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Air-cooled air conditioners and air-to-air heat pumps — Testing and calculating methods for seasonal performance factors

Part 1: Cooling seasonal performance factor

bsi.

National foreword

This British Standard is the UK implementation of ISO 16358-1:2013, incorporating corrigendum November 2013.

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INTERNATIONAL STANDARD

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Air-cooled air conditioners and air-to-air heat pumps — Testing and calculating methods for seasonal performance factors —

Part 1:
Cooling seasonal performance factor

Climatiseurs à condenseur à air et pompes à chaleur air/air — Essais et méthodes de calcul des coefficients de performance saisonniers —

Partie 1: Coefficient de performance saisonnier de refroidissement (COPSR)

Reference number
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Foreword

ISO (the International Organization for Standardization) is a worldwide federation of national standards bodies (ISO member bodies). The work of preparing International Standards is normally carried out through ISO technical committees. Each member body interested in a subject for which a technical committee has been established has the right to be represented on that committee. International organizations, governmental and non-governmental, in liaison with ISO, also take part in the work. ISO collaborates closely with the International Electrotechnical Commission (IEC) on all matters of electrotechnical standardization.

The procedures used to develop this document and those intended for its further maintenance are described in the ISO/IEC Directives, Part 1. In particular the different approval criteria needed for the different types of ISO documents should be noted. This document was drafted in accordance with the editorial rules of the ISO/IEC Directives, Part 2. www.iso.org/directives

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The committee responsible for this document is ISO/TC 86, *Refrigeration and air-conditioning*, Subcommittee SC 6, *Testing and rating of air-conditioners and heat pumps*.

The parts of ISO 16358 are given below:

— *Part 1: Cooling seasonal performance factor*

— *Part 2: Heating seasonal performance factor*

— *Part 3: Annual performance factor*

Air-cooled air conditioners and air-to-air heat pumps — Testing and calculating methods for seasonal performance factors —

Part 1:
Cooling seasonal performance factor

1 Scope

1.1 This part of ISO 16358 specifies the testing and calculating methods for seasonal performance factor of equipment covered by ISO 5151, ISO 13253 and ISO 15042.

1.2 This part of ISO 16358 also specifies the seasonal performance test conditions and the corresponding test procedures for determining the seasonal performance factor of equipment, as specified in 1.1, under mandatory test conditions and is intended for use only in marking, comparison, and certification purposes. For the purposes of this part of ISO 16358, the rating conditions are those specified under T1 in the reference standards in 1.1. The procedures in this part of ISO 16358 may be used for other temperature conditions.

1.3 This part of ISO 16358 does not apply to the testing and rating of:

a) water-source heat pumps or water-cooled air conditioners;

b) portable units having a condenser exhaust duct;

c) individual assemblies not constituting a complete refrigeration system; or

d) equipment using the absorption refrigeration cycle.

2 Normative references

The following documents, in whole or in part, are normatively referenced in this document and are indispensable for its application. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

ISO 5151, *Non-ducted air conditioners and heat pumps — Testing and rating for performance*

ISO 13253, *Ducted air-conditioners and air-to-air heat pumps — Testing and rating for performance*

ISO 15042, *Multiple split-system air-conditioners and air-to-air heat pumps — Testing and rating for performance*

3 Terms and definitions

For the purposes of this document, the terms and definitions given in ISO 5151, ISO 13253, ISO 15042 and the following apply.

3.1
defined cooling load, L_C
heat defined as cooling demand for a given outdoor temperature

3.2
cooling seasonal total load
CSTL
total annual amount of heat that is removed from the indoor air when the equipment is operated for cooling in active mode

3.3
cooling seasonal energy consumption
CSEC
total annual amount of energy consumed by the equipment when it is operated for cooling in active mode

3.4
cooling seasonal performance factor
CSPF
ratio of the total annual amount of heat that the equipment can remove from the indoor air when operated for cooling in active mode to the total annual amount of energy consumed by the equipment during the same period

3.5
part load factor
PLF
ratio of the performance when the equipment is cyclically operated to the performance when the equipment is continuously operated, at the same temperature and humidity conditions

3.6
degradation coefficient, C_D
coefficient that indicates efficiency loss caused by cyclic operation

3.7
fixed capacity unit
equipment which does not have possibility to change its capacity

Note 1 to entry: This definition applies to each cooling and heating operation individually.

3.8
two (2)-stage capacity unit
equipment where the capacity is varied by two steps

Note 1 to entry: This definition applies to each cooling and heating operation individually.

3.9
multi-stage capacity unit
equipment where the capacity is varied by three or four steps

Note 1 to entry: This definition applies to each cooling and heating operation individually.

3.10
variable capacity unit
equipment where the capacity is varied by five or more steps to represent continuously variable capacity

Note 1 to entry: This definition applies to each cooling and heating operation individually.

3.11
cooling full-load operation
operation with the equipment and controls configured for the maximum continuous refrigeration capacity specified by the manufacturer and allowed by the unit controls

Note 1 to entry: Unless otherwise regulated by the automatic controls of the equipment, all indoor units and compressors shall be functioning during the full-load operation.

3.12
minimum-load operation
operation of the equipment and controls at minimum continuous refrigeration capacity

Note 1 to entry: All indoor units shall be functioning during the minimum-load operation.

3.13
standard cooling full capacity
cooling capacity at T1 at full-load operating conditions

3.14
standard cooling full power input
electric power input at T1 at full-load operating conditions

3.15
standard cooling half capacity
capacity which is 50 % of cooling full capacity at T1 condition with all indoor units functioning

3.16
standard cooling half power input
electric power input when operated at 50 % of cooling full capacity at T1 condition with all indoor units functioning

3.17
standard cooling minimum capacity
capacity at T1 condition at the minimum-load operation

3.18
standard cooling minimum power input
electric power input at T1 condition at the minimum-load operation

3.19
total cooling seasonal performance factor
TCSPF
ratio of the total annual amount of heat that the equipment can remove from the indoor air to the total annual amount of energy consumed by the equipment, including the active, inactive and disconnected modes

3.20
active mode
mode corresponding to the hours with a cooling demand of the building and whereby the cooling function of the unit is switched on

3.21
inactive mode
mode corresponding to the hours when the unit is not operating to meet cooling demand

Note 1 to entry: This mode may include the operation of a crankcase heater.

3.22
disconnected mode
mode corresponding to the hours when the unit is electrically disconnected from the main power supply

Note 1 to entry: Power consumption is zero.

4 Symbols

Symbol	Description	Unit
C_{CSE}	cooling seasonal energy consumption (CSEC)	Wh
$E_{\mathrm{ER}}(t)$	energy efficiency ratio (EER) at continuous outdoor temperature t	W/W

Symbol	Description	Unit
$E_{\mathrm{ER}}(t_j)$	energy efficiency ratio (EER) at outdoor temperature t_j	W/W
$E_{\mathrm{ER,\ ful}}(t_b)$	energy efficiency ratio (EER) when cooling load is equal to cooling full capacity	W/W
$E_{\mathrm{ER,\ haf}}(t_c)$	energy efficiency ratio (EER) when cooling load is equal to cooling half capacity	W/W
$E_{\mathrm{ER,\ hf}}(t_j)$	energy efficiency ratio (EER) in variable operation between half and full capacity at outdoor temperature t_j	W/W
$E_{\mathrm{ER,\ mh}}(t_j)$	energy efficiency ratio (EER) in variable operation between minimum and half capacity at outdoor temperature t_j	W/W
$E_{\mathrm{ER,\ min}}(t_p)$	energy efficiency ratio (EER) when cooling load is equal to cooling minimum capacity	W/W
F_{CSP}	cooling seasonal performance factor (CSPF)	–
$F_{\mathrm{PL}}(t_j)$	part load factor (PLF) at outdoor temperature t_j	–
F_{TCSP}	total cooling seasonal performance factor (TCSPF)	–
L_{CST}	cooling seasonal total load (CSTL)	Wh
$L_c(t_j)$	defined cooling load at outdoor temperature t_j	W
n_j	bin hours	h
k, p, n, m	number of temperature bins	–
$P(t)$	cooling power input calculated by equation of $P(t_j)$ at continuous outdoor temperature t	W
$P(t_j)$	cooling power input applicable to any capacity at outdoor temperature t_j	W
$P_{\mathrm{ful}}(t_j)$	cooling full power input at outdoor temperature t_j	W
$P_{\mathrm{ful}}(35)$	cooling full power input at T1 temperature condition	W
$P_{\mathrm{ful}}(29)$	cooling full power input at outdoor temperature 29 °C	W
$P_{\mathrm{haf}}(t_j)$	cooling half power input at outdoor temperature t_j	W
$P_{\mathrm{haf}}(35)$	cooling half power input at T1 temperature condition	W
$P_{\mathrm{haf}}(29)$	cooling half power input at outdoor temperature 29 °C	W
$P_{\mathrm{hf}}(t_j)$	cooling power input in variable operation between half and full capacity at outdoor temperature t_j	W
$P_{\mathrm{mf}}(t_j)$	cooling power input in second stage cyclic operation between minimum and full capacity at outdoor temperature t_j	W
$P_{\mathrm{mh}}(t_j)$	cooling power input in variable operation between minimum and half capacity at outdoor temperature t_j	W
$P_{\mathrm{min}}(t_j)$	cooling minimum power input at outdoor temperature t_j	W
$P_{\mathrm{min}}(35)$	cooling minimum power input at T1 temperature condition	W
$P_{\mathrm{min}}(29)$	cooling minimum power input at outdoor temperature 29 °C	W
t	general continuous outdoor temperature	°C
t_j	outdoor temperature corresponding to each temperature bin	°C
t_b	outdoor temperature when cooling load is equal to cooling full capacity	°C
t_c	outdoor temperature when cooling load is equal to cooling half capacity	°C
t_p	outdoor temperature when cooling load is equal to cooling minimum capacity	°C
$X(t_j)$	ratio of load to capacity at outdoor temperature t_j	–
$X_{\mathrm{hf}}(t_j)$	ratio of excess capacity over load to capacity difference between half and full capacity at outdoor temperature t_j	–

Symbol	Description	Unit
$X_{\mathrm{mf}}(t_{\mathrm{j}})$	ratio of excess capacity over load to capacity difference between minimum and full capacity at outdoor temperature t_{j}	–
$X_{\mathrm{mh}}(t_{\mathrm{j}})$	ratio of excess capacity over load to capacity difference between minimum and half capacity at outdoor temperature t_{j}	–
$\phi(t)$	cooling capacity calculated by equation of $\phi(t_{\mathrm{j}})$ at continuous outdoor temperature t	W
$\phi(t_{\mathrm{j}})$	cooling capacity applicable to any capacity at outdoor temperature t_{j}	W
$\phi_{\mathrm{ful}}(t_{\mathrm{j}})$	cooling full capacity at outdoor temperature t_{j}	W
$\phi_{\mathrm{ful}}(35)$	cooling full capacity at T1 temperature condition	W
$\phi_{\mathrm{ful}}(29)$	cooling full capacity at outdoor temperature 29 °C	W
$\phi_{\mathrm{haf}}(t_{\mathrm{j}})$	cooling half capacity at outdoor temperature t_{j}	W
$\phi_{\mathrm{haf}}(35)$	cooling half capacity at T1 temperature condition	W
$\phi_{\mathrm{haf}}(29)$	cooling half capacity at outdoor temperature 29 °C	W
$\phi_{\mathrm{min}}(t_{\mathrm{j}})$	cooling minimum capacity at outdoor temperature t_{j}	W
$\phi_{\mathrm{min}}(35)$	cooling minimum capacity at T1 temperature condition	W
$\phi_{\mathrm{min}}(29)$	cooling minimum capacity at outdoor temperature 29 °C	W

5 Tests

5.1 General

These tests are additional to those in ISO 5151, ISO 13253 and ISO 15042.

The accuracy of the instruments used for tests shall conform to the test methods and uncertainties of measurements specified in ISO 5151, ISO 13253 and ISO 15042.

5.2 Test conditions

Temperature and humidity conditions as well as default values for calculation shall be as specified in Table 1.

Table 1 — Temperature and humidity conditions and default values for cooling at T1 moderate climate condition of ISO 5151, ISO 13253 and ISO 15042

Test	Characteristics	Fixed	Two-stage	Multi-stage	Variable	Default value
Standard cooling capacity Indoor DB 27°C WB 19°C Outdoor DB 35°C WB 24°C	Full capacity $\phi_{\mathrm{ful}}(35)$ (W)	■	■	■	■	—
	Full power input $P_{\mathrm{ful}}(35)$ (W)					
	Half capacity $\phi_{\mathrm{haf}}(35)$ (W)	—	—	○	■	$\phi_{\mathrm{haf}}(29)/1{,}077$
	Half power input $P_{\mathrm{haf}}(35)$ (W)					$P_{\mathrm{haf}}(29)/0{,}914$
	Minimum capacity $\phi_{\mathrm{min}}(35)$ (W)	—	○	○	○	$\phi_{\mathrm{min}}(29)/1{,}077$
	Minimum power input $P_{\mathrm{min}}(35)$ (W)					$P_{\mathrm{min}}(29)/0{,}914$

■ required test.

○ optional test.

NOTE 1 If the minimum capacity test is measured, min(29) test is conducted first. Min(35) test may be measured or may be calculated by using default value.

NOTE 2 Voltage(s) and frequency(ies) are as given in the three referenced standards.

Table 1 *(continued)*

Test	Characteristics		Fixed	Two-stage	Multi-stage	Variable	Default value
Low temperature cooling capacity Indoor DB 27°C WB 19°C Outdoor DB 29°C WB 19°C	Full capacity $\phi_{\mathrm{ful}}(29)$ (W)		■	■	■	—	1,077 × $\phi_{\mathrm{ful}}(35)$
	Full power input $P_{\mathrm{ful}}(29)$ (W)						0,914 × $P_{\mathrm{ful}}(35)$
	Half capacity $\phi_{\mathrm{haf}}(29)$ (W)		—	—	■	○	1,077 × $\phi_{\mathrm{haf}}(35)$
	Half power input $P_{\mathrm{haf}}(29)$ (W)						0,914 × $P_{\mathrm{haf}}(35)$
	Minimum capacity $\phi_{\mathrm{min}}(29)$ (W)		—	■	○	○	—
	Minimum power input $P_{\mathrm{min}}(29)$ (W)						
Low humidity and cyclic cooling Indoor DB 27°C WB 16°C or lower Outdoor DB 29°C WB -	Degradation coefficient C_D	Full capacity	○	—	—	—	0,25
		Half capacity	—	—	○	—	0,25
		Minimum capacity	—	○	○	—	0,25

■ required test.

○ optional test.

NOTE 1 If the minimum capacity test is measured, min(29) test is conducted first. Min(35) test may be measured or may be calculated by using default value.

NOTE 2 Voltage(s) and frequency(ies) are as given in the three referenced standards.

5.3 Test methods

5.3.1 Standard cooling capacity tests

The standard cooling capacity tests shall be conducted in accordance with Annex A of ISO 5151 and Annex B of ISO 13253 and ISO 15042. The cooling capacity and effective power input shall be measured during the standard cooling capacity tests.

The half capacity test shall be conducted at 50 % of full load operation. The test tolerance shall be ± 5 % of full load capacity for continuously variable equipment. For multi-stage equipment, if 50 % capacity is not achievable, then the tests shall be conducted at the next step above 50 %.

The minimum capacity test shall be conducted at the lowest capacity control setting which allows steady-state operation of the equipment at the given test conditions.

If the minimum capacity tests are conducted, but if the required uncertainty of measurement specified in ISO 5151, ISO 13253 and ISO 15042 cannot be achieved, the alternative method of calculation shall be used. (Refer to 6.6.4 and 6.7.4.)

The manufacturer shall provide information on how to set the capacity if requested by the testing laboratories.

5.3.2 Low temperature cooling capacity tests

The low temperature cooling capacity test shall be conducted in accordance with Annex A of ISO 5151 and Annex B of ISO 13253 and ISO 15042. If the test is not conducted, default values as given in Table 1 shall be used.

The half capacity test shall be conducted at 50 % of full load operation. The test tolerance shall be ± 5 % of full load capacity for continuously variable equipment. For multi-stage equipment, if 50 % capacity is not achievable, then the tests shall be conducted at the next step above 50 %.

The minimum capacity test shall be conducted at the lowest capacity control setting which allows steady-state operation of the equipment at the given test conditions.

If the minimum capacity tests are conducted, but if the required uncertainty of measurement specified in ISO 5151, ISO 13253 and ISO 15042 cannot be achieved, the alternative method of calculation shall be used. (Refer to 6.6.4 and 6.7.4.)

The manufacturer shall provide information on how to set the capacity if requested by the testing laboratories.

5.3.3 Low humidity cooling test and cyclic cooling test

The low humidity cooling test and cyclic cooling test shall be conducted in accordance with Annex C. If the test is not conducted, default values as given in Table 1 shall be used.

6 Calculations

6.1 Cooling seasonal performance factor (CSPF) and total cooling seasonal performance factor (TCSPF)

The cooling seasonal performance factor (CSPF), F_{CSP}, of the equipment shall be calculated by Formula (1).

$$F_{\mathrm{CSP}} = \frac{L_{\mathrm{CST}}}{C_{\mathrm{CSE}}} \tag{1}$$

In case of calculating the total cooling seasonal performance factor (TCSPF), refer to Annex B.

6.2 Defined cooling load

The defined cooling load shall be represented by a value and the assumption that it is linearly changing depending on the change in outdoor temperature.

Defined cooling load which shall be used is shown in Table 2.

Table 2 — Defined cooling load

Parameter	Load zero (0)	Load 100 %
Cooling load (W)	0	$\phi_{\mathrm{ful}}(t_{100})$
Temperature (°C)	t_0	t_{100}

where t_{100} is the outdoor temperature at 100 % load and t_0 is the outdoor temperature at 0 % load.

Reference values of defined cooling load to be used shall be as follows:

t_0 = 20 °C and t_{100} = 35 °C

In case of setting other cooling load, refer to the setting method as described in Annex D.

Defined cooling load $L_{\mathrm{c}}(t_{\mathrm{j}})$ at outdoor temperature t_{j}, which is necessary to calculate the cooling seasonal energy consumption, shall be determined by Formula (2).

$$L_{\mathrm{c}}(t_{\mathrm{j}}) = \phi_{\mathrm{ful}}(t_{100}) \times \frac{t_{\mathrm{j}} - t_0}{t_{100} - t_0} \tag{2}$$

where $\phi_{\mathrm{ful}}(t_{100})$ is the cooling capacity at t_{100} at full-load operating conditions.

6.3 Outdoor temperature bin distribution for cooling

Table 3 shows the reference outdoor temperature bin distribution.

Cooling seasonal performance factor (CSPF) shall be calculated at the reference climate condition in Table 3.

The calculation of cooling seasonal performance factor may also be done for other climate conditions.

Table 3 — Reference outdoor temperature bin distribution

Bin number j	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	Total
Outdoor temperature t_j °C	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	—
Fractional bin hours	0,055	0,076	0,091	0,108	0,116	0,118	0,116	0,100	0,083	0,066	0,041	0,019	0,006	0,003	0,002	
Bin hours n_j	n_1	n_2	n_3	n_4	n_5	n_6	n_7	n_8	n_9	n_{10}	n_{11}	n_{12}	n_{13}	n_{14}	n_{15}	—
Reference bin hours (n_j) h	100	139	165	196	210	215	210	181	150	120	75	35	11	6	4	1 817

Bin hours of each outdoor temperature may be calculated by multiplying the fractional bin hours by the total annual cooling hours if the fractional bin hours are applicable.

In case of setting other outdoor temperature bin distribution, refer to the setting method as described in Annex D.

6.4 Cooling seasonal characteristics of fixed capacity units

Operational performance at each test, which is used for calculation of seasonal performance factor, shall be in accordance with Table 1.

6.4.1 Capacity characteristics against outdoor temperature

Capacity $\phi_{\text{ful}}(t_j)$ (W) of the equipment when it is operated for cooling at outdoor temperature t_j linearly changes depending on outdoor temperatures as shown in Figure A.1 in Annex A, and it is determined by Formula (3) from two characteristics, one at 35 °C and the other at 29 °C.

$$\phi_{\text{ful}}(t_j)=\phi_{\text{ful}}(35)+\frac{\phi_{\text{ful}}(29)-\phi_{\text{ful}}(35)}{35-29}\times(35-t_j) \qquad (3)$$

6.4.2 Power input characteristics against outdoor temperature

Power input $P_{\text{ful}}(t_j)$ (W) of the equipment when it is operated for cooling at outdoor temperature t_j linearly changes depending on outdoor temperatures as shown in Figure A.1 in Annex A, and it is determined by Formula (4) from two characteristics, one at 35 °C and the other at 29 °C.

$$P_{\text{ful}}(t_j)=P_{\text{ful}}(35)+\frac{P_{\text{ful}}(29)-P_{\text{ful}}(35)}{35-29}\times(35-t_j) \qquad (4)$$

6.4.3 Calculation of cooling seasonal total load (CSTL)

Cooling seasonal total load (CSTL), L_{CST}, shall be determined using Formula (5) from the total sum of cooling load at each outdoor temperature t_j multiplied by bin hours n_j.

$$L_{\text{CST}}=\sum_{j=1}^{m}L_c(t_j)\times n_j+\sum_{j=m+1}^{n}\phi_{\text{ful}}(t_j)\times n_j \qquad (5)$$

a) In the range of $L_c(t_j) \leq \phi_{\text{ful}}(t_j)$ (j = 1 to m):

$L_c(t_j)$ shall be calculated by Formula (2).

b) In the range of $L_c(t_j) > \phi_{\text{ful}}(t_j)$ (j = m+1 to n):

$\phi_{\text{ful}}(t_j)$ shall be calculated by Formula (3).

6.4.4 Calculation of cooling seasonal energy consumption (CSEC)

Cooling seasonal energy consumption (CSEC), C_{CSE}, shall be determined using Formula (6) from the total sum of cooling energy consumption at each outdoor temperature t_j.

$$C_{\mathrm{CSE}} = \sum_{j=1}^{n} X(t_j) \times P_{\mathrm{ful}}(t_j) \times \frac{n_j}{F_{\mathrm{PL}}(t_j)} \tag{6}$$

Operation factor $X(t_j)$ shall be calculated by Formula (7).

$$X(t_j) = \frac{L_c(t_j)}{\phi(t_j)} \tag{7}$$

In the case of $L_c(t_j) > \phi(t_j)$, $X(t_j) = 1$.

Part load factor (PLF), $F_{\mathrm{PL}}(t_j)$, caused by the equipment when it is cyclically operated at outdoor temperature t_j, shall be determined by Formula (8) using degradation coefficient C_D.

$$F_{\mathrm{PL}}(t_j) = 1 - C_D\ (1 - X(t_j)) \tag{8}$$

a) Cyclic operation ($L_c(t_j) \leq \phi_{\mathrm{ful}}(t_j)$):

In Formula (6), $X(t_j)$ shall be calculated by Formula (7).

In Formula (7), $\phi(t_j) = \phi_{\mathrm{ful}}(t_j)$.

b) Full capacity operation ($L_c(t_j) > \phi_{\mathrm{ful}}(t_j)$):

In Formula (6), $X(t_j) = F_{\mathrm{PL}}(t_j) = 1$.

6.5 Cooling seasonal characteristics of two-stage capacity units

Coefficients specified in Table 1 may be used for each characteristic.

6.5.1 Capacity characteristics against outdoor temperature

Capacity $\phi_{\mathrm{ful}}(t_j)$ (W) of the equipment when it is operated for cooling full capacity at outdoor temperature t_j shall be defined by Formula (3).

Capacity $\phi_{\mathrm{min}}(t_j)$ (W) of the equipment when it is operated for cooling minimum capacity at outdoor temperature t_j shall be defined by Formula (9).

$$\phi_{\mathrm{min}}(t_j) = \phi_{\mathrm{min}}(35) + \frac{\phi_{\mathrm{min}}(29) - \phi_{\mathrm{min}}(35)}{35 - 29} \times (35 - t_j) \tag{9}$$

6.5.2 Power input characteristics against outdoor temperature

Power input $P_{\mathrm{ful}}(t_j)$ (W) of the equipment when it is operated for cooling full capacity at outdoor temperature t_j shall be defined by Formula (4).

Power input $P_{\mathrm{min}}(t_j)$ (W) of the equipment when it is operated for cooling minimum capacity at outdoor temperature t_j shall be defined by Formula (10).

$$P_{\mathrm{min}}(t_j) = P_{\mathrm{min}}(35) + \frac{P_{\mathrm{min}}(29) - P_{\mathrm{min}}(35)}{35 - 29} \times (35 - t_j) \tag{10}$$

6.5.3 Calculation of cooling seasonal total load (CSTL)

Formula (5) in 6.4.3 shall be used.

6.5.4 Calculation of cooling seasonal energy consumption (CSEC)

Cooling seasonal energy consumption (CSEC), C_{CSE}, shall be calculated by Formula (11).

$$C_{\mathrm{CSE}}=\sum_{\mathrm{j}=1}^{k}\frac{X(t_{\mathrm{j}})\times P_{\mathrm{min}}(t_{\mathrm{j}})\times n_{\mathrm{j}}}{F_{\mathrm{PL}}(t_{\mathrm{j}})}+\sum_{\mathrm{j}=k+1}^{m}P_{\mathrm{mf}}(t_{\mathrm{j}})\times n_{\mathrm{j}}+\sum_{\mathrm{j}=m+1}^{n}P_{\mathrm{ful}}(t_{\mathrm{j}})\times n_{\mathrm{j}} \tag{11}$$

Relation of cooling capacity characteristics and power input characteristics to cooling load at outdoor temperature t_{j} is shown in Figure A.2 in Annex A.

a) First stage cyclic operation ($L_{\mathrm{c}}(t_{\mathrm{j}}) \le \phi_{\mathrm{min}}(t_{\mathrm{j}})$, j = 1 to k):

In Formula (11), $X(t_{\mathrm{j}})$ shall be calculated by Formula (7).

In Formula (7), $\phi(t_{\mathrm{j}}) = \phi_{\mathrm{min}}(t_{\mathrm{j}})$.

b) Second stage cyclic operation ($\phi_{\mathrm{min}}(t_{\mathrm{j}}) < L_{\mathrm{c}}(t_{\mathrm{j}}) \le \phi_{\mathrm{ful}}(t_{\mathrm{j}})$, j = k+1 to m):

$$P_{\mathrm{mf}}(t_{\mathrm{j}})=X_{\mathrm{mf}}(t_{\mathrm{j}})\times P_{\mathrm{min}}(t_{\mathrm{j}})+\left(1-X_{\mathrm{mf}}(t_{\mathrm{j}})\right)\times P_{\mathrm{ful}}(t_{\mathrm{j}}) \tag{12}$$

$$X_{\mathrm{mf}}(t_{\mathrm{j}})=\frac{\phi_{\mathrm{ful}}(t_{\mathrm{j}})-L_{\mathrm{c}}(t_{\mathrm{j}})}{\phi_{\mathrm{ful}}(t_{\mathrm{j}})-\phi_{\mathrm{min}}(t_{\mathrm{j}})} \tag{13}$$

c) Full capacity operation ($L_{\mathrm{c}}(t_{\mathrm{j}}) > \phi_{\mathrm{ful}}(t_{\mathrm{j}})$, j = m+1 to n):

$P_{\mathrm{ful}}(t_{\mathrm{j}})$ shall be calculated by Formula (4).

6.6 Cooling seasonal characteristics of multi-stage capacity units

6.6.1 Capacity characteristics against outdoor temperature

Capacities $\phi_{\mathrm{ful}}(t_{\mathrm{j}})$ and $\phi_{\mathrm{min}}(t_{\mathrm{j}})$ (W) of the equipment when it is operated for cooling at outdoor temperature t_{j} are shown in Figure A.3 in Annex A and shall be determined by Formulae (3) and (9), respectively.

Formula (14) shows cooling half capacity characteristics at outdoor temperature t_{j}.

$$\phi_{\mathrm{haf}}(t_{\mathrm{j}})=\phi_{\mathrm{haf}}(35)+\frac{\phi_{\mathrm{haf}}(29)-\phi_{\mathrm{haf}}(35)}{35-29}\times(35-t_{\mathrm{j}}) \tag{14}$$

6.6.2 Power input characteristics against outdoor temperature

Power input $P_{\mathrm{ful}}(t_{\mathrm{j}})$ and $P_{\mathrm{min}}(t_{\mathrm{j}})$ (W) of the equipment when it is operated for cooling at outdoor temperature t_{j} shall be determined by Formulae (4) and (10), respectively.

Formula (15) shows cooling half power input at outdoor temperature t_{j}.

$$P_{\mathrm{haf}}(t_{\mathrm{j}})=P_{\mathrm{haf}}(35)+\frac{P_{\mathrm{haf}}(29)-P_{\mathrm{haf}}(35)}{35-29}\times(35-t_{\mathrm{j}}) \tag{15}$$

6.6.3 Calculation of cooling seasonal total load (CSTL)

Formula (5) in 6.4.3 shall be used.

6.6.4 Calculation of cooling seasonal energy consumption (CSEC)

When the minimum capacity data are available, then the cooling seasonal energy consumption (CSEC), C_{CSE}, shall be calculated by Formula (16).

$$C_{\mathrm{CSE}} = \sum_{\mathrm{j}=1}^{k} \frac{X(t_{\mathrm{j}}) \times P_{\mathrm{min}}(t_{\mathrm{j}}) \times n_{\mathrm{j}}}{F_{\mathrm{PL}}(t_{\mathrm{j}})} + \sum_{\mathrm{j}=k+1}^{p} P_{\mathrm{mh}}(t_{\mathrm{j}}) \times n_{\mathrm{j}} + \sum_{\mathrm{j}=p+1}^{m} P_{\mathrm{hf}}(t_{\mathrm{j}}) \times n_{\mathrm{j}} + \sum_{\mathrm{j}=m+1}^{n} P_{\mathrm{ful}}(t_{\mathrm{j}}) \times n_{\mathrm{j}} \tag{16}$$

Relation of cooling capacity and power input characteristics to cooling load at outdoor temperature t_{j} is shown in Figure A.3 in Annex A.

a) First stage cyclic operation ($L_{\mathrm{c}}(t_{\mathrm{j}}) \le \phi_{\mathrm{min}}(t_{\mathrm{j}})$, j = 1 to k):

In Formula (16), $X(t_{\mathrm{j}})$ shall be calculated by Formula (7).

In Formula (7), $\phi(t_{\mathrm{j}}) = \phi_{\mathrm{min}}(t_{\mathrm{j}})$.

b) Second stage cyclic operation ($\phi_{\mathrm{min}}(t_{\mathrm{j}}) < L_{\mathrm{c}}(t_{\mathrm{j}}) \le \phi_{\mathrm{haf}}(t_{\mathrm{j}})$, j = k+1 to p):

$$P_{\mathrm{mh}}(t_{\mathrm{j}}) = X_{\mathrm{mh}}(t_{\mathrm{j}}) \times P_{\mathrm{min}}(t_{\mathrm{j}}) + \left(1 - X_{\mathrm{mh}}(t_{\mathrm{j}})\right) \times P_{\mathrm{haf}}(t_{\mathrm{j}}) \tag{17}$$

$$X_{\mathrm{mh}}(t_{\mathrm{j}}) = \frac{\phi_{\mathrm{haf}}(t_{\mathrm{j}}) - L_{\mathrm{c}}(t_{\mathrm{j}})}{\phi_{\mathrm{haf}}(t_{\mathrm{j}}) - \phi_{\mathrm{min}}(t_{\mathrm{j}})} \tag{18}$$

c) Third stage cyclic operation ($\phi_{\mathrm{haf}}(t_{\mathrm{j}}) < L_{\mathrm{c}}(t_{\mathrm{j}}) \le \phi_{\mathrm{ful}}(t_{\mathrm{j}})$, j = p+1 to m):

$$P_{\mathrm{hf}}(t_{\mathrm{j}}) = X_{\mathrm{hf}}(t_{\mathrm{j}}) \times P_{\mathrm{haf}}(t_{\mathrm{j}}) + \left(1 - X_{\mathrm{hf}}(t_{\mathrm{j}})\right) \times P_{\mathrm{ful}}(t_{\mathrm{j}}) \tag{19}$$

$$X_{\mathrm{hf}}(t_{\mathrm{j}}) = \frac{\phi_{\mathrm{ful}}(t_{\mathrm{j}}) - L_{\mathrm{c}}(t_{\mathrm{j}})}{\phi_{\mathrm{ful}}(t_{\mathrm{j}}) - \phi_{\mathrm{haf}}(t_{\mathrm{j}})} \tag{20}$$

d) Full capacity operation ($L_{\mathrm{c}}(t_{\mathrm{j}}) > \phi_{\mathrm{ful}}(t_{\mathrm{j}})$, j = m+1 to n):

$P_{\mathrm{ful}}(t_{\mathrm{j}})$ shall be calculated by Formula (4).

When the minimum capacity data are not available, then the cooling seasonal energy consumption (CSEC), C_{CSE}, shall be calculated alternatively by Formula (21).

$$C_{\mathrm{CSE}} = \sum_{\mathrm{j}=1}^{p} \frac{X(t_{\mathrm{j}}) \times P_{\mathrm{haf}}(t_{\mathrm{j}}) \times n_{\mathrm{j}}}{F_{\mathrm{PL}}(t_{\mathrm{j}})} + \sum_{\mathrm{j}=p+1}^{m} P_{\mathrm{hf}}(t_{\mathrm{j}}) \times n_{\mathrm{j}} + \sum_{\mathrm{j}=m+1}^{n} P_{\mathrm{ful}}(t_{\mathrm{j}}) \times n_{\mathrm{j}} \tag{21}$$

a) First stage cyclic operation ($L_{\mathrm{c}}(t_{\mathrm{j}}) \le \phi_{\mathrm{haf}}(t_{\mathrm{j}})$, j = 1 to p):

In Formula (21), $X(t_{\mathrm{j}})$ shall be calculated by Formula (7).

In Formula (7), $\phi(t_{\mathrm{j}}) = \phi_{\mathrm{haf}}(t_{\mathrm{j}})$.

b) Second stage cyclic operation ($\phi_{\mathrm{haf}}(t_{\mathrm{j}}) < L_{\mathrm{c}}(t_{\mathrm{j}}) \le \phi_{\mathrm{ful}}(t_{\mathrm{j}})$, j = p+1 to m):

In Formula (21), $P_{\mathrm{hf}}(t_{\mathrm{j}})$ and $X_{\mathrm{hf}}(t_{\mathrm{j}})$ shall be calculated by Formulae (19) and (20), respectively.

c) Full capacity operation ($L_{\mathrm{c}}(t_{\mathrm{j}}) > \phi_{\mathrm{ful}}(t_{\mathrm{j}})$, j = m+1 to n):

$P_{\mathrm{ful}}(t_{\mathrm{j}})$ shall be calculated by Formula (4).

6.7 Cooling seasonal characteristics of variable capacity units

Coefficients specified in Table 1 may be used for each characteristic.

6.7.1 Capacity characteristics against outdoor temperature

Capacities $\phi_{\text{ful}}(t_j)$, $\phi_{\text{min}}(t_j)$ and $\phi_{\text{haf}}(t_j)$ (W) of the equipment when it is operated for cooling at outdoor temperature t_j are shown in Figure A.4 in Annex A and shall be determined by Formulae (3), (9) and (14), respectively.

6.7.2 Power input characteristics against outdoor temperature

Power input $P_{\text{ful}}(t_j)$, $P_{\text{min}}(t_j)$ and $P_{\text{haf}}(t_j)$ (W) of the equipment when it is operated for cooling at outdoor temperature t_j shall be determined by Formulae (4), (10) and (15), respectively.

6.7.3 Calculation of cooling seasonal total load (CSTL)

Formula (5) in 6.4.3 shall be used.

6.7.4 Calculation of cooling seasonal energy consumption (CSEC)

When the minimum capacity data are available, then the cooling seasonal energy consumption (CSEC), C_{CSE}, shall be calculated by Formula (16).

When the minimum capacity data are not available, then the cooling seasonal energy consumption (CSEC), C_{CSE}, shall be calculated alternatively by Formula (21).

Relation of cooling capacity, power input and EER characteristics to cooling load at outdoor temperature t_j is shown in Figure A.4 in Annex A.

Calculation methods for each term of Formula (16) are as follows:

a) Cyclic operation ($L_c(t_j) \leq \phi_{\text{min}}(t_j)$, j = 1 to k):

In Formula (16), $X(t_j)$ shall be calculated by Formula (7).

In Formula (7), $\phi(t_j) = \phi_{\text{min}}(t_j)$.

b) Variable capacity operation between minimum and half capacity ($\phi_{\text{min}}(t_j) < L_c(t_j) \leq \phi_{\text{haf}}(t_j)$, j = k+1 to p):

t_p is outdoor temperature when cooling load is equal to cooling minimum capacity. (The calculation method for the crossing point is described in Annex E.)

$E_{\text{ER,min}}(t_p)$ shall be calculated from $\phi_{\text{min}}(t_p)$ and $P_{\text{min}}(t_p)$.

t_c is outdoor temperature when cooling load is equal to cooling half capacity (refer to Annex E).

$E_{\text{ER, haf}}(t_c)$ shall be calculated from $\phi_{\text{haf}}(t_c)$ and $P_{\text{haf}}(t_c)$.

It is assumed that EER linearly changes depending on outdoor temperature when the capacity of equipment changes continuously.

$$E_{\text{ER, mh}}(t_j) = E_{\text{ER, min}}(t_p) + \frac{E_{\text{ER, haf}}(t_c) - E_{\text{ER, min}}(t_p)}{t_c - t_p} \times (t_j - t_p) \tag{22}$$

$P_{\text{mh}}(t_j)$, power input between minimum and half capacity operation, shall be calculated from $L_c(t_j)$ cooling load and $E_{\text{ER, mh}}(t_j)$ by Formula (23).

$$P_{\text{mh}}(t_j) = \frac{L_c(t_j)}{E_{\text{ER, mh}}(t_j)} \tag{23}$$

c) Variable capacity operation between half and full capacity ($\phi_{\text{haf}}(t_j) < L_c(t_j) \leq \phi_{\text{ful}}(t_j)$, j = p+1 to m):

t_c is outdoor temperature when cooling load is equal to cooling half capacity (refer to Annex E).

$E_{\mathrm{ER,\,haf}}(t_\mathrm{c})$, Energy Efficiency Ratio (EER) at outdoor temperature t_c at half capacity operation, shall be calculated from $\phi_{\mathrm{haf}}(t_\mathrm{c})$ and $P_{\mathrm{haf}}(t_\mathrm{c})$ by Formula (24).

$$E_{\mathrm{ER,\,haf}}(t_\mathrm{c})=\frac{\phi_{\mathrm{haf}}(t_\mathrm{c})}{P_{\mathrm{haf}}(t_\mathrm{c})} \tag{24}$$

t_b is outdoor temperature when cooling load is equal to cooling full capacity (refer to Annex E).

$E_{\mathrm{ER,\,ful}}(t_\mathrm{b})$, Energy Efficiency Ratio (EER) at outdoor temperature t_b at full capacity operation, shall be calculated from $\phi_{\mathrm{ful}}(t_\mathrm{b})$ and $P_{\mathrm{ful}}(t_\mathrm{b})$ by Formula (25).

$$E_{\mathrm{ER,\,ful}}(t_\mathrm{b})=\frac{\phi_{\mathrm{ful}}(t_\mathrm{b})}{P_{\mathrm{ful}}(t_\mathrm{b})} \tag{25}$$

It is assumed that EER linearly changes depending on outdoor temperature when the capacity of equipment changes continuously.

$$E_{\mathrm{ER,\,hf}}(t_\mathrm{j})=E_{\mathrm{ER,\,haf}}(t_\mathrm{c})+\frac{E_{\mathrm{ER,\,ful}}(t_\mathrm{b})-E_{\mathrm{ER,\,haf}}(t_\mathrm{c})}{t_\mathrm{b}-t_\mathrm{c}}\times(t_\mathrm{j}-t_\mathrm{c}) \tag{26}$$

$P_{\mathrm{hf}}(t_\mathrm{j})$, power input between half and full capacity operation, shall be calculated from $L_\mathrm{c}(t_\mathrm{j})$ cooling load and $E_{\mathrm{ER,\,hf}}(t_\mathrm{j})$ by Formula (27).

$$P_{\mathrm{hf}}(t_\mathrm{j})=\frac{L_\mathrm{c}(t_\mathrm{j})}{E_{\mathrm{ER,\,hf}}(t_\mathrm{j})} \tag{27}$$

d) Full capacity operation ($\phi_{\mathrm{ful}}(t_\mathrm{j}) < L_\mathrm{c}(t_\mathrm{j})$, j = m+1 to n):

   $P_{\mathrm{ful}}(t_\mathrm{j})$ shall be calculated by Formula (4).

In case that the minimum capacity is not measured, the cooling seasonal energy consumption (CSEC), C_{CSE}, shall be calculated by Formula (21).

a) Cyclic operation ($L_\mathrm{c}(t_\mathrm{j}) \leq \phi_{\mathrm{haf}}(t_\mathrm{j})$, j = 1 to p):

   In this range, calculation shall be made assuming that the air conditioner cyclically operates with the half operating capacity.

   In Formula (21), $X(t_\mathrm{j})$ shall be calculated by Formula (7).

   In Formula (7), $\phi(t_\mathrm{j}) = \phi_{\mathrm{haf}}(t_\mathrm{j})$.

b) Variable capacity operation between half and full capacity ($\phi_{\mathrm{haf}}(t_\mathrm{j}) < L_\mathrm{c}(t_\mathrm{j}) \leq \phi_{\mathrm{ful}}(t_\mathrm{j})$, j = p+1 to m):

   This calculation shall be made by using Formulae (24) to (27).

c) Full capacity operation ($\phi_{\mathrm{ful}}(t_\mathrm{j}) < L_\mathrm{c}(t_\mathrm{j})$, j = m+1 to n):

   $P_{\mathrm{ful}}(t_\mathrm{j})$ shall be calculated by Formula (4).

7 Test report

The test report shall include:

a) the type of unit;

b) the list of mandatory test points performed, and the resulting capacity and *EER* values;

c) the list of optional test points performed, and the resulting capacity and *EER* values;

d) the default values used;

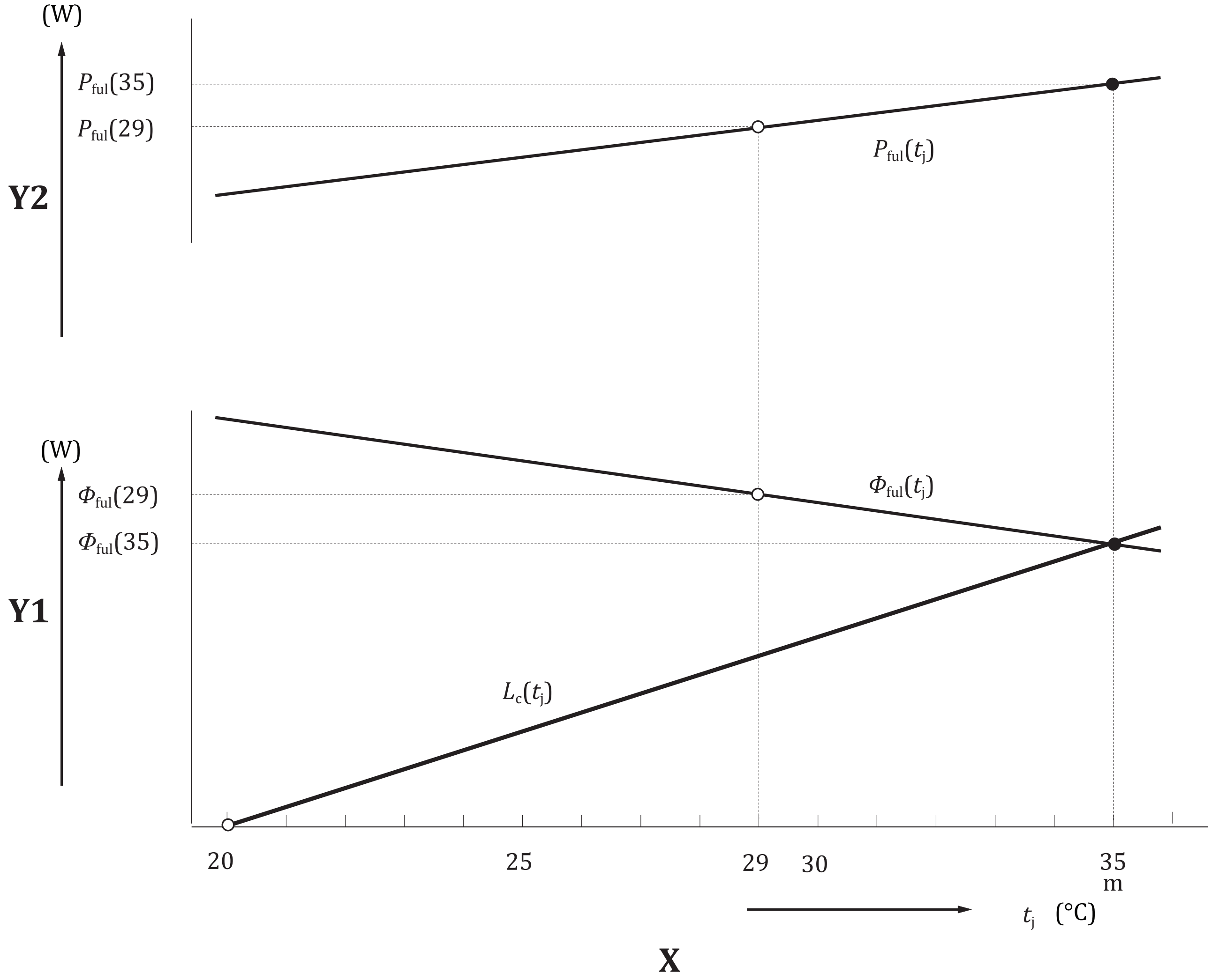
e) for multi-split systems, a combination of indoor units and an outdoor unit.

For variable capacity units, frequency settings for each performed test shall also be indicated.

The cooling seasonal performance factor (CSPF) shall be declared with three significant digits, with reference to the reference defined cooling load and to the reference outdoor temperature bin distribution used.

Annex A
(informative)

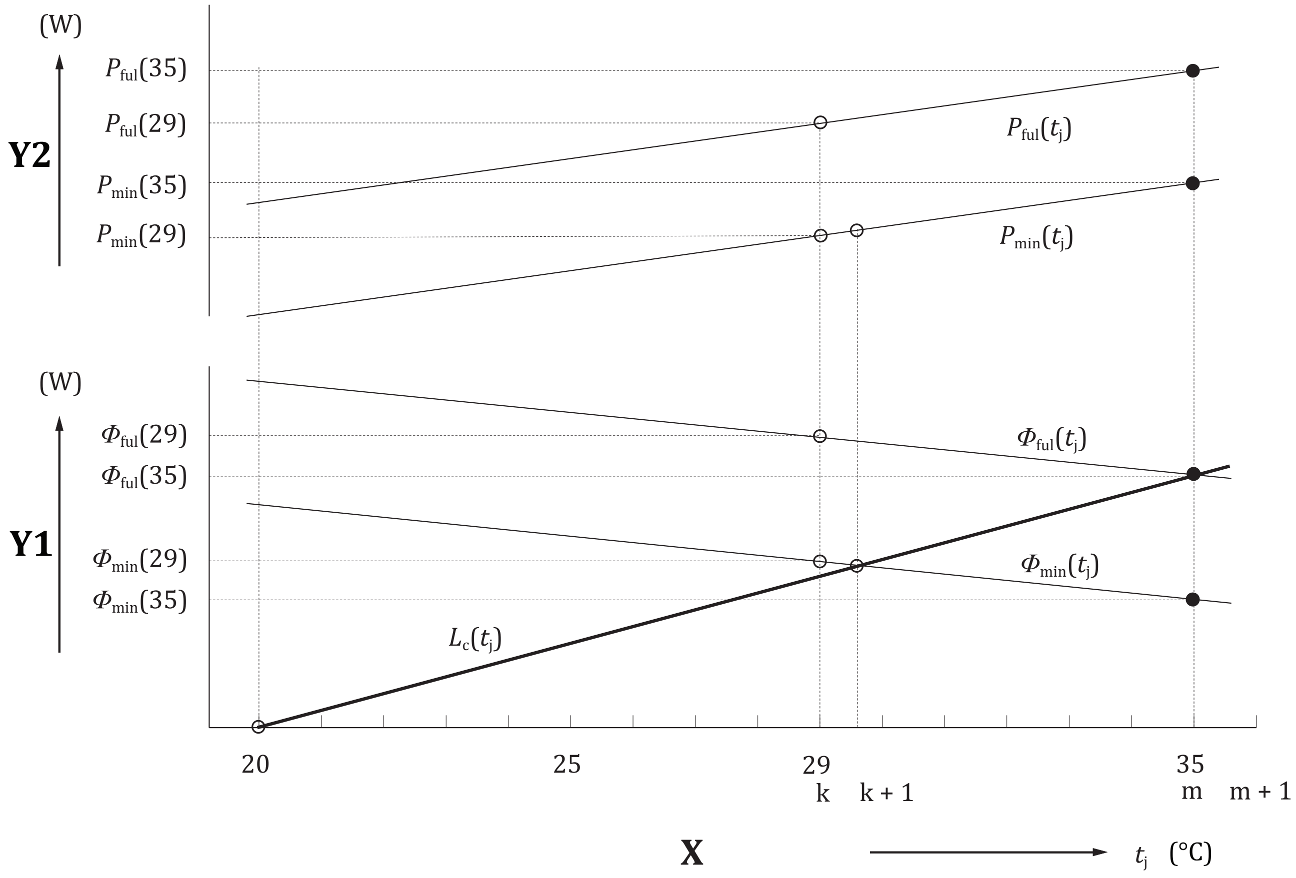
Figures



Key

X	outdoor temperature
Y1	capacity or load
Y2	power input

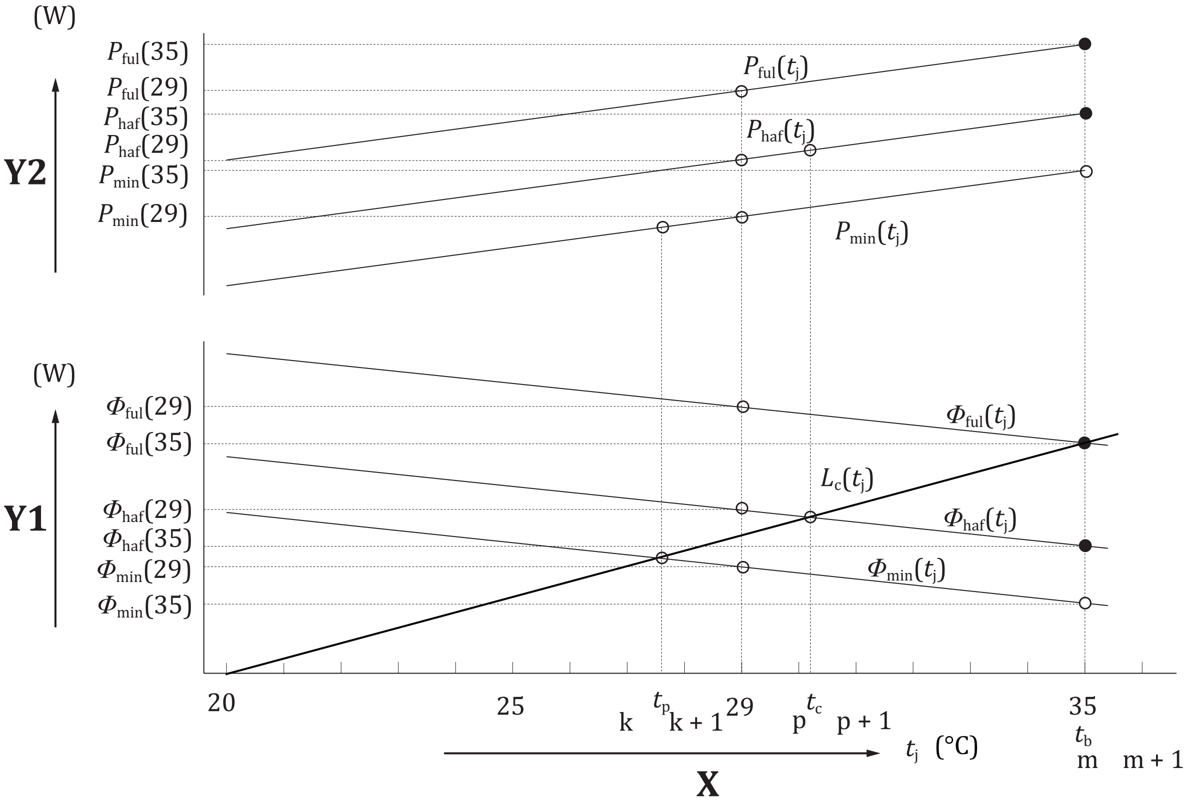
Figure A.1 — Cooling capacity, power input and cooling load for fixed capacity units



Key

X	outdoor temperature
Y1	capacity or load
Y2	power input

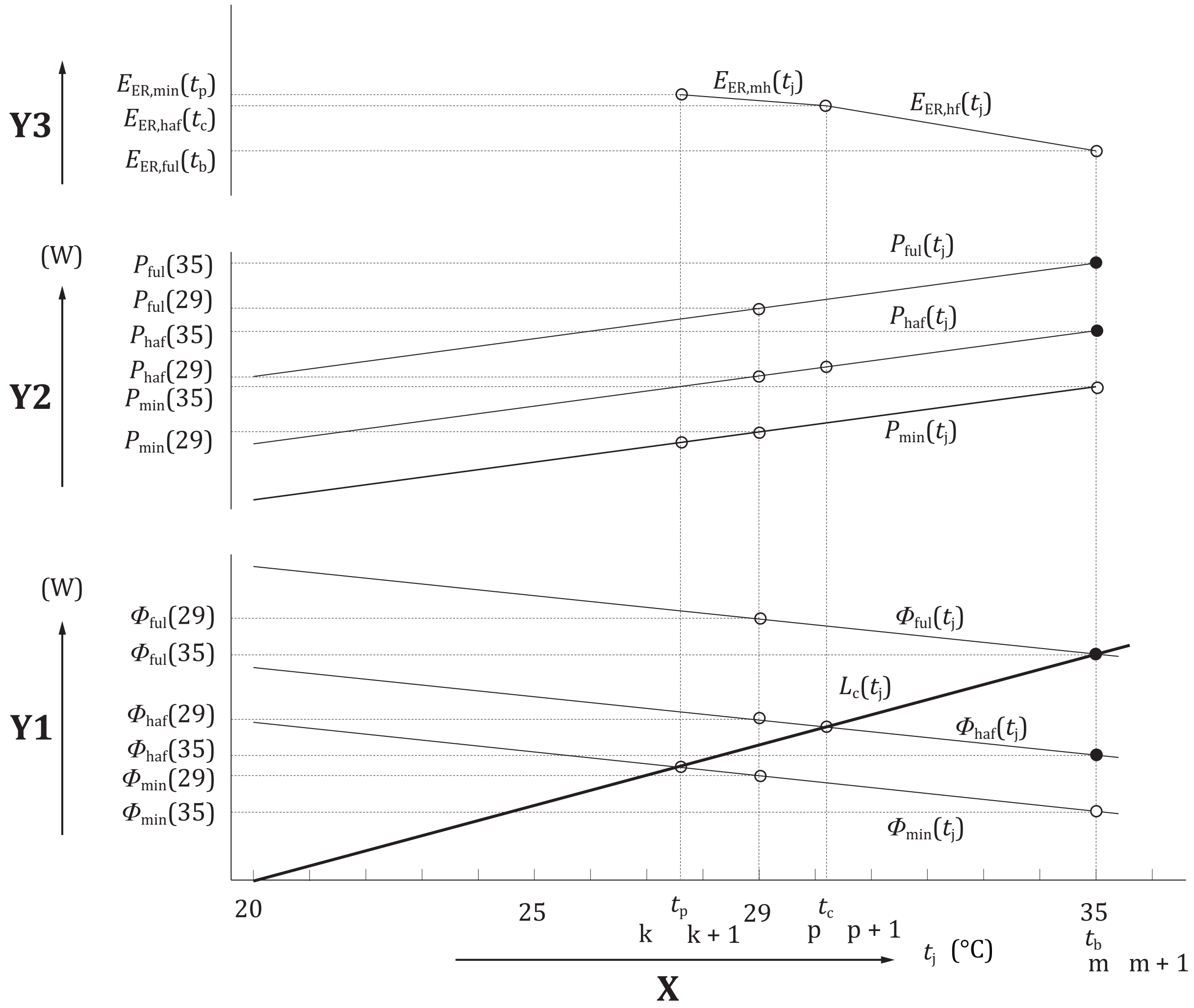
Figure A.2 — Cooling capacity, power input and cooling load for two-stage capacity units



Key

X	outdoor temperature
Y1	capacity or load
Y2	power input

Figure A.3 — Cooling capacity, power input and cooling load for multi-stage capacity units



Key

X	outdoor temperature
Y1	capacity or load
Y2	power input
Y3	energy efficiency ratio (EER)

Figure A.4 — Cooling capacity, power input, cooling load and EER for variable capacity units

Annex B
(informative)

Calculation of total cooling seasonal performance factor (TCSPF)

B.1 General

This Annex applies to cooling only units, cooling units with supplemental heat and reversible units.

B.2 Measurement of the electric power consumption during the inactive mode

The unit shall be electrically connected to the main power source after shut-down for 6 h. Indoor and outdoor temperature of 20 °C condition shall be reached. The power consumption shall be measured for one hour after the temperature conditions are stabilized. The same test is repeated with the temperature condition of 5 °C, 10 °C and then 15 °C with the stabilization period of 2 h between each test. As a reference case, each power consumption value shall be weighted by the weighting factors in Table B.1 and then integrated to obtain a weighted average inactive power consumption, P_{ia}. The calculation of inactive power may also be undertaken for other climate conditions and operating schedules.

NOTE If the results of the tests at 20 °C and 5 °C are within 5 % or 1 W, then the tests at 15 °C and 10 °C are not mandatory. The average value of these results is used for the four considered temperature conditions.

Table B.1 — Default weighting factors for determination of reference inactive energy consumption

Temperature condition	5 °C	10 °C	15 °C	20 °C
Weighting factor	0,05	0,13	0,27	0,55

Inactive energy consumption (IAEC) shall be calculated by Formula (B.1).

$$C_{\mathrm{IAE}} = H_{\mathrm{ia}} \times P_{\mathrm{ia}} \qquad \text{(B.1)}$$

where

C_{IAE} is the inactive energy consumption;

H_{ia} is the number of hours of inactive mode as given in Table B.2;

P_{ia} is the weighted average power consumption.

B.3 Calculation of total cooling seasonal performance factor (TCSPF)

Total cooling seasonal performance factor (TCSPF), F_{TCSP}, shall be calculated by Formula (B.2).

$$F_{\mathrm{TCSP}} = L_{\mathrm{CST}} / (C_{\mathrm{CSE}} + C_{\mathrm{IAE}}) \qquad \text{(B.2)}$$

Calculation of L_{CST} and C_{CSE} is according to the main body of this part of ISO 16358.

Inactive energy consumption (IAEC), C_{IAE}, shall be calculated by Formula (B.1).

The default mode hours for the calculation of reference total cooling seasonal performance factor are shown in Table B.2. The calculation of total cooling seasonal performance factor may also be undertaken for other distributions of mode hours.

Table B.2 — Default hours by mode for the calculation of reference total cooling seasonal performance factor

Unit	Active mode h	Inactive mode, H_{ia} h	Disconnected mode h
Cooling only unit	1 817	4 077	2 866
Cooling unit with supplemental heat	1 817 (Heating operation: 2 866)	4 077	0
Reversible unit	1 817 (Heating operation: 2 866)	4 077	0

Annex C
(normative)

Testing and calculation method for degradation coefficient of cyclic operation

C.1 Low humidity cooling test and cyclic cooling test

The low humidity cooling test and the cyclic cooling test shall be conducted in accordance with Annex A of ISO 5151 and Annex B of ISO 13253 and ISO 15042 as specified in C.2 of this annex.

Testing condition for cyclic cooling test is shown in Table C.1.

Table C.1 — Temperature and humidity conditions for cyclic cooling test

Test	Indoor temperature °C		Outdoor temperature °C	
	Dry-bulb	Wet-bulb	Dry-bulb	Wet-bulb
A test: Steady, dry coil	27	13,9 or less	29	—
B test: Cyclic, dry coil	27	13,9 or less	29	—

NOTE 1 The entering air to the unit must have a low enough moisture content so no condensate forms on the indoor coil. (It is recommended that an indoor wet-bulb temperature of 13,9 °C or less be used.)

NOTE 2 Maintain the airflow nozzles static pressure difference or velocity pressure during the ON period at the same pressure difference or velocity pressure as measured during the A test.

Duration of ON and OFF interval of cyclic operation test is shown in Table C.2.

Table C.2 — Duration of ON and OFF interval of cyclic operation test

Unit type	Operation	Interval (min)		1 Cycle (min)
		ON	OFF	
Fixed capacity type	Full capacity operation	6	24	30
Two-stage capacity type	Minimum capacity operation	6	24	30
Multi-stage capacity type	Minimum capacity operation or Half capacity operation[a]	6	24	30
Variable capacity type[b]	Minimum capacity operation or Half capacity operation[a]	12	48	60

[a] If minimum capacity steady operation is not measured, then half capacity operation cyclic test instead of minimum capacity operation cyclic test shall be done.

[b] For variable capacity units, the cyclic test is not needed. The above is for information only.

C.2 Test procedure

C.2.1 Test procedure for steady-state dry-coil cooling mode test (A test)

Prior to recording data during the steady-state dry coil test, operate the unit at least one hour after achieving dry coil conditions. Drain the drain pan and plug the drain opening. Thereafter, the drain pan should remain completely dry.

Record the cooling capacity and electrical power derived from the steady-state dry-coil mode test. In preparing for C.2.2 cyclic tests, record the average indoor-side air volume rate derived from either pressure difference or velocity pressure for the flow nozzles and air properties.

C.2.2 Test procedure for optional cyclic dry-coil cooling mode test (B test)

C.2.2.1 Test condition

After completing the steady-state dry-coil test, remove the Outdoor Air Enthalpy method test apparatus, if connected, and begin manual OFF/ON cycling of the unit's compressor. The test set-up should otherwise be identical to the set-up used during the steady-state dry-coil test. When testing heat pumps, leave the reversing valve during the compressor OFF cycles in the same position as used for the compressor ON cycles, unless automatically changed by the controls of the unit.

Duration of ON and OFF interval shall be in accordance with Table C.2.

Repeat the OFF/ON compressor cycling pattern until the test is completed. Allow the controls of the unit to regulate cycling of the outdoor fan.

In all cases, use the exhaust fan of the airflow measuring apparatus along with the indoor fan of the unit, if installed and operating, to approximate a step response in the indoor coil airflow.

C.2.2.2 Measurement by using the automatic exhaust fan control of airflow measuring apparatus

If the airflow measuring apparatus has a function to adjust static pressure automatically and immediately so that static pressure difference is equal to zero for ductless units or static pressure is equal to a certain external pressure value for duct units by controlling the exhaust fan operation, the difference between the value of nozzle pressure difference or velocity pressure which is measured by the airflow measuring apparatus having an automatic exhaust fan control and the value which is measured at the steady-state dry-coil test shall be within 2 % within 15 s after airflow initiation. If the airflow measuring apparatus does not meet the requirements or if the apparatus does not have the ability to automatically control the exhaust fan, it may be measured by manually adjusting the exhaust fan.

C.2.2.3 Measurement by using the manual exhaust fan control of airflow measuring apparatus

Regulate the exhaust fan to quickly obtain and then maintain the flow nozzle static pressure difference or velocity pressure at the same value as was measured during the steady-state dry-coil test. The pressure difference or velocity pressure should be within 2 % of the value from the steady-state dry-coil test within 15 s after airflow initiation.

C.2.2.4 Data collection

After completing a minimum of two complete compressor OFF/ON cycles, determine the overall cooling delivered and total electrical energy consumption during any subsequent data collection interval.

Test tolerance of the dry-bulb temperature shall be ± 2,5 °C on the indoor side and ± 5 °C on the outdoor side as specified in ISO 5151, ISO 13253 and ISO 15042.

Sample the air property, air flow rate and electrical voltage at least every 2 min during periods when air flows through the coil. Record the dry-bulb temperature of the air entering and leaving the indoor coil at equal intervals that span 10 s or less.

Integrate the cooling capacity and the electrical power over complete cycles. For ducted units tested with an indoor fan installed and operating, integrate electrical power from indoor fan OFF to indoor fan OFF. For all other ducted units and for non-ducted units, integrate electrical power from compressor OFF to compressor OFF.

Degradation coefficient (C_D) shall be calculated by using the result of A test and B test of Table C.1 by Formula (C.1).

Formula (C.1) is expressed for the case of full capacity operation. Formula (C.1) can be applied for half cooling capacity cyclic operation $\phi_{\text{haf(cyc)}}$ and minimum cooling capacity cyclic operation $\phi_{\text{min(cyc)}}$.

$$C_D = \frac{1 - \dfrac{\phi_{\text{ful(cyc)}} / P_{\text{ful(cyc)}}}{\phi_{\text{ful(dry)}} / P_{\text{ful(dry)}}}}{1 - \phi_{\text{ful(cyc)}} / \phi_{\text{ful(dry)}}} = \frac{1 - \dfrac{E_{\text{ER, ful(cyc)}}}{E_{\text{ER, ful(dry)}}}}{1 - F_{\text{CL, ful}}} \tag{C.1}$$

where

$\phi_{\text{ful(cyc)}}$	is the capacity (W) of air conditioner when operated for cooling with the rated operating capacity tested by the method specified in C.2.2;
$P_{\text{ful(cyc)}}$	is the cooling power consumption (W) when operated for cooling with the rated operating capacity tested by the method specified in C.2.2;
$\phi_{\text{ful(dry)}}$	is the capacity (W) of air conditioner when operated for cooling with the rated operating capacity tested by the method specified in C.2.1;
$P_{\text{ful(dry)}}$	is the cooling power consumption (W) when operated for cooling with the rated operating capacity tested by the method specified in C.2.1;
$E_{\text{ER, ful(cyc)}}$	is the energy efficiency ratio of air conditioner when operated for cooling with the rated operating capacity tested by the method specified in C.2.2;
$E_{\text{ER, ful(dry)}}$	is the energy efficiency ratio of air conditioner when operated for cooling with the rated operating capacity tested by the method specified in C.2.1;
$F_{\text{CL, ful}}$	is the ratio of $\phi_{\text{ful(cyc)}}$ and $\phi_{\text{ful(dry)}}$.

Annex D
(informative)

Calculating method for seasonal performance factor when setting a specific cooling load

A specific cooling load widely varies from region to region on the globe depending on climate conditions, building structures and the situations in which air conditioners and heat pumps (hereinafter referred to as equipment) are used.

In order to evaluate and compare different seasonal performance factors of the equipment, it is desirable that a representative cooling load is established.

For this purpose, this annex is given to establish a minimum, representative cooling load and to show an evaluation method of the equipment operating at the conditions fixed by this load.

This annex also specifies a calculation method for seasonal performance factor of the equipment installed in a specific region or in a specific building.

D.1 Cooling seasonal performance factor (CSPF)

Calculation of cooling seasonal performance factor (CSPF) is made in accordance with the provisions specified in the main body for each type of equipment.

D.1.1 Setting of bin hours of outdoor temperature which requires cooling in a specific region

Bin hours of each outdoor temperature which requires cooling during the cooling season shall be set.

D.1.2 Setting of a specific cooling load, L_c

a) An outdoor temperature at 100 % cooling load shall be set.

b) The highest outdoor temperature occurred is determined from the data in D.1.1, but it is desirable to exclude the abnormal condition which is thought to be unusual.

c) A load of a specific building is calculated to determine the required cooling capacity at the 100 % load outdoor temperature.

d) 0 % load outdoor temperature shall be set based on the calculated load of the specific building and the purpose of using the equipment.

e) From these, a load curve is obtained.

D.1.3 Outdoor temperature characteristics of equipment

Outdoor temperature characteristics of equipment relative to cooling capacity and power input are obtained from the main body.

Annex E
(informative)

Calculating method for temperature when defined load line crosses each capacity line

Defined load $L_c(t_j)$ is calculated by Formula (E.1), which is the same as Formula (2) of the main body.

$$L_c(t_j) = \phi_{ful}(t_{100}) \times \frac{(t_j - t_0)}{(t_{100} - t_0)} \tag{E.1}$$

Each capacity characteristic $\phi(t_j)$ is given by Formulae (E.2) to (E.4), which are the same as Formulae (3), (9) and (14) of the main body.

$$\phi_{ful}(t_j) = \phi_{ful}(35) + \frac{\phi_{ful}(29) - \phi_{ful}(35)}{(35 - 29)} \times (35 - t_j) \tag{E.2}$$

$$\phi_{haf}(t_j) = \phi_{haf}(35) + \frac{\phi_{haf}(29) - \phi_{haf}(35)}{(35 - 29)} \times (35 - t_j) \tag{E.3}$$

$$\phi_{min}(t_j) = \phi_{min}(35) + \frac{\phi_{min}(29) - \phi_{min}(35)}{(35 - 29)} \times (35 - t_j) \tag{E.4}$$

Crossing point of full capacity operation line and load line, t_b, is calculated by Formulae (E.1) and (E.2).

$$L_c(t_j) = \phi_{ful}(t_j)$$

$$\phi_{\mathrm{ful}}(t_{100})\times\frac{(t_{\mathrm{b}}-t_0)}{(t_{100}-t_0)}=\phi_{\mathrm{ful}}(35)+\frac{\phi_{\mathrm{ful}}(29)-\phi_{\mathrm{ful}}(35)}{(35-29)}\times(35-t_{\mathrm{b}}) \tag{E.5}$$

Then, t_{b} is given by Formula (E.6).

$$t_{\mathrm{b}}=\frac{6\phi_{\mathrm{ful}}(t_{100})t_0+6\phi_{\mathrm{ful}}(35)(t_{100}-t_0)+35(\phi_{\mathrm{ful}}(29)-\phi_{\mathrm{ful}}(35))(t_{100}-t_0)}{6\phi_{\mathrm{ful}}(t_{100})+(\phi_{\mathrm{ful}}(29)-\phi_{\mathrm{ful}}(35))(t_{100}-t_0)} \tag{E.6}$$

Crossing point of half capacity operation line and load line, t_{c}, is calculated by Formulae (E.1) and (E.3).

$$\phi_{\mathrm{ful}}(t_{100})\times\frac{(t_c-t_0)}{(t_{100}-t_0)}=\phi_{\mathrm{haf}}(35)+\frac{\phi_{\mathrm{haf}}(29)-\phi_{\mathrm{haf}}(35)}{(35-29)}\times(35-t_{\mathrm{c}}) \tag{E.7}$$

Then, t_{c} is given by Formula (E.8).

$$t_{\mathrm{c}}=\frac{6\phi_{\mathrm{ful}}(t_{100})t_0+6\phi_{\mathrm{haf}}(35)(t_{100}-t_0)+35(\phi_{\mathrm{haf}}(29)-\phi_{\mathrm{haf}}(35))(t_{100}-t_0)}{6\phi_{\mathrm{ful}}(t_{100})+(\phi_{\mathrm{haf}}(29)-\phi_{\mathrm{haf}}(35))(t_{100}-t_0)} \tag{E.8}$$

Crossing point of minimum capacity operation line and load line, t_{p}, is calculated by Formulae (E.1) and (E.4).

$$\phi_{\mathrm{ful}}(t_{100})\times\frac{(t_{\mathrm{p}}-t_0)}{(t_{100}-t_0)}=\phi_{\min}(35)+\frac{\phi_{\min}(29)-\phi_{\min}(35)}{(35-29)}\times(35-t_{\mathrm{p}}) \tag{E.9}$$

Then, t_{p} is given by Formula (E.10).

$$t_{\mathrm{p}}=\frac{6\phi_{\mathrm{ful}}(t_{100})t_0+6\phi_{\min}(35)(t_{100}-t_0)+35(\phi_{\min}(29)-\phi_{\min}(35))(t_{100}-t_0)}{6\phi_{\mathrm{ful}}(t_{100})+(\phi_{\min}(29)-\phi_{\min}(35))(t_{100}-t_0)} \tag{E.10}$$

Using default $\phi(29) = 1{,}077 \times \phi\,(35)$ in Table 1 of the main body, $\phi(t_{\mathrm{j}})$ becomes Formula (E.11).

$$\phi_{\mathrm{ful}}(t_{\mathrm{j}})=\phi_{\mathrm{ful}}(35)\times\left(1+\frac{0{,}077(35-t_{\mathrm{j}})}{6}\right) \tag{E.11}$$

Crossing point of full capacity operation line and load line, t_{b}, is calculated by Formulae (E.1) and (E.11).

$$\phi_{\mathrm{ful}}(t_{100})\times\frac{(t_{\mathrm{b}}-t_0)}{(t_{100}-t_0)}=\phi_{\mathrm{ful}}(35)\times\left(1+\frac{0{,}077(35-t_{\mathrm{b}})}{6}\right) \tag{E.12}$$

Then, t_{b} is given by Formula (E.13).

$$t_{\mathrm{b}}=\frac{6\phi_{\mathrm{ful}}(t_{100})t_0+6\phi_{\mathrm{ful}}(35)(t_{100}-t_0)+0{,}077\times35\phi_{\mathrm{ful}}(35)(t_{100}-t_0)}{6\phi_{\mathrm{ful}}(t_{100})+0{,}077\phi_{\mathrm{ful}}(35)(t_{100}-t_0)} \tag{E.13}$$

In the same way, crossing point of half capacity operation line and load line, t_{c}, is given by Formula (E.14).

$$t_{\mathrm{c}}=\frac{6\phi_{\mathrm{ful}}(t_{100})t_0+6\phi_{\mathrm{haf}}(35)(t_{100}-t_0)+0{,}077\times35\phi_{\mathrm{haf}}(35)(t_{100}-t_0)}{6\phi_{\mathrm{ful}}(t_{100})+0{,}077\phi_{\mathrm{haf}}(35)(t_{100}-t_0)} \tag{E.14}$$

In the same way, crossing point of minimum capacity operation line and load line, t_{p}, is given by Formula (E.15).

$$t_{\mathrm{p}}=\frac{6\phi_{\mathrm{ful}}(t_{100})t_0+6\phi_{\min}(35)(t_{100}-t_0)+0{,}077\times35\phi_{\min}(35)(t_{100}-t_0)}{6\phi_{\mathrm{ful}}(t_{100})+0{,}077\phi_{\min}(35)(t_{100}-t_0)} \tag{E.15}$$

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