BS ISO 10791-7:2014



BSI Standards Publication

Test conditions for machining centres

Part 7: Accuracy of finished test pieces



BS ISO 10791-7:2014

National foreword

This British Standard is the UK implementation of ISO 10791-7:2014. It supersedes BS ISO 10791-7:1998 which is withdrawn.

The UK participation in its preparation was entrusted to Technical Committee MTE/1/2, Machine tools - Accuracy.

A list of organizations represented on this committee can be obtained on request to its secretary.

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Second edition 2014-12-01

Test conditions for machining centres —

Part 7: **Accuracy of finished test pieces**

Conditions d'essai pour centres d'usinage — Partie 7: Exactitude des pièces d'essai usinées



BS ISO 10791-7:2014 **ISO 10791-7:2014(E)**



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Foreword

ISO (the International Organization for Standardization) is a worldwide federation of national standards bodies (ISO member bodies). The work of preparing International Standards is normally carried out through ISO technical committees. Each member body interested in a subject for which a technical committee has been established has the right to be represented on that committee. International organizations, governmental and non-governmental, in liaison with ISO, also take part in the work. ISO collaborates closely with the International Electrotechnical Commission (IEC) on all matters of electrotechnical standardization.

The procedures used to develop this document and those intended for its further maintenance are described in the ISO/IEC Directives, Part 1. In particular the different approval criteria needed for the different types of ISO documents should be noted. This document was drafted in accordance with the editorial rules of the ISO/IEC Directives, Part 2 (see www.iso.org/directives).

Attention is drawn to the possibility that some of the elements of this document may be the subject of patent rights. ISO shall not be held responsible for identifying any or all such patent rights. Details of any patent rights identified during the development of the document will be in the Introduction and/or on the ISO list of patent declarations received (see www.iso.org/patents).

Any trade name used in this document is information given for the convenience of users and does not constitute an endorsement.

For an explanation on the meaning of ISO specific terms and expressions related to conformity assessment, as well as information about ISO's adherence to the WTO principles in the Technical Barriers to Trade (TBT), see the following URL: Foreword — Supplementary information.

The committee responsible for this document is ISO/TC 39, *Machine Tools*, Subcommittee SC 2, *Test conditions for metal cutting machine tools*.

This second edition cancels and replaces the first edition, which has been technically revised.

ISO 10791 consists of the following parts, under the general title *Test conditions for machining centres*:

- Part 1: Geometric tests for machines with horizontal spindle and with accessory heads (horizontal Z-axis)
- Part 2: Geometric tests for machines with vertical spindle or universal heads with vertical primary rotary axis (vertical Z-axis)
- Part 3: Geometric tests for machines with integral indexable or continuous universal heads (vertical Z-axis)
- Part 4: Accuracy and repeatability of positioning of linear and rotary axes
- Part 5: Accuracy and repeatability of positioning of work-holding pallets
- Part 6: Accuracy of speeds and interpolations
- Part 7: Accuracy of finished test pieces
- Part 8: Evaluation of contouring performance in the three coordinate planes
- Part 9: Evaluation of the operating times of tool change and pallet change
- Part 10: Evaluation of thermal distortions

Introduction

A machining centre is a numerically controlled machine tool capable of performing multiple machining operations, including milling, boring, drilling, and tapping, as well as automatic tool changing from a magazine or similar storage unit in accordance with a machining programme. Most machining centres have facilities for automatically changing the direction in which the workpieces are presented to the tool.

The purpose of ISO 10791 (all parts) is to supply information as wide and comprehensive as possible on tests and checks which can be carried out for comparison, acceptance, maintenance, or any other purpose.

This International Standard specifies, by reference to the relevant parts of ISO 230, several families of tests for machining centres with horizontal or vertical spindle or with universal heads of different types, standing alone, or integrated in flexible manufacturing systems. This International Standard also establishes the tolerances or maximum acceptable values for the test results corresponding to general purpose and normal accuracy machining centres.

This International Standard is also applicable, totally, or partially, to numerically controlled milling and boring machines, when their configuration, components, and movements are compatible with the tests described herein.

Test conditions for machining centres —

Part 7:

Accuracy of finished test pieces

1 Scope

This part of ISO 10791 specifies standard test pieces with reference to ISO 230-1, cutting tests under finishing conditions. It also specifies the characteristics and dimensions of the test pieces themselves. This part of ISO 10791 is intended to supply minimum requirements for assessing the cutting accuracy of the machine. This part of ISO 10791 takes into consideration 3- to 5-axis machining centres.

2 Normative references

The following documents, in whole or in part, are normatively referenced in this document and are indispensable for its application. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

ISO 230-1:2012, Test code for machine tools — Part 1: Geometric accuracy of machines operating under no-load or quasi-static conditions

3 Preliminary remarks

3.1 Measuring units

In this part of ISO 10791, all linear dimensions and deviations are expressed in millimetres. All angular dimensions are expressed in degrees. Angular deviations are, in principle, expressed in ratios (e.g. $0.00x/1\ 0.00$), but in some cases, microradians or arcseconds can be used for clarification purposes. The following expression should be used for conversion of angular deviations or tolerances:

 $0.010/1\ 000 = 10\ \mu grad \approx 2''$

3.2 Reference to ISO 230-1

To apply this part of ISO 10791, reference shall be made to ISO 230-1, especially for the installation of the machine before testing, warming up of the machine, description of measuring methods, and evaluation and presentation of the results.

3.3 Testing sequence

The sequence in which the tests are presented in this part of ISO 10791 in no way defines the practical order of testing. In order to make the mounting of fixtures and machining easier, tests can be performed in any order.

3.4 Tests to be performed

When testing a machine, it is not always necessary or possible to carry out all the tests described in this part of ISO 10791. When the tests are required for acceptance purposes, it is up to the user to choose, in agreement with the manufacturer/supplier, those tests relating to the components and/or the properties of the machine which are of interest. These tests are to be clearly stated when ordering a

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machine. Mere reference to this part of ISO 10791 for the acceptance tests, without specifying the tests to be carried out, and without agreement on the relevant expenses, cannot be considered as binding for any contracting party.

In principle, no more than one piece of each type should be machined for acceptance purposes. In case of special requirements, such as statistical assessment of the machine tool performance (e.g. according to ISO 26303, short-term capability), the machining of more test pieces is to be submitted to agreement between manufacturer/supplier and user.

3.5 Measuring instruments

The measuring instruments indicated in the tests described in <u>Clause 4</u> are examples only. Other instruments measuring the same quantities and having the same or smaller measurement uncertainty can be used.

3.6 Location of test pieces

The test piece should be placed approximately at mid-travel of the X- axis, and in positions along Y- and Z- axes suitable for the location of the test piece and/or fixture, and for the tool lengths if not specified otherwise in the test procedure.

3.7 Fixing of test pieces

The test piece shall be conveniently mounted on a proper fixture, such that maximum stability of tools and fixture is achieved. The mounting surfaces of the fixture and of the test piece shall be flat. It is recommended that a suitable means of fixturing should be used to allow for tool breakthrough and full length machining of, for example, a centre hole. It is further recommended to mount the test piece on the fixture with countersink/counterbored screws such that subsequent machining does not interfere with the screws. Other methods are possible and can be selected. Overall height of the test piece depends on the selected method of fixing.

3.8 Material of test pieces, tooling, and cutting parameters

The test piece material, tooling, and the subsequent cutting parameters are subject to agreement between manufacturer/supplier and user and shall be recorded. The parameters provided in the cutting tests are for suggestions only. The test piece material shall be specified with proper material designations.

3.9 Sizes of test pieces

If the test pieces come from previous cutting tests and are re-useable, their characteristic dimensions should remain within ±10 % of those indicated in this part of ISO 10791. When the test pieces are re-used, a shallow cut shall be made to clean up all surfaces before new finishing test cuts are taken.

It is also recommended that type and serial number of the machine, date of test, and names and orientation of the axes are marked on the test pieces.

Preliminary cuts should be taken in order to make the depth of cut as constant as possible.

The nominal size of test pieces can be modified by mutual agreement with the manufacturer/supplier and user. When the nominal size of test pieces is modified, the feed speed (for circular contouring) can be modified in an analogous manner as shown in ISO 230-4:2005, Annex C. The tool size and other machining conditions may be also modified.

3.10 Types of test piece

In this part of ISO 10791, four types of test piece are considered, each of them in two or three sizes. Types, sizes, and corresponding designation of the particular test piece are shown in <u>Table 1</u>. Among

these types, Type M1 and M2 are applicable for 3-, 4-, and 5-axis machining centres. M3 is applicable only for 5-axis machining centres. M4 is applicable for 4- and 5-axis machining centres.

Table 1 — Types, sizes, and designation of the test pieces

Туре	Nominal size	Designation
	80	Test piece ISO 10791-7, M1_80
M1 Positioning and contouring test piece	160	Test piece ISO 10791-7, M1_160
r obtaining and contouring test piece	80 Test piece ISO 10791-7, M1_2 320 Test piece ISO 10791-7, M1_2 80 Test piece ISO 10791-7, M2_ 160 Test piece ISO 10791-7, M2_ 15a Test piece ISO 10791-7, M3_ 45a Test piece ISO 10791-7, M3_ 80 Test piece ISO 10791-7, M4_ 160 Test piece ISO 10791-7, M4_	Test piece ISO 10791-7, M1_320
M2	80	Test piece ISO 10791-7, M2_80
Face milling test piece	160	Test piece ISO 10791-7, M2_160
M3	15a	Test piece ISO 10791-7, M3_15
Cone frustum test piece	45a	Test piece ISO 10791-7, M1_80 Test piece ISO 10791-7, M1_160 Test piece ISO 10791-7, M1_320 Test piece ISO 10791-7, M2_80 Test piece ISO 10791-7, M2_160
	80	Test piece ISO 10791-7, M4_80
M4 Three-step square test piece	160	Test piece ISO 10791-7, M4_160
Times step square test piece	320	Test piece ISO 10791-7, M4_320
a Half-apex angle of test piece.	_	

3.11 Information to be recorded

For tests made according to the requirements of this part of ISO 10791, the following information shall be compiled as completely as possible and included in the test report:

- a) material and designation of the test piece;
- b) material, dimensions, and number of teeth of the tool;
- c) cutting speed;
- d) feed speed;
- e) depth of cut;
- f) other cutting parameters, e.g. cutting fluid;
- g) position and orientation of the workpiece in the work space;
- h) direction of cuts (where applicable).

3.12 Software compensation

When software facilities are available for compensating some geometric errors, based on an agreement between the manufacturer/supplier and user, the relevant test can be carried out with these compensations. When the software compensation is used, this shall be stated in the test report.

4 Machining tests

Object M1

Checking the performance of the machine under different kinematic conditions, i.e. only one axis feed, linear interpolation of two axes and circular interpolation by machining five bored holes and a series of finishing passes on different profiles.

NOTE 1 This test is usually performed in the XY plane of the machine, but may be performed in the other coordinate planes when a universal spindle head is available.

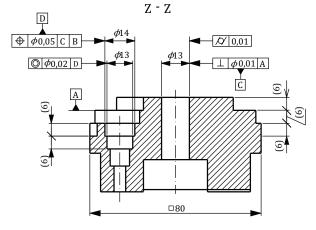
NOTE 2 Test M4 defines additions to test M1 for testing accuracy and positioning of rotary and swivelling axes.

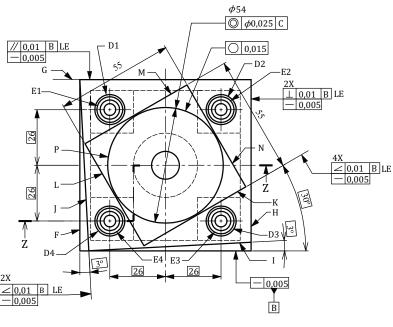
Diagram

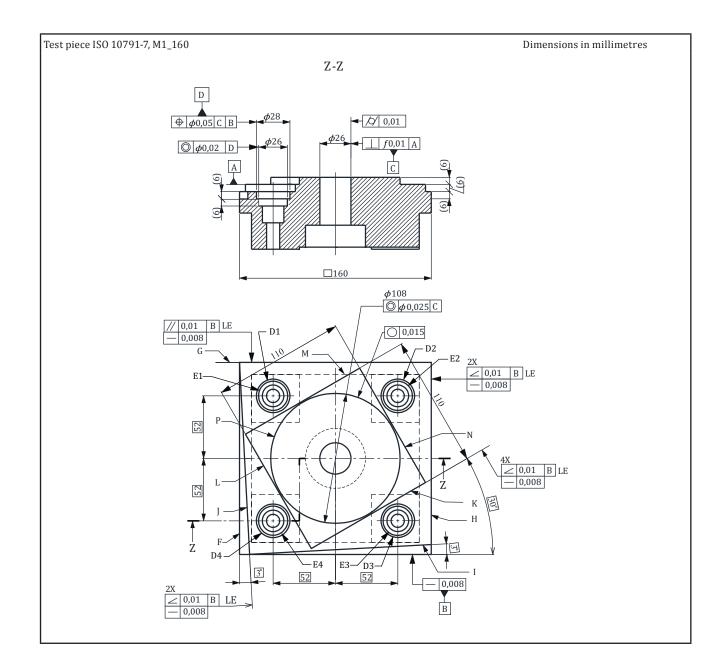
Three sizes of contouring test piece are considered and their dimensions are shown below.

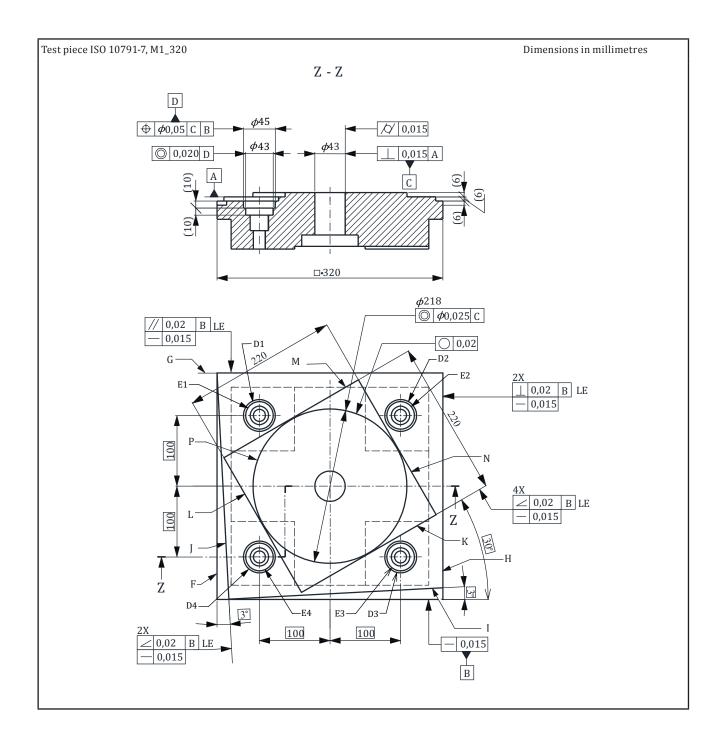
Test piece ISO 10791-7, M1_80:

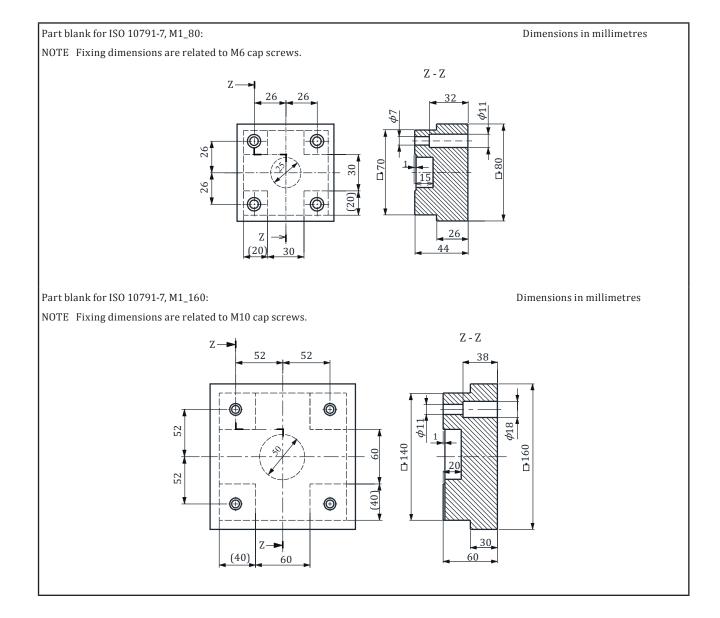
Dimensions in millimetres







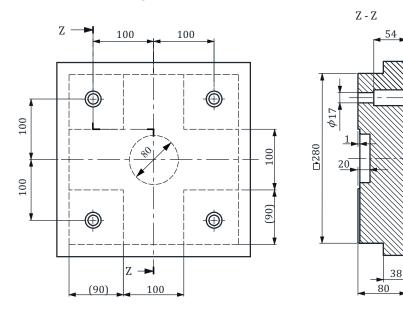




Part blank ISO 10791-7, M1_320:

Dimensions in millimetres

NOTE Fixing dimensions are related to M16 cap screws.



Datum surface B shall be parallel to one of the linear axes.

The bored holes (E) shall be approached in the positive direction of the positioning axes, the counterbored holes (D) shall be approached in the negative direction.

The diamond (K-L-M-N) on the upper face of the square shall only be machined when two linear axes are used (e.g. X and Y).

Sloping faces (I and J), with an angle of 3° and a depth of 6 mm on the top of the external square sides, should only be machined when two linear axes are used (e.g. X and Y).

Since the different contouring surfaces are machined at different axial heights, face contact should be avoided by keeping the tool a fraction of a millimetre apart from the lower plane surface. The overall height of the test piece depends on the selected method of fixing.

Cutting speed should be about 50 m/min for cast iron and 300 m/min for aluminium. Feed rate should be about 0.05 mm/tooth to 0.1 mm/tooth. Depth of cut should be 0.2 mm in the radial direction for all the milling operations and about 6 mm in the axial direction for the slab milling operations.

NOTE The same tool can be used to machine all the contouring test surfaces; an end mill with a cutting edge 35 mm long and 30 mm in diameter is recommended. A boring tool may be used for holes.

Tolerances	Measured deviations		
See <u>Table 2</u> .	See <u>Table 2</u> .		
Measuring instruments			

See Table 2.

Observations and references to ISO 230-1

Preliminary cuts shall be taken in order to make the depth of cut as constant as possible.

Table 2 — Contouring test piece geometric tests

Dimensions in millimetres

Object and references to the drawing			olerance ominal si		Measuring instruments	Measured deviations
	the drawing	80	160	320	instruments	deviations
Central	Cylindricity of the bored hole C	0,010	0,010	0,015	CMM ^a	
hole	Perpendicularity between the hole C axis and datum plane A	0,010	0,010	0,015	СММ	
	Straightness of the side B				СММ	
	Straightness of the side F	0.005	0.008	0.015	or straightness reference artefact and	
	Straightness of the side G	0,005	0,008	0,015	linear displacement	
	Straightness of the side H				sensor	
Square	Perpendicularity of the side H to datum plane B				CMM or squareness	
	Perpendicularity of the side F to datum plane B	0,010	0,010	0,020	reference artefact and linear displacement sensor	
	Parallelism of the side G to datum plane B	0,010	0,010	0,020	CMM or height gauge and linear displacement sensor	
	Straightness of the side K				СММ	
	Straightness of the side L	0.005	0.000	0.015	or straightness reference artefact and linear displacement sensor	
	Straightness of the side M	0,005	0,008	0,015		
Diamond	Straightness of the side N					
Diamonu	Angularity of 30° angle of side K to datum plane B				CMM or sine bar and linear displacement sensor	
	Angularity of 60° angle of side L to datum plane B	0,010	0,010	0,020		
	Angularity of 30° angle of the side M to datum plane B	0,010	0,010	0,020		
	Angularity of 60° angle of the side N to datum plane B					
	Roundness of the contouring circle P	0,015	0,015	0,020	CMM	
Circle	Concentricity of the external circle P and datum hole C	0,025 0,025 0,025		0,025	or linear displacement sensor or roundness-measuring instruments	
	Straightness of the face I				СММ	
Sloping faces	Straightness of the face J	0,005	0,008	0,015	or straightness reference artefact and linear displacement senor	
	Angularity of 3° of the side I to datum plane B	0.040	0.040	0.000	СММ	
	Angularity of 93° of the side J to datum plane B	0,010	0,010	0,020	or sine bar and linear displacement sensor	

NOTE 1 If possible, take the test piece to a coordinate measuring machine (CMM) and take the required measurements.

NOTE 2 To minimize the influence of the test piece distortion due to its clamping, it is recommended to measure the parts while still clamped to the fixture plate.

NOTE 3 For the straight sides (or the square, diamond, and sloping faces), touch the measured surface by the probe at least at 10 points in order to obtain the straightness, perpendicularity, and parallelism deviations.

NOTE 4 For the roundness (or cylindricity) test, if the measurement is not continuous, check at least 15 points (for cylindricity in each measured plane).

a Coordinate measuring machine.

Table 2 (continued)

	Position of the hole D1 with respect to datum hole C		0,050	0.050	СММ	
	Position of the hole D2 with respect to datum hole C	0.050				
	Position of the hole D3 with respect to datum hole C	0,050		0,050		
Bored holes	Position of the hole D4 with respect to datum hole C					
	Concentricity of inner hole E1 with respect to outer hole D1		0,020		CMM or linear displacement sensor with or reference rotary axis, or roundness-measuring instruments	
	Concentricity of inner hole E2 with respect to outer hole D2					
	Concentricity of inner hole E3 with respect to outer hole D3	0,020		0,020		
	Concentricity of inner hole E4 with respect to outer hole D4					

NOTE 1 If possible, take the test piece to a coordinate measuring machine (CMM) and take the required measurements.

NOTE 2 To minimize the influence of the test piece distortion due to its clamping, it is recommended to measure the parts while still clamped to the fixture plate.

NOTE 3 For the straight sides (or the square, diamond, and sloping faces), touch the measured surface by the probe at least at 10 points in order to obtain the straightness, perpendicularity, and parallelism deviations.

NOTE 4 For the roundness (or cylindricity) test, if the measurement is not continuous, check at least 15 points (for cylindricity in each measured plane).

^a Coordinate measuring machine.

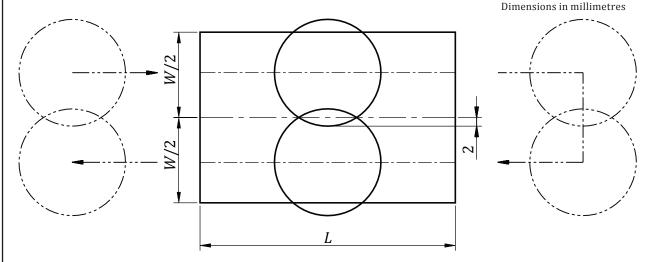
Object M2

Checking the flatness of a surface machined by a finish face milling operation performed by bidirectional two cuts.

If the machine has a universal spindle head, the tests can be performed in other planes as well.

Usually the test is performed by a longitudinal movement along the X- axis and a transverse movement along the Y- axis, but can be performed otherwise, subject to agreement between manufacturer/supplier and user.

Diagram ISO 10791-7, M2_80 and ISO 10791-7, M2_160:



A choice of two sets of dimensions for test piece and relevant tooling is left to agreement between the manufacturer /supplier and the

Face width Face length		Cut width	Cutter diameter
W	L		
Mm	mm	mm	mm
80	100 to 130	40	50
160	200 to 250	80	100

Face milling cutter with indexable inserts (see ISO 6462 and ISO 1832) is recommended. Neither the maximum corner radius nor chamfer of cutter inserts should exceed 2 mm.

Material of the test piece shall be agreed upon between manufacturer/supplier and user of the machine tool. If cast iron is used, with a feed speed of 300 mm/min, the feed per tooth is almost constant and close to 0,12 mm. The depth of cut should not exceed 0,5 mm. The axis square to the machined surface (usually Z) shall not be programmed to move during the test.

Tolerance

Object	Tolerances
Flatness of the machined surface	ISO 10791-7-M2_80: 0,02 ISO 10791-7-M2_160: 0,03

Measured deviations

NOTE The straightness check parallel to the milling direction would show the influence of the ingoing or outgoing of the cutter.

Measuring instruments

Straightness reference artefact, gauge blocks, linear displacement sensor and CMM

Observations and references to ISO 230-1

The blank shall be provided with a base suitable for being fastened to the work holding table/pallet or to a fixture, providing a sufficient stiffness both for horizontal and vertical machines. Preliminary cuts should be taken in order to make the depth of cut as constant as possible.

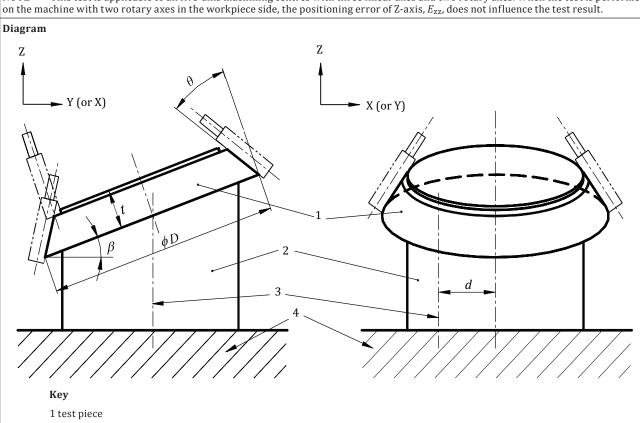
When mounted, the cutter shall conform to the following tolerances:

- a) run-out < 0,02 mm;
- b) run-out of the face at tool diameter < 0,03 mm.

Object М3

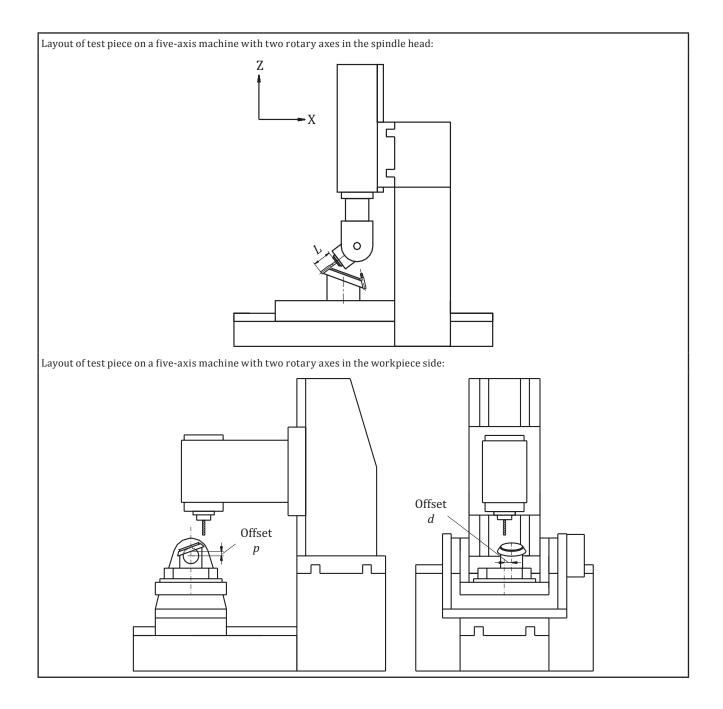
Checking the cutting performance of five-axis machining centres under the five-axis simultaneous feed motion by machining the coneshaped test piece with flank milling.

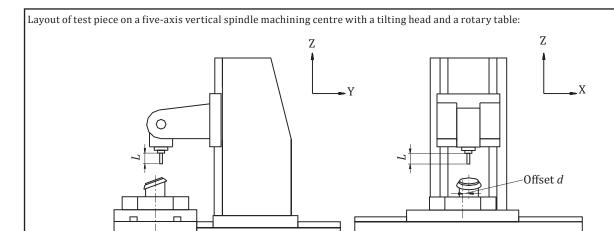
This test is applicable to all five-axis machining centres with three linear axes and two rotary axes. When the test is performed



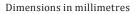
- 2 fixture
- 3 axis average line of rotary table
- 4 rotary table

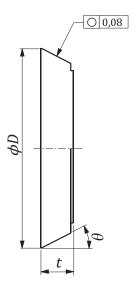
NOTE The diagram above shows the test piece setup in the workpiece coordinate system. Keys 3 and 4 are only for five-axis machining centres with a rotary table. For machines with two rotary axes in the spindle head, the offset d is not needed.





Test piece ISO 10791-7, M3_15 (θ = 15°) and Test piece ISO 10791-7, M3_45 (θ = 45°):





Either of the two alternative conditions (sizes of contouring test piece and setting positions) are considered and their dimensions are given in the table below.

Diameter of bottom surface	Thickness t	Inclination angle β Half apex angle θ		Centre offset d (in case of rotary table)		
Test piece ISO 10791-7-M3_15						
80 mm 20 mm		10° 15°		25 % of the diameter of rotary table size (if possible)		
Test piece ISO 10791-	Test piece ISO 10791-7-M3_45					
80 mm	15 mm	30°	45°	25 % of the diameter of rotary table size (if possible)		

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The final shape of the test piece, as shown in the diagram above, shall result from the following machining:

- a) The test piece should be fixed on the table with inclination angle β to the table surface as shown in the table above.
- b) The bottom centre of the test piece should have the centre offset distance, *d*, as shown in the diagrams above, from the rotary table axis average line (only in case of rotary table). When the test cannot be performed due to limited strokes of linear axes, the offset may be reduced based on an agreement between the manufacturer/supplier and user.
- c) The bottom centre of the test piece shall have an offset *p* from the swiveling axis (only in case of swiveling rotary table), which shall be stated with the test report. The offset *p* is recommended to be larger than 10 % of the table diameter, but may be reduced based on an agreement between the manufacturer/supplier and user.
- d) The outer surface of the frustum shall be machined by flank milling (rough and finish cut allowed). The cutter path shall be circle at constant speed in the workpiece coordinate system.
- e) A ring-shaped flat surface shall be machined on the top surface of the workpiece as the reference for the measurement. It shall be machined by the same cutting tool used for the finishing. It shall be machined by driving linear axes only, with rotary axes fixed.

The test setup can be modified based on an agreement between the manufacturer/supplier and user. For example, on a five-axis machine with a tilting head and a rotary table, the setup shown above may not be possible due to the limitation in the stroke of A-axis or y-axis. In such a case, by installing the test piece with the inclination angle $\beta = 90^{\circ}$ using a square fixture on the machine table, the test may be possible. Note that such a modification may significantly reduce the moving range of each axis compared to the original setup, which often reduces geometric errors of the machined test piece. For example, on a machine with a tilting head and a rotary table, the rotary table makes full (360°) rotation in the original setup, while it does not in the modified setup with $\beta = 90^{\circ}$. Similarly, when the centre offset, d, is reduced, the moving range of each axis often becomes smaller. When the setup is modified, it shall be stated in the report. The tolerances given in Table 3 are for the original setups.

NOTE 1 A flat end mill with a cutting edge 40 mm long and 20 mm in diameter is recommended. When a ϕ 20 tool cannot be used, a smaller tool (e.g. ϕ 10) may be used based on an agreement between the manufacturer/supplier and user. Attention must be paid on the influence of tool deflection.

NOTE 2 Cutting speed, feed speed, and depth of cut shall be agreed upon between manufacturer/supplier and user. As default values, the following may be chosen: cutting speed of 50 m/min for cast iron and 300 m/min for aluminium, feed rate of 0,05 mm/tooth, depth of cut of 0,1 mm in radial direction.

NOTE 3 The dimension of the ring-shaped surface is arbitrary, as long as it can be used as the reference for the measurement.

Tolerance	Measured deviations
See <u>Table 3</u> .	See <u>Table 3</u> .

Measuring instruments

See Table 3.

Observations and references to ISO 230-1

Preliminary cuts shall be taken in order to make the depth of cut as constant as possible.

The information on the inclination angle and centre offset distances, as well as the tool length, L, shall be included in the test report.

If easily available, the range of movement of each axis (three linear axes and two rotary axes) shall be reported.

Table 3 — Cone frustum test piece geometric tests for test pieces ISO 10791-7, M3_15 and ISO 10791-7, M3_45

Dimensions in millimetres

Object	Tolerances	Measuring instru- ments	Measured deviations
Cone upper surface (2 mm apart from top) a) Roundness		Roundness-measuring instruments or CMM ^a or linear displacement sensor and rotary table	a)
a Coordinate measuring machine.			

Table 3 (continued)

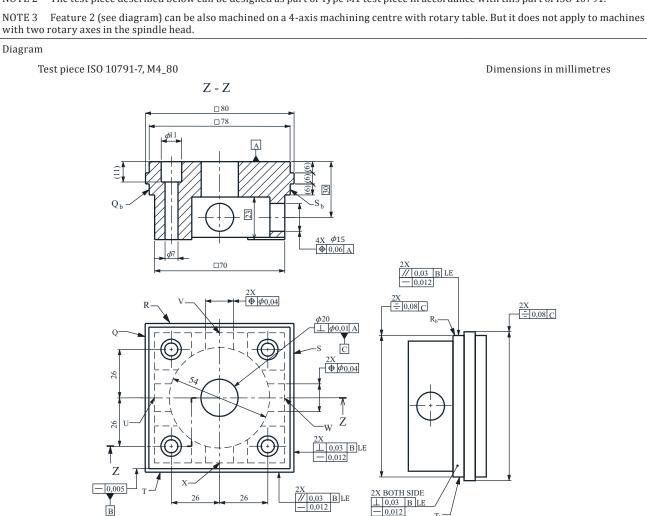
Object	Tolerances	Measuring instru- ments	Measured deviations
Cone lower surface (2 mm apart from bottom) b) Roundness	0,08	Roundness-measuring instruments or CMM or linear displacement sensor and rotary table	b)
a Coordinate measuring machine.			

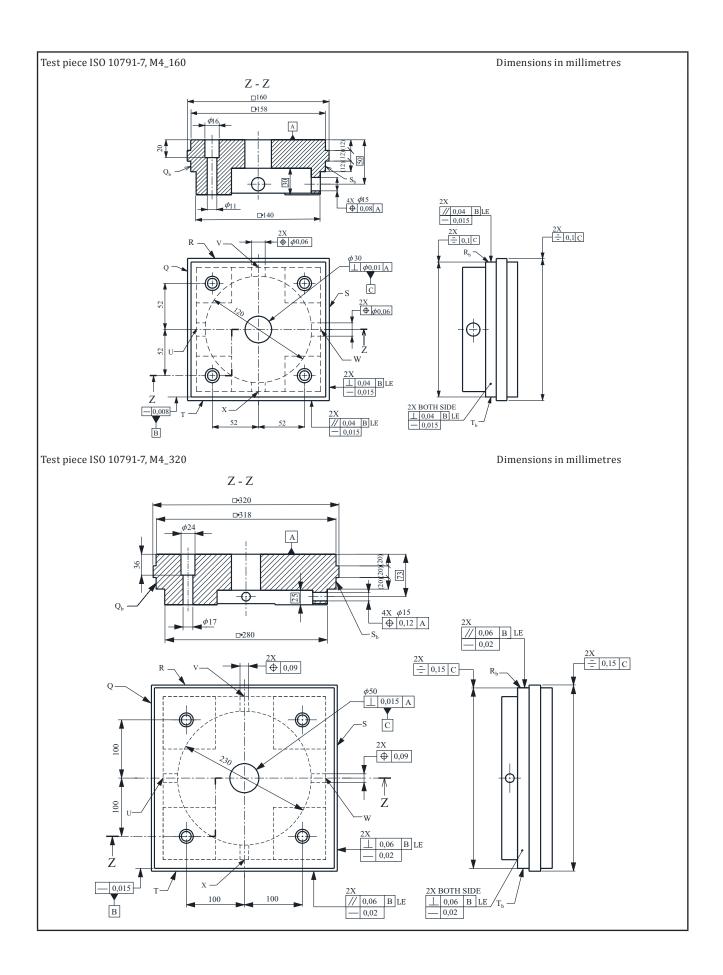
Object M4
Additions to Type M1 test piece

Checking the accuracy of angular positioning and of the position of rotary axis average lines.

NOTE 1 This test is applicable to all five-axis machining centres with three linear and two rotary axes.

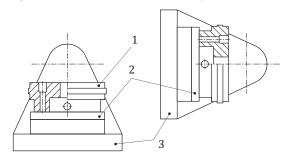
NOTE 2 The test piece described below can be designed as part of Type M1 test piece in accordance with this part of ISO 10791.





The part blanks used for M1 test shall be used as the part blanks for M4 test.

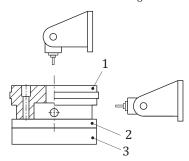
The layout of the test piece on a machine tool with two rotary axes on the workpiece side:



Key

- 1 test piece 2 rotary table 3 cradle

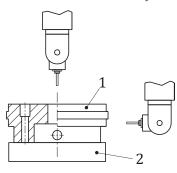
The layout of the test piece on a machine tool with a tilting head and a rotary table:



Key

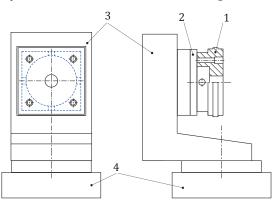
- 1 test piece
- 2 rotary table
- 3 bed

The layout of the test piece on a machine tool with two rotary axes in the spindle side:



- 1 test piece
- 2 work table

The layout of the test piece on a machine with table-on-table configuration:



- 1 test piece
- 2 rotary table3 swivelling table4 table saddle

The final shape of the test piece, as shown in the diagram above, shall result from the following machining sequences:

- a) Feature 1: Top square shall be machined by end milling using two linear motions (X- and Y-axes).
- b) Feature 2: Middle square shall be machined by end milling using one linear and one rotary axis with the following machining sequence (not applicable for machines with two rotary axes in the spindle head):
- 1) end milling of first plane (face) of the square parallel to x-axis;
- 2) rotating test piece with rotary axis C by 90°;
- 3) end milling of next plane parallel to X;
- 4) repetition of 2) and 3) until all 4 planes are end milled.
- c) Feature 3: Bottom square shall be machined by face milling using one or two linear and one or two rotary axes with the following machining sequence:
- 1) swiveling axis (or tilting head) is rotated by 90°;
- 2) first plane is face milled by moving along a linear axis;
- 3) rotary axis C (table or spindle head) is rotated by 90°;
- 4) next plane is face milled by moving along either same linear axis or the one orthogonal to the first linear axis (for machines with two rotary axes in the spindle head);
- 5) repetition of 3) and 4) until all 4 planes are face milled.

If the swiveling axis (or tilting head) can be rotated by ±90°, the following procedure shall be applied:

- 6) swiveling axis (or tilting head) is rotated by 90°;
- 7) first plane is face milled by moving along a linear axis;
- 8) rotary axis C (table or spindle head) is rotated by 180°;
- 9) second plane is face milled by moving along the same linear axis (this may require preparatory move along the orthogonal axis);
- 10) swiveling axis (or tilting head) is rotated by -180°, rotary axis C (table or spindle head) is rotated by -90°;
- 11) third plane is face milled by moving along either the same linear axis or the one orthogonal to the first linear axis (for machines with two rotary axes in the spindle head);
- 12) rotary axis C (table or spindle head) is rotated by 180°;
- 13) forth plane is face milled by moving along the previous linear axis (this may require preparatory move along the orthogonal axis).
- d) Feature 4: Radial holes.
- 1) swiveling axis (or tilting head) is rotated by 90°;
- 2) first hole, dia. 15 mm is machined by circular milling, dia. of tool is 10 mm;
- 3) rotary axis C (table or spindle head) is rotated by 90°;
- 4) next hole is machined by circular milling;
- 5) repetition of 2) and 3) until all 4 holes are machined by circular milling.

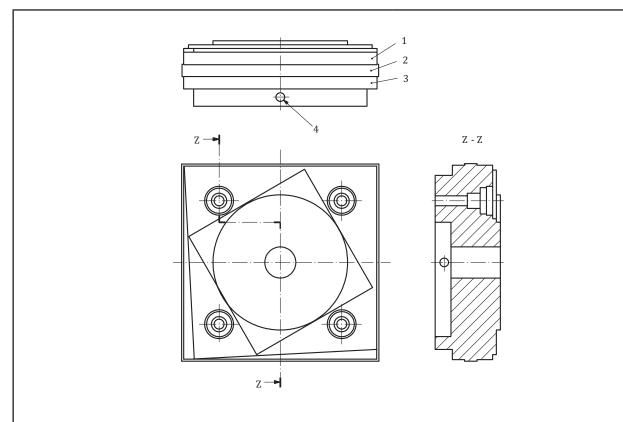
If the swiveling axis (or tilting head) can be rotated by ±90°, the following procedure shall be applied:

- swiveling axis (or tilting head) is rotated by 90°;
- 7) first hole, dia. 15 mm is machined by circular milling, dia. of tool is 10 mm;
- 8) rotary axis C (table or spindle head) is rotated by 180° ;
- 9) second hole is machined by circular milling;
- 10) swiveling axis (or tilting head) is rotated by -180°, rotary axis C (table or spindle head) is rotated by -90°;
- 11) third hole is machined by circular milling;
- 12) rotary axis C (table or spindle head) is rotated by 180°;
- 13) fourth hole is machined by circular milling.

Cutting parameters are subject to agreement between manufacturer/supplier and user of the machine tool.

NOTE 1 M1 and M4 test pieces can be made to one test piece. The following figures represent such embodiments. Alternatively, M1 and M4 test pieces can be combined using proper fixturing that may provide more flexibility in testing.

NOTE 2 Holes can be machined by using a boring tool.



Key

- $1 \hspace{0.1cm}$ feature 1: square feature machined using linear motions along X- and Y-axes
- 2 feature 2: square feature machined using one linear and rotary axis (C)
- 3 feature 3: face milled square feature machined using one linear and two rotary axes
- 4 feature 4: radial holes.

Tolerance

The end-milled square (1) shall satisfy the tolerances given in M1 test piece. Other tolerances are given in <u>Table 4</u>.

Measured deviations

See <u>Table 4</u>.

Measuring instruments

See Table 4.

Observations and references to ISO 230-1

Preliminary cuts shall be taken in order to make the depth of cut as constant as possible.

The distance between the centre positions of the reference bore C and the axis average line of rotary table, as well as the distance between the reference surface C and the axis average line of swivelling axis, shall be reported.

Table 4 — Three-step square test piece geometric tests for test pieces ISO 10791-7, M4_80, _160, and _320

Dimensions in millimetres

	Object and references to the drawing		olerance ominal si		Measuring instruments	Measured deviations
	, g	80	160	320	instruments	deviations
	Straightness of the side Q		,012 0,015			
	Straightness of the side R	0,012		0.02	CMM ^a or straightness reference artefact and	
	Straightness of the side S			0,02	linear displacement sensor	
	Straightness of the side T				School	
Ne: 1 11	Symmetry to datum hole C	0,08	0,1	0,15	CMM	
Middle square	Squareness of the side Q to datum plane B				CMM or squareness	
	Squareness of the side S to datum plane B	0,03	0,04	0,06	reference artefact and linear displacement sensor	
	Parallelism of the side R to datum plane B				CMM or height gauge	
	Parallelism of the side T to datum plane B				and linear displace- ment sensor	
	Difference of size between planes in X and Y	0,1	0,12	0,18	CMM	
	Straightness of the side Q_{b}	0,012			CMM or straightness reference artefact and	
	Straightness of the side $R_{\rm b}$		0.015	0,02		
	Straightness of the side S_b		0,015	0,02	linear displacement sensor	
	Straightness of the side T_b					
	Symmetry to datum hole C	0,08	0,1	0,15	CMM	
Bottom square	Squareness of the side $Q_{\boldsymbol{b}}$ to datum plane \boldsymbol{B}				CMM or squareness reference artefact and linear displacement sensor CMM or height gauge and linear displacement sensor	
	Squareness of the side S_b to datum plane B	0,03	0,04 0,06	0,06		
	Parallelism of the side $R_{\mbox{\scriptsize b}}$ to datum plane B					
	Parallelism of the side $T_{\mbox{\scriptsize b}}$ to datum plane B					
	Difference of size between planes in X and Y	0,1	0,12	0,18	CMM	
	Difference of hole U position in distance to datum plane A					
	Difference of hole V position in distance to datum plane A	0,06	0,08	0,12	СММ	
Radial	Difference of hole W position in distance to datum plane A	0,06	0,06	0,12	CIVIW	
holes	Difference of hole X position in distance to datum plane A					
	Difference of hole U position to hole W	0,04	0,06	0,09	CMM	
	Difference of hole V position to hole X	0,04	0,00	0,09	CMM	

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