

# Rubber, raw — Determination of the glass transition temperature by differential scanning calorimetry (DSC)

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## National foreword

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A list of organizations represented on PRI/23 can be obtained on request to its secretary.

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**Rubber, raw — Determination of the glass  
transition temperature by differential  
scanning calorimetry (DSC)**

*Caoutchouc brut — Détermination de la température de transition  
vitreuse par analyse calorimétrique différentielle (DSC)*



Reference number  
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## Foreword

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ISO 22768 was prepared by Technical Committee ISO/TC 45, *Rubber and rubber products*, Subcommittee SC 2, *Testing and analysis*.



# Rubber, raw — Determination of the glass transition temperature by differential scanning calorimetry (DSC)

**WARNING** — Persons using this International Standard should be familiar with normal laboratory practice. This standard does not purport to address all of the safety problems, if any, associated with its use. It is the responsibility of the user to establish appropriate safety and health practices and to ensure compliance with any national regulatory conditions.

## 1 Scope

This International Standard specifies a method using a differential scanning calorimeter to determine the glass transition temperature of raw rubber.

## 2 Normative references

The following referenced documents are indispensable for the application of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

ISO/TR 9272:2005, *Rubber and rubber products — Determination of precision for test method standards*

ISO 11357-1:1997, *Plastics — Differential scanning calorimetry (DSC) — Part 1: General principles*

ISO 23529, *Rubber — General procedures for preparing and conditioning test pieces for physical test methods*

## 3 Terms and definitions

For the purposes of this document, the terms and definitions given in ISO 11357-1, together with the following, apply.

### 3.1

#### **glass transition**

reversible change in an amorphous polymer, or in amorphous regions of a partially crystalline polymer, from (or to) a rubbery or viscous condition to (or from) a glassy or hard condition

### 3.2

#### **glass transition temperature**

$T_g$

approximate midpoint of the temperature range over which the glass transition takes place

NOTE For the purposes of this International Standard, the glass transition temperature is defined as the point of inflection of the DSC curve which has been obtained at a heating rate of 20 °C/min (see 12.3).

## 4 Principle

The change in specific heat capacity of the rubber as a function of temperature under a specified inert atmosphere is measured using a differential scanning calorimeter (DSC). The glass transition temperature is determined from the curve thus produced.

## 5 Apparatus and materials

**5.1 Differential scanning calorimeter**, in accordance with ISO 11357-1:1997, 5.1.

The calorimeter should be operated in a room held at standard laboratory temperature. It should be protected from draughts, direct sunlight and sudden temperature changes.

**5.2 Specimen pans**, in accordance with ISO 11357-1:1997, 5.2.

**5.3 Gas supply**, analytical grade, usually nitrogen or helium.

**5.4 Balance**, capable of measuring the specimen mass to an accuracy of  $\pm 0,000$  1 g.

## 6 Test specimen

The test specimen shall be as representative as possible of the sample being examined and shall have a mass of between 0,01 g and 0,02 g.

## 7 Conditioning

Condition the sample to be examined and the test specimen according to ISO 23529.

## 8 Calibration

Calibrate the calorimeter according to the manufacturer's instructions.

The use of suitable analytical grade substances is recommended to check the accuracy of the temperature scale. Ideally substances whose melting points bracket the temperature range of interest should be chosen. *n*-Octane and cyclohexane have been found to be useful. Indium should be used if a higher temperature calibrant is required.

## 9 Procedure

### 9.1 Gas flow rate

The same inert gas flow rate, with a tolerance of  $\pm 10$  %, shall be used throughout the procedure. Flow rates between 10 ml/min and 100 ml/min have been found to be suitable.

### 9.2 Loading the test specimen

Determine the mass of the test specimen to an accuracy of  $\pm 0,001$  g. The same nominal mass shall be used for all determinations. If possible, the specimen shall have a flat surface so as to give good thermal contact with the bottom of the pan.

NOTE Intimate thermal contact between the test specimen and the bottom of the pan is essential for good repeatability.

Place the specimen in the pan, using tweezers, and seal with a lid. Place the sealed pan in the calorimeter using tweezers.

Do not handle the test specimen or the pan with bare hands.



### 9.3 Temperature scan

**9.3.1** Cool the test specimen to a temperature of approximately  $-140\text{ }^{\circ}\text{C}$  at a rate of  $10\text{ }^{\circ}\text{C}/\text{min}$  and hold at this temperature for 1 min.

NOTE A starting temperature of  $-140\text{ }^{\circ}\text{C}$  is required for the determination of rubbers with very low glass transition temperatures, e.g. high-*cis* polybutadiene. For rubbers with higher glass transitions, this temperature is not necessary.

A starting temperature should be chosen so that a stable base line is achieved before the glass transition region, e.g. about  $30\text{ }^{\circ}\text{C}$  to  $40\text{ }^{\circ}\text{C}$  below the expected glass transition temperature.

If the apparatus is not capable of maintaining the specified cooling rate, it should be adjusted to give a rate as close as possible to that specified.

**9.3.2** Perform the temperature scan at a heating rate of  $20\text{ }^{\circ}\text{C}/\text{min}$ , heating until a temperature about  $30\text{ }^{\circ}\text{C}$  above the upper limit of the glass transition range is reached.

NOTE Most instruments can be programmed to carry out the required thermal cycle automatically.

## 10 Expression of results

Determine the glass transition temperature as the inflection point of the transition curve using the instrument software.

NOTE If the glass transition temperature has to be determined directly from the curve, a better indication of the position of the inflection point is given by studying the derivative of the curve.

## 11 Test report

The test report shall include the following:

- a) a reference to this International Standard;
- b) identification of the sample;
- c) the mass of the specimen, in grams;
- d) the type of DSC instrument used;
- e) the type of inert gas and the flow rate;
- f) the calibrants used;
- g) the thermal cycle used;
- h) the  $T_g$  value in degrees Celsius, together with the DSC curve;
- i) the date of the test.

## 12 Precision

### 12.1 General

**12.1.1** The interlaboratory test programme (ITP) for precision evaluation for  $T_g$  was conducted in 2004, using the precision procedures and guidelines as described in ISO/TR 9272:2005 (this revised precision standard was under ballot review at the time of this ITP). Refer to this revised edition for other details and terminology on precision evaluation.

**12.1.2** The ITP was conducted using four rubbers, NdBR (neodymium-catalysed high-*cis* BR), SBR 1502, SBR 1721 and OESSBR. These represent a range of  $T_g$  values from about  $-100\text{ }^{\circ}\text{C}$  to  $-20\text{ }^{\circ}\text{C}$ . Thirty laboratories participated in the ITP and a Type 1 precision was evaluated. A test result represents a single determination or measurement of  $T_g$  using the DSC procedure as specified in this International Standard. Two

measurements of  $T_g$  were conducted on two test days, one week apart. Measurements were conducted at both 10 °C/min and at 20 °C/min on each test day. For precision analysis, all  $T_g$  values were converted to Kelvin. This avoids negative values in the calculation algorithms and, more importantly, it provides mean values (for  $T_g$ ) that are not near zero and thus permits relative precision (in percent) to be more meaningful for all materials; i.e. it avoids large percent values.

**12.1.3** The precision results as determined by this ITP may not be applied to acceptance or rejection testing for any group of materials or products without documentation that the results of this precision evaluation actually apply to the products or materials tested.

## 12.2 Precision results

**12.2.1** Precision results are given in Table 1 for each of the four materials for both 10 °C/min and 20 °C/min. The precision results were obtained using the outlier deletion procedures as described in ISO/TR 9272:2005. Table 1 lists the number of laboratories remaining in the database for the precision evaluation after the deletion of laboratories that had outlier values. General statements for the use of the precision results are cited in 12.2.2. These are given in terms of both the absolute precision,  $r$  or  $R$ , and also for relative precision ( $r$ ) and ( $R$ ).

**12.2.2** Repeatability and reproducibility statements are as follows.

- a) **Repeatability:** The repeatability, or local domain precision, for each of the materials (rubbers) has been established by the values found in Table 1, for each of the materials as listed in the table. Two single test results (obtained by the proper use of the method of this International Standard) that differ by more than the tabulated values for  $r$  in measurement units, and ( $r$ ) in percent, shall be considered as suspect, i.e. to have come from different populations. Such a decision suggests that some appropriate investigative action be taken.
- b) **Reproducibility:** The reproducibility, or global domain precision, for each of the materials has been established by the values found in Table 1, for each of the materials as listed in the table. Two single test results obtained in different laboratories (by the proper use of the method of this International Standard) that differ by more than the tabulated values for  $R$  in measurement units, and ( $R$ ) in percent, shall be considered as suspect, i.e. to have come from different populations. Such a decision suggests that some appropriate investigative action be taken.

**12.2.3 Additional analysis comments:** The last column of Table 1 (the number of laboratories that were included in the database used for the final calculations for precision) indicates that a substantial number of laboratory data values were deleted as outliers. The final number of laboratories for NdBR is low because several laboratories did not submit data. There was some variation in precision improvement among the materials with outlier deletion but, on an overall basis (mean for all four materials), the repeatability limit,  $r$ , was reduced by a reduction factor ( $r_{\text{final}}/r_{\text{orig}}$ ) of 0,56 for 10 °C/min and 0,46 for 20 °C/min, after all repeatability outlier data were deleted. On the same overall basis, the reproducibility limit,  $R$ , was reduced by a reduction factor of 0,71 for both 10 °C/min and 20 °C/min procedures, after all reproducibility data outliers were deleted. Individual laboratories may show poor agreement in repeatability or poor agreement in reproducibility, or both.

There does not appear to be any substantial overall difference in the precision for 10 °C/min vs. 20 °C/min. The repeatability  $r$  for 10 °C/min is 9 % greater than for 20 °C/min, while the reproducibility  $R$  for 10 °C/min is 3 % less than for 20 °C/min.

The final precision, as expressed in Table 1, represents the precision for the majority of laboratories in the ITP; these may be considered as a core group of high quality testing laboratories that constitute a benchmark level of performance for this particular property measurement.

**12.2.4 Bias** is the difference between a measured average test result and a reference or true value for the measurement in question. Reference values do not exist for this test method and therefore bias cannot be evaluated.

Table 1 — Precision data for glass transition temperature

Material	Mean level		Within laboratories			Between laboratories			No. of labs <sup>a</sup>
	°C	K	$s_r$	$r$	( $r$ )	$s_R$	$R$	( $R$ )	
Measurements at 10 °C/min									
1 — NdBR	−106,3	166,7	0,379	1,06	0,64	1,531	4,29	2,57	20
2 — SBR 1502	−54,5	218,5	0,382	1,07	0,49	1,160	3,25	1,49	25
3 — SBR 1721	−34,3	238,7	0,408	1,14	0,48	1,417	3,97	1,66	24
4 — OESSBR	−24,3	248,7	0,245	0,69	0,28	1,449	4,06	1,63	23
Pooled or average value <sup>b</sup>			0,354	0,990	0,473	1,39	3,89	1,84	
Measurements at 20 °C/min									
1 — NdBR	−104,8	168,2	0,273	0,76	0,45	1,418	3,97	2,36	19
2 — SBR 1502	−52,7	220,3	0,462	1,29	0,59	1,431	4,01	1,82	27
3 — SBR 1721	−32,2	240,8	0,372	1,04	0,43	1,164	3,26	1,35	22
4 — OESSBR	−21,9	251,1	0,190	0,53	0,21	1,724	4,83	1,92	24
Pooled or average value <sup>b</sup>			0,324	0,908	0,420	1,43	4,02	1,86	
NOTE 1 Notation used:									
$s_r$ = within-laboratory standard deviation (in measurement units)									
$r$ = repeatability (in measurement units)									
( $r$ ) = repeatability (percent of mean level expressed in K)									
$s_R$ = between-laboratory standard deviation (for total between-laboratory variation in measurement units)									
$R$ = reproducibility (in measurement units)									
( $R$ ) = reproducibility (percent of mean level expressed in K)									
NOTE 2 The relative precision parameters, ( $r$ ) and ( $R$ ), are calculated using values of $T_g$ in K.									
<sup>a</sup> Number of labs after outliers deleted; 3-step analysis; total of 30 labs participated.									
<sup>b</sup> Simple averages calculated.									

### 12.3 Conclusions

The glass transition temperature determined at a heating rate of 20 °C/min is about 2 °C higher than with a heating rate of 10 °C/min. The heating rate of 10 °C/min or 20 °C/min makes no significant difference to the precision. Therefore, in the interests of convenience, the faster rate has been chosen.

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