g) Surface finish, if necessary.

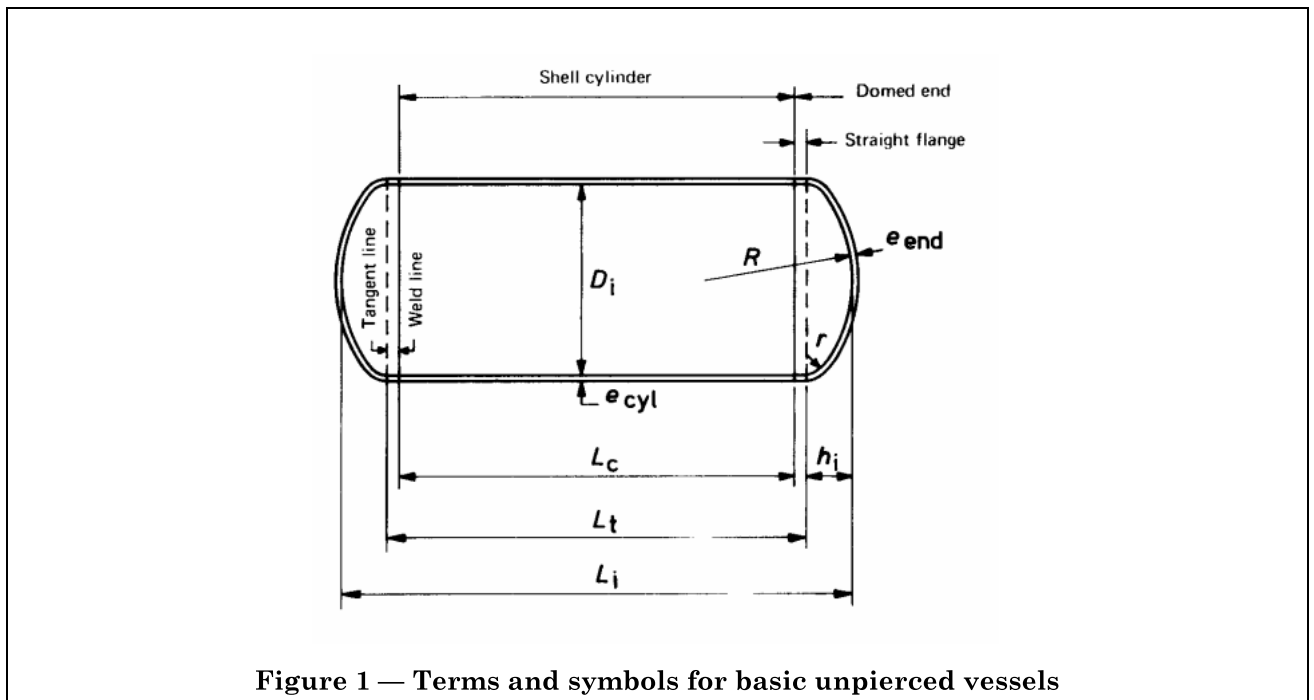


Table 1 — Volumes, diameters and aspect ratios of standard vessels

Volume range m <sup>3</sup>	D <sub>i</sub> mm	Modular plate length														Nominal volume of vessel m <sup>3</sup>							
		¼	½	¾	1	1¼	1½	1⅔	2	2¼	2½	3	3½	4	4½		5	5½	6	6½	7	7½	8
< 1	600 <sup>a</sup>	0.26	0.43	0.61	0.78	0.96																	
	650	0.31	0.51	0.72	0.93	1.13	1.34																
	700	0.36	0.6	0.84	1.08	1.32	1.56																
1 < 2	750 <sup>a</sup>	0.42	0.7	0.97	1.25	1.52	1.79																
	800	0.49	0.8	1.12	1.43	1.73	2.05	2.36															
	850	0.56	0.91	1.27	1.62	1.97	2.32	2.68															
2 < 3	900 <sup>a</sup>	0.64	1.04	1.43	1.83	2.22	2.61	3.01	3.41														
	950	0.72	1.17	1.61	2.05	2.48	2.92	3.37	3.81	5.21													
	1 000 <sup>a</sup>	0.81	1.3	1.79	2.28	2.76	3.25	3.74	4.23	5.73	6.93												
3 < 5	1 050	0.91	1.45	1.99	2.53	3.06	3.6	4.14	4.68	7.56													
	1 100		1.61	2.2	2.79	3.37	3.97	4.56	5.15	8.22													
	1 150 <sup>a</sup>		1.77	2.42	3.07	3.7	4.35	5	5.64	9.43	10.4												
5 < 10	1 200		1.95	2.66	3.36	4.05	4.76	5.46	6.16	10.9	12												
	1 250		2.14	2.9	3.66	4.41	5.18	5.95	6.71	12	13.7												
	1 300 <sup>a</sup>		2.33	3.16	3.99	4.79	5.62	6.45	7.28	14.1	15.5	16.2											
10 < 15	1 400		2.76	3.72	4.67	5.61	6.57	7.54	8.49	14.4	16	17.6											
	1 500 <sup>a</sup>		3.22	4.32	5.42	6.5	7.6	8.71	9.8	14.4	16.2	18.2											
	1 600		3.73	4.99	6.23	7.46	8.72	9.97	11.2	12.7	14.4	16.2	18.4										
15 < 25	1 700		4.28	5.7	7.11	8.49	9.91	11.3	12.9	14.4	16.2	18.4	20.8										
	1 800 <sup>a</sup>		4.96	6.55	8.13	9.68	11.3	12.9	14.4	16.2	18.4	20.8	23.9										
	1 900			7.39	9.15	10.9	12.7	14.4	16.2	18.4	20.8	23.9	27.1										
20 < 30	2 000 <sup>a</sup>			8.29	10.2	12.2	14.1	16.1	18	19.9	21.9	23.2	26.7										
	2 100			9.26	11.4	13.5	15.7	17.8	20	22.1	24.3	26.8	29.7	30.2									
	2 200			10.3	12.6	15	17.3	19.7	22.1	24.4	26.8	29.4	32.9	33.6									
24 < 40	2 300 <sup>a</sup>			11.4	13.9	16.5	19.1	21.7	24.3	26.8	29.4	32.1	37.8	41.4									
	2 400				15.3	18.1	20.9	23.7	26.6	29.3	32.1	35	38.1	41.1									
	2 500				16.8	19.8	22.9	25.9	29	32	35	38.1	41.1	44.7									
25 < 40	2 600 <sup>a</sup>				18.3	21.6	24.9	28.2	31.5	34.7	38.1	41.1	44.7	48.4									
	2 700				20	23.5	27	30.6	34.2	37.7	41.2	44.5	48.4	51.2									
	2 800				21.7	25.4	29.3	33.1	36.9	40.7	44.5	48.4	52.2	55.4									
40 < 60	2 900					27.5	31.6	35.7	39.8	43.9	48	52.2	56.2	59.8									
	3 000 <sup>a</sup>					29.6	34.1	38.5	42.9	47.2	51.6	56.2	60.4	64.4									
	3 100					31.9	36.6	41.3	46	50.6	55.3	60.4	64.7	69.2									
≥ 60	3 200					34.3	39.3	44.3	49.3	54.2	59.2	64.7	69.2	74.1									
	3 300					36.7	42.1	47.4	52.7	57.9	63.3	68.8	73.9	79.2									
	3 400					39.3	44.9	50.6	56.2	61.8	67.5	73.9	79.2	84.5									
Aspect ratio	3 500						47.9	53.9	59.9	65.8	71.8	78.8	85.8	92.8									
	3 600 <sup>a</sup>						51	57.4	63.7	69.9	76.3	83.8	91.1	98.4									
	3 700						54.3	61	67.7	74.2	80.9	88.8	96.1	104									
a Preferred rationalized diameters	3 800						57.6	64.7	71.7	78.6	85.7	93.3	101	109									
	3 900						61.1	68.5	75.9	83.2	90.7	99.9	108	117									
	4 000 <sup>a</sup>						64.6	72.5	80.3	88	95.8	106	115	124									

2: 1 < 3: 1  
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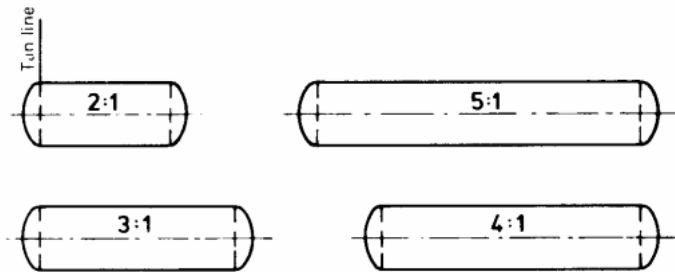
3: 1 &lt; 4: 1

4: 1 < 5: 1  
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a Preferred rationalized diameters



Aspect ratio (i.e. Length between tan lines : diameter)



In calculating volumes of vessels “ellipsoidal” values from Table 4 are used for inside crown radii and inside knuckle radii of domed ends.

Table 2 — Lengths of vessels

Modular plate length	Internal length of vessel $L_i$ , mm																						
	$\frac{1}{4}$	$\frac{1}{2}$	$\frac{3}{4}$	1	1 $\frac{1}{4}$	1 $\frac{1}{2}$	1 $\frac{3}{4}$	2	2 $\frac{1}{4}$	2 $\frac{1}{2}$	3	3 $\frac{1}{2}$	4	4 $\frac{1}{2}$	5	5 $\frac{1}{2}$	6	6 $\frac{1}{2}$	7	7 $\frac{1}{2}$	8		
$D_1$ Lc	610	1 235	1 860	2 480	3 090	3 715	4 340	4 960	5 570	6 195	7 440	8 675	9 920	11 155	12 400	13 635	14 880	16 115	17 360	18 595	19 840		
mm Lt	710	1 335	1 960	2 580	3 190	3 815	4 440	5 060	5 670	6 295	7 540	8 775	10 020	11 255	12 500	13 735	14 980	16 215	17 460	18 695	19 940		
600	1 010	1 635	2 260	2 880	3 490																		
650	1 035	1 660	2 285	2 905	3 515	4 140																	
700	1 060	1 685	2 310	2 930	3 540	4 165																	
750	1 085	1 710	2 335	2 955	3 565	4 190																	
800	1 110	1 735	2 360	2 980	3 590	4 215	4 840																
850	1 135	1 760	2 385	3 005	3 615	4 240	4 865																
900	1 160	1 785	2 410	3 030	3 640	4 265	4 890	5 510															
950	1 185	1 810	2 435	3 055	3 665	4 290	4 915	5 535															
1 000	1 210	1 835	2 460	3 080	3 690	4 315	4 940	5 560															
1 050	1 235	1 860	2 485	3 105	3 715	4 340	4 965	5 585	6 195														
1 100		1 885	2 510	3 130	3 740	4 365	4 990	5 610	6 220														
1 150		1 910	2 535	3 155	3 765	4 390	5 015	5 635	6 245	6 870													
1 200		1 935	2 560	3 180	3 790	4 415	5 040	5 660	6 270	6 895													
1 250		1 960	2 585	3 205	3 815	4 440	5 065	5 685	6 295	6 920													
1 300		1 985	2 610	3 230	3 840	4 465	5 090	5 710	6 320	6 945	8 190												
1 400		2 035	2 660	3 280	3 890	4 515	5 140	5 760	6 370	6 995	8 240												
1 500		2 085	2 710	3 330	3 940	4 565	5 190	5 810	6 420	7 045	8 290	9 525											
1 600		2 135	2 760	3 380	3 990	4 615	5 240	5 860	6 470	7 095	8 340	9 575											
1 700		2 185	2 810	3 430	4 040	4 665	5 290	5 910	6 520	7 145	8 390	9 625											

Table 2 — Lengths of vessels

Modular plate length		Internal length of vessel $L_i$ , mm																					
		$\frac{1}{4}$	$\frac{1}{2}$	$\frac{3}{4}$	1	$1\frac{1}{4}$	$1\frac{1}{2}$	$1\frac{3}{4}$	2	$2\frac{1}{4}$	$2\frac{1}{2}$	3	$3\frac{1}{2}$	4	$4\frac{1}{2}$	5	$5\frac{1}{2}$	6	$6\frac{1}{2}$	7	$7\frac{1}{2}$	8	
$D_i$	Lc	610	1 235	1 860	2 480	3 090	3 715	4 340	4 960	5 570	6 195	7 440	8 675	9 920	11 155	12 400	13 635	14 880	16 115	17 360	18 595	19 840	
	Lt	740	1 365	1 990	2 610	3 220	3 845	4 470	5 090	5 700	6 325	7 570	8 805	10 050	11 285	12 530	13 765	15 010	16 245	17 490	18 725	19 970	
1 800			2 265	2 890	3 510	4 120	4 745	5 370	5 990	6 600	7 225	8 470	9 705	10 950									
1 900				2 940	3 560	4 170	4 795	5 420	6 040	6 650	7 275	8 520	9 755	11 000									
2 000				2 990	3 610	4 220	4 845	5 470	6 090	6 700	7 325	8 570	9 805	11 050									
2 100				3 040	3 660	4 270	4 895	5 520	6 140	6 750	7 375	8 620	9 855	11 100	12 335								
2 200				3 090	3 710	4 320	4 945	5 570	6 190	6 800	7 425	8 670	9 905	11 150	12 385								
2 300				3 140	3 760	4 370	4 995	5 620	6 240	6 850	7 475	8 720	9 955	11 200	12 435	13 680							
2 400					3 810	4 420	5 045	5 670	6 290	6 900	7 525	8 770	10 005	11 250	12 485	13 730							
2 500					3 860	4 470	5 095	5 720	6 340	6 950	7 575	8 820	10 055	11 300	12 535	13 780							
2 600					3 910	4 520	5 145	5 770	6 390	7 000	7 625	8 870	10 105	11 350	12 585	13 830	15 065						
2 700					3 960	4 570	5 195	5 820	6 440	7 050	7 675	8 920	10 155	11 400	12 635	13 880	15 115						
2 800					4 010	4 620	5 245	5 870	6 490	7 100	7 725	8 970	10 205	11 450	12 685	13 930	15 165	16 410					
2 900						4 670	5 295	5 920	6 540	7 150	7 775	9 020	10 255	11 500	12 735	13 980	15 215	16 460					
3 000						4 720	5 345	5 970	6 590	7 200	7 825	9 070	10 305	11 550	12 785	14 030	15 265	16 510	17 745				
3 100						4 770	5 395	6 020	6 640	7 250	7 875	9 120	10 355	11 600	12 835	14 080	15 315	16 560	17 795				
3 200						4 820	5 445	6 070	6 690	7 300	7 925	9 170	10 405	11 650	12 885	14 130	15 365	16 610	17 845				
3 300						4 870	5 495	6 120	6 740	7 350	7 975	9 220	10 455	11 700	12 935	14 180	15 415	16 660	17 895	19 140			
3 400						4 920	5 545	6 170	6 790	7 400	8 025	9 270	10 505	11 750	12 985	14 230	15 465	16 710	17 945	19 190			
3 500							5 595	6 220	6 840	7 450	8 075	9 320	10 555	11 800	13 035	14 280	15 515	16 760	17 995	19 240	20 475		
3 600							5 645	6 270	6 890	7 500	8 125	9 370	10 605	11 850	13 085	14 330	15 565	16 810	18 045	19 290	20 525		
3 700							5 695	6 320	6 940	7 550	8 175	9 420	10 655	11 900	13 135	14 380	15 615	16 860	18 095	19 340	20 575		
3 800							5 745	6 370	6 990	7 600	8 225	9 470	10 705	11 950	13 185	14 430	15 665	16 910	18 145	19 390	20 625	21 870	
3 900							5 795	6 420	7 040	7 650	8 275	9 520	10 755	12 000	13 235	14 480	15 715	16 960	18 195	19 440	20 675	21 920	
4 000							5 845	6 470	7 090	7 700	8 325	9 570	10 805	12 050	13 285	14 530	15 765	17 010	18 245	19 490	20 725	21 970	

Table 3 — Vessel thicknesses and pressure coefficients

Nominal diameter of vessel $D_i$ , mm	$e_{\text{cyl}}$ , mm									
		6	8	10	12.5	15	20	25	30	35
600	$e_{\text{end}}$ $k$	6.084 0.145	8 0.209	10 0.273	12.5 0.351	15 0.43	20 0.584	25 0.736	30 0.886	35 1.033
650	$e_{\text{end}}$ $k$	6.119 0.134	8 0.194	10 0.252	12.5 0.325	15 0.398	20 0.541	25 0.683	30 0.822	35 0.959
700	$e_{\text{end}}$ $k$	6.155 0.125	8.02 0.18	10 0.235	12.5 0.303	15 0.371	20 0.504	25 0.636	30 0.767	35 0.895
750	$e_{\text{end}}$ $k$	6.192 0.117	8.051 0.169	10 0.22	12.5 0.284	15 0.347	20 0.472	25 0.596	30 0.718	35 0.839
800	$e_{\text{end}}$ $k$	6.23 0.11	8.083 0.158	10 0.206	12.5 0.266	15 0.326	20 0.444	25 0.561	30 0.676	35 0.79
850	$e_{\text{end}}$ $k$	6.269 0.104	8.116 0.149	10 0.195	12.5 0.251	15 0.307	20 0.419	25 0.529	30 0.638	35 0.746
900	$e_{\text{end}}$ $k$	6.309 0.098	8.15 0.141	10.03 0.184	12.5 0.238	15 0.291	20 0.396	25 0.501	30 0.604	35 0.706
950	$e_{\text{end}}$ $k$	6.349 0.093	8.185 0.134	10.06 0.175	12.5 0.225	15 0.276	20 0.376	25 0.475	30 0.574	35 0.671
1 000	$e_{\text{end}}$ $k$	6.39 0.088	8.22 0.127	10.09 0.166	12.5 0.214	15 0.263	20 0.358	25 0.453	30 0.546	35 0.639
1 050	$e_{\text{end}}$ $k$	6.432 0.084	8.256 0.121	10.12 0.158	12.5 0.204	15 0.25	20 0.341	25 0.432	30 0.521	35 0.61
1 100	$e_{\text{end}}$ $k$	6.473 0.08	8.294 0.116	10.15 0.151	12.5 0.195	15 0.239	20 0.326	25 0.413	30 0.498	35 0.583
1 150	$e_{\text{end}}$ $k$	6.515 0.077	8.33 0.111	10.19 0.145	12.53 0.187	15 0.229	20 0.313	25 0.395	30 0.478	35 0.559
1 200	$e_{\text{end}}$ $k$	6.557 0.074	8.369 0.106	10.22 0.139	12.56 0.179	15 0.22	20 0.3	25 0.379	30 0.458	35 0.537
1 250	$e_{\text{end}}$ $k$	6.6 0.071	8.409 0.102	10.25 0.133	12.59 0.172	15 0.211	20 0.288	25 0.365	30 0.441	35 0.516
1 300	$e_{\text{end}}$ $k$	6.641 0.068	8.449 0.098	10.29 0.128	12.62 0.166	15 0.203	20 0.277	25 0.351	30 0.424	35 0.497
1 400	$e_{\text{end}}$ $k$	6.714 0.064	8.519 0.092	10.35 0.12	12.68 0.156	15.02 0.191	20 0.26	25 0.329	30 0.398	35 0.466
1 500	$e_{\text{end}}$ $k$	6.796 0.06	8.6 0.086	10.43 0.112	12.74 0.145	15.09 0.178	20 0.243	25 0.308	30 0.372	35 0.436
1 600	$e_{\text{end}}$ $k$	6.876 0.056	8.684 0.081	10.5 0.105	12.81 0.136	15.15 0.167	20 0.228	25 0.289	30 0.349	35 0.409
1 700	$e_{\text{end}}$ $k$	6.953 0.053	8.766 0.076	10.58 0.099	12.88 0.128	15.21 0.157	20 0.215	25 0.272	30 0.329	35 0.386
1 800	$e_{\text{end}}$ $k$	7.028 0.05	8.85 0.072	10.66 0.094	12.95 0.121	15.27 0.149	20 0.203	25 0.257	30 0.311	35 0.365
1 900	$e_{\text{end}}$ $k$	7.099 0.047	8.934 0.068	10.74 0.089	13.02 0.115	15.34 0.141	20.03 0.193	25 0.244	30 0.295	35 0.346

Table 3 — Vessel thicknesses and pressure coefficients

Nominal diameter of vessel $D_i$ mm	$e_{\text{cyl}}$ mm																
		6	8	10	12.5	15	20	25	30	35	40	45	50	55	60	65	70
2 000	$e_{\text{end}}$ $k$	7.165 0.045	9.018 0.065	10.83 0.085	13.1 0.109	15.41 0.134	20.09 0.183	25 0.232	30 0.281	35 0.329	40 0.377	45 0.425	50 0.473	55 0.52	60 0.568	65 0.615	70 0.661
2 100	$e_{\text{end}}$ $k$	7.228 0.043	9.099 0.062	10.91 0.081	13.18 0.104	15.48 0.128	20.15 0.174	25 0.221	30 0.267	35 0.314	40 0.36	45 0.405	50 0.451	55 0.496	60 0.541	65 0.586	70 0.631
2 200	$e_{\text{end}}$ $k$	7.286 0.041	9.18 0.059	10.99 0.077	13.26 0.099	15.55 0.122	20.21 0.167	25 0.211	30 0.255	35 0.3	40 0.344	45 0.387	50 0.431	55 0.474	60 0.517	65 0.56	70 0.603
2 300	$e_{\text{end}}$ $k$	7.341 0.039	9.26 0.056	11.08 0.074	13.34 0.095	15.62 0.117	20.28 0.159	25 0.202	30 0.244	35 0.287	40 0.329	45 0.371	50 0.413	55 0.454	60 0.495	65 0.537	70 0.578
2 400	$e_{\text{end}}$ $k$	7.391 0.037	9.337 0.054	11.16 0.07	13.42 0.091	15.7 0.112	20.34 0.153	25.04 0.194	30 0.234	35 0.275	40 0.315	45 0.356	50 0.396	55 0.436	60 0.475	65 0.515	70 0.554
2 500	$e_{\text{end}}$ $k$	7.435 0.036	9.414 0.052	11.24 0.068	13.5 0.088	15.77 0.107	20.41 0.147	25.1 0.186	30 0.225	35 0.264	40 0.303	45 0.342	50 0.38	55 0.419	60 0.457	65 0.495	70 0.533
2 600	$e_{\text{end}}$ $k$	7.475 0.035	9.486 0.05	11.33 0.065	13.58 0.084	15.85 0.103	20.47 0.141	25.16 0.179	30 0.217	35 0.254	40 0.292	45 0.329	50 0.366	55 0.403	60 0.44	65 0.476	70 0.513
2 700	$e_{\text{end}}$ $k$	7.509 0.033	9.559 0.048	11.41 0.063	13.66 0.081	15.93 0.099	20.54 0.136	25.22 0.172	30 0.209	35 0.245	40 0.281	45 0.317	50 0.353	55 0.388	60 0.424	65 0.459	70 0.494
2 800	$e_{\text{end}}$ $k$	7.537 0.032	9.627 0.046	11.49 0.06	13.75 0.078	16.01 0.096	20.61 0.131	25.28 0.166	30 0.201	35 0.236	40 0.271	45 0.306	50 0.34	55 0.375	60 0.409	65 0.443	70 0.477
2 900	$e_{\text{end}}$ $k$	7.561 0.031	9.693 0.045	11.57 0.058	13.83 0.075	16.09 0.093	20.68 0.127	25.34 0.161	30.05 0.194	35 0.228	40 0.262	45 0.295	50 0.329	55 0.362	60 0.395	65 0.428	70 0.461
3 000	$e_{\text{end}}$ $k$	7.58 0.03	9.756 0.043	11.65 0.056	13.91 0.073	16.17 0.09	20.75 0.122	25.4 0.155	30.1 0.188	35 0.221	40 0.253	45 0.286	50 0.318	55 0.35	60 0.382	65 0.414	70 0.446
3 100	$e_{\text{end}}$ $k$		9.816 0.042	11.73 0.055	14 0.071	16.25 0.087	20.82 0.119	25.47 0.15	30.16 0.182	35 0.214	40 0.245	45 0.276	50 0.308	55 0.339	60 0.37	65 0.401	70 0.432
3 200	$e_{\text{end}}$ $k$		9.874 0.041	11.8 0.053	14.08 0.068	16.33 0.084	20.89 0.115	25.54 0.146	30.22 0.176	35 0.207	40 0.238	45 0.268	50 0.298	55 0.329	60 0.359	65 0.389	70 0.419
3 300	$e_{\text{end}}$ $k$		9.927 0.039	11.88 0.051	14.16 0.066	16.42 0.081	20.97 0.111	25.6 0.141	30.28 0.171	35 0.201	40 0.23	45 0.26	50 0.289	55 0.319	60 0.348	65 0.377	70 0.406
3 400	$e_{\text{end}}$ $k$		9.98 0.038	11.95 0.05	14.24 0.064	16.5 0.079	21.04 0.108	25.67 0.137	30.34 0.166	35.05 0.195	40 0.224	45 0.252	50 0.281	55 0.31	60 0.338	65 0.366	70 0.395
3 500	$e_{\text{end}}$ $k$		10.03 0.037	12.02 0.048	14.33 0.063	16.58 0.077	21.12 0.105	25.74 0.133	30.41 0.161	35.11 0.189	40 0.217	45 0.245	50 0.273	55 0.301	60 0.329	65 0.356	70 0.384
3 600	$e_{\text{end}}$ $k$		10.07 0.036	12.09 0.047	14.41 0.061	16.67 0.075	21.2 0.102	25.81 0.13	30.47 0.157	35.17 0.184	40 0.211	45 0.239	50 0.266	55 0.293	60 0.32	65 0.346	70 0.373
3 700	$e_{\text{end}}$ $k$		10.12 0.035	12.16 0.046	14.49 0.059	16.75 0.073	21.28 0.099	25.87 0.126	30.53 0.153	35.23 0.179	40 0.206	45 0.232	50 0.259	55 0.285	60 0.311	65 0.337	70 0.363
3 800	$e_{\text{end}}$ $k$		10.15 0.034	12.23 0.045	14.57 0.058	16.83 0.071	21.36 0.097	25.95 0.123	30.6 0.149	35.29 0.175	40 0.2	45 0.226	50 0.252	55 0.277	60 0.303	65 0.328	70 0.354
3 900	$e_{\text{end}}$ $k$		10.19 0.033	12.29 0.043	14.65 0.056	16.92 0.069	21.44 0.094	26.02 0.12	30.66 0.145	35.35 0.17	40.06 0.195	45 0.22	50 0.245	55 0.27	60 0.295	65 0.32	70 0.345
4 000	$e_{\text{end}}$ $k$		10.22 0.032	12.35 0.042	14.73 0.055	17 0.067	21.52 0.092	26.09 0.117	30.73 0.141	35.41 0.166	40.12 0.191	45 0.215	50 0.239	55 0.264	60 0.288	65 0.312	70 0.336

Table 4 — Dimensions of domed ends

Inside diameter $D_i$	Inside crown radius $R$			Inside knuckle radius $r$			Inside height $h_i$ ( $0.25 D_i$ )
	Minimum ( $0.75 D_i$ )	“Ellipsoidal” ( $0.8 D_i$ )	Maximum ( $0.95 D_i$ )	Minimum ( $0.125 D_i$ )	“Ellipsoidal” ( $0.146 D_i$ )	Maximum ( $0.1805 D_i$ )	
mm	mm	mm	mm	mm	mm	mm	mm
600 <sup>a</sup>	450	480	570	75	88	103	150
650	488	520	617	82	95	117	163
700	525	560	665	88	102	126	175
750 <sup>a</sup>	563	600	712	94	110	135	188
800	600	640	760	100	117	144	200
850	638	680	807	107	124	153	213
900 <sup>a</sup>	675	720	855	113	131	162	225
950	713	760	902	119	139	171	238
1 000 <sup>a</sup>	750	800	950	125	146	180	250
1 050	788	840	997	132	153	189	263
1 100	825	880	1 045	138	161	198	275
1 150 <sup>a</sup>	863	920	1 092	144	168	207	288
1 200	900	960	1 140	150	175	216	300
1 250	938	1 000	1 187	157	183	225	313
1 300 <sup>a</sup>	975	1 040	1 235	163	190	234	325
1 400	1 050	1 120	1 330	175	204	252	350
1 500 <sup>a</sup>	1 125	1 200	1 425	188	219	270	375
1 600	1 200	1 280	1 520	200	234	288	400
1 700	1 275	1 360	1 615	213	248	306	425
1 800 <sup>a</sup>	1 350	1 440	1 710	225	263	324	450
1 900	1 425	1 520	1 805	238	277	342	475
2 000 <sup>a</sup>	1 500	1 600	1 900	250	292	361	500
2 100	1 575	1 680	1 995	263	307	379	525
2 200	1 650	1 760	2 090	275	321	397	550
2 300 <sup>a</sup>	1 725	1 840	2 185	288	336	415	575
2 400	1 800	1 920	2 280	300	350	433	600
2 500	1 875	2 000	2 375	313	365	451	625
2 600 <sup>a</sup>	1 950	2 080	2 470	325	380	469	650
2 700	2 025	2 160	2 565	338	394	487	675
2 800	2 100	2 240	2 660	350	409	505	700
2 900	2 175	2 320	2 755	363	423	523	725
3 000 <sup>a</sup>	2 250	2 400	2 850	375	438	541	750
3 100	2 325	2 480	2 945	388	453	559	775
3 200	2 400	2 560	3 040	400	467	577	800
3 300	2 475	2 640	3 135	413	482	595	825
3 400	2 550	2 720	3 230	425	496	613	850
3 500	2 625	2 800	3 325	438	511	631	875
3 600 <sup>a</sup>	2 700	2 880	3 420	450	526	649	900
3 700	2 775	2 960	3 515	463	540	667	925
3 800	2 850	3 040	3 610	475	555	685	950
3 900	2 925	3 120	3 705	488	569	703	975
4 000 <sup>a</sup>	3 000	3 200	3 800	500	584	722	1 000

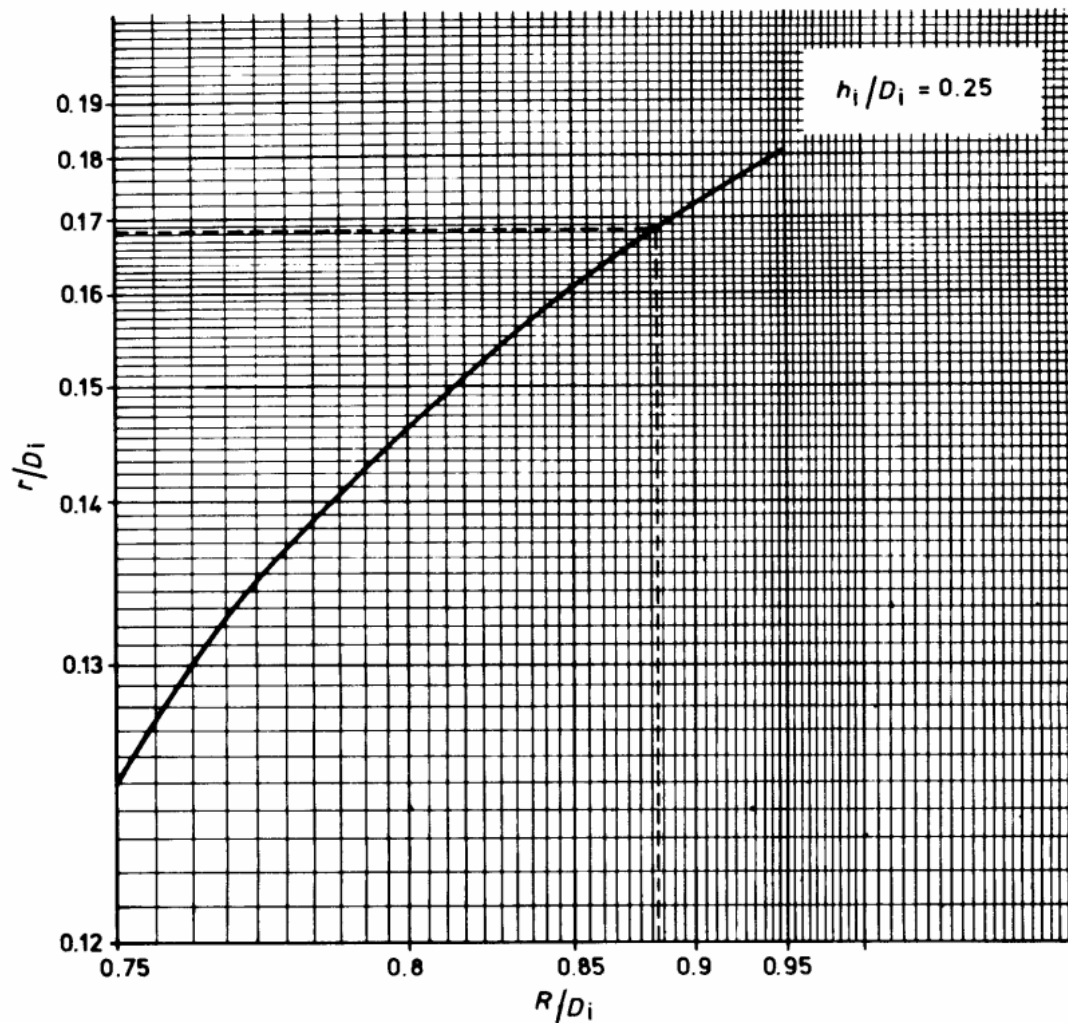
NOTE 1 The manufacturer is free to select any values of  $R$  and  $r$  within the range given to produce the specific depth of head  $h_i$ .

NOTE 2 The “ellipsoidal” values of  $R$  and  $r$  are the particular combinations of radii which produce the nearest approximation to a semi-ellipsoidal shape.

NOTE 3 For inside diameters 600 mm to 1 300 mm inclusive, a permissible variation of  $\pm 12$  mm is applicable with corresponding variation of inside crown radius, inside knuckle radius, and head height (see 5.3.1).

<sup>a</sup> Preferred rationalized diameters

## Appendix A Relationship between inside crown radius $R$ and inside knuckle radius $r$



Graph for determining the appropriate values of  $R$  and  $r$  to give  $h_i/D_i = 0.25$

Example:

If  $D_i = 1\ 600$

$r$  can be between 200 and 288

say  $r = 270$

therefore  $r/D_i = 0.1688$

From graph  $R/D_i = 0.883$

Thus,  $R = 1\ 413$

The equation for this curve is:

$$h_i = R - \sqrt{\left(R - \frac{D_i}{2}\right) \times \left(R + \frac{D_i}{2} - 2r\right)}$$





## Publications referred to

BS 5500, *Unfired fusion welded pressure vessels.*

DD 42, *Recommendations for dimensional tolerances for pressure vessels.*

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