BS ISO 606:2015



### **BSI Standards Publication**

Short-pitch transmission precision roller and bush chains, attachments and associated chain sprockets



BS ISO 606:2015 BRITISH STANDARD

#### National foreword

This British Standard is the UK implementation of ISO 606:2015.

The UK participation in its preparation was entrusted to Technical Committee MCE/1, Chains and chain sprockets for power transmission.

A list of organizations represented on this committee can be obtained on request to its secretary.

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ISBN 978 0 580 82025 0

ICS 21.220.30

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This British Standard was published under the authority of the Standards Policy and Strategy Committee on 31 August 2015.

Amendments/corrigenda issued since publication

Date Text affected

## INTERNATIONAL STANDARD

ISO 606:2015 606

Fourth edition 2015-08-15

# Short-pitch transmission precision roller and bush chains, attachments and associated chain sprockets

Chaînes de transmission de précision à rouleaux et à douilles, plaquesattaches et roues dentées correspondantes



BS ISO 606:2015 ISO 606:2015(E)



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#### Foreword

ISO (the International Organization for Standardization) is a worldwide federation of national standards bodies (ISO member bodies). The work of preparing International Standards is normally carried out through ISO technical committees. Each member body interested in a subject for which a technical committee has been established has the right to be represented on that committee. International organizations, governmental and non-governmental, in liaison with ISO, also take part in the work. ISO collaborates closely with the International Electrotechnical Commission (IEC) on all matters of electrotechnical standardization.

The procedures used to develop this document and those intended for its further maintenance are described in the ISO/IEC Directives, Part 1. In particular the different approval criteria needed for the different types of ISO documents should be noted. This document was drafted in accordance with the editorial rules of the ISO/IEC Directives, Part 2 (see <a href="www.iso.org/directives">www.iso.org/directives</a>).

Attention is drawn to the possibility that some of the elements of this document may be the subject of patent rights. ISO shall not be held responsible for identifying any or all such patent rights. Details of any patent rights identified during the development of the document will be in the Introduction and/or on the ISO list of patent declarations received (see <a href="www.iso.org/patents">www.iso.org/patents</a>).

Any trade name used in this document is information given for the convenience of users and does not constitute an endorsement.

For an explanation on the meaning of ISO specific terms and expressions related to conformity assessment, as well as information about ISO's adherence to the WTO principles in the Technical Barriers to Trade (TBT) see the following URL: Foreword - Supplementary information

The committee responsible for this document is ISO/TC 100, *Chains and chain sprockets for power transmission and conveyors*.

This fourth edition cancels and replaces the third edition (ISO 606:2004), which has been technically revised. It also incorporates Technical Corrigendum ISO 606:2004/Cor. 1:2006.

#### Introduction

The provisions of this revised International Standard have been established by including sizes of chains used by the majority of countries in the world, and by unifying dimensions, strengths and other data which differed in current national standards, while eliminating those for which it was considered a universal usage had not been established.

The whole field of application open to this medium of transmission has been covered by the ranges of chains already established. To achieve this, the sizes of 6,35 mm pitch to 76,2 mm pitch inclusive have been duplicated, on the one hand, by the inclusion of chains derived from standards originating and centred around ANSI, and on the other by chains representing the unification of the principal standards originating in Europe, the two being complementary for the coverage of the widest possible field of application.

The ANSI chain reference numbers (25, 35, 40, 50, etc.) are used world-wide and these numbers have now been introduced into this International Standard in place of the previous ISO reference numbers (04C, 06C, 08A, 10A, etc.) To assist in cross-referencing the ANSI and previous ISO numbers, details are included in Annex B of this International Standard.

The ANSI heavy series of chains (suffix H) are specified in this International Standard. The ANSI heavy series of chains differs from the ANSI standard series in that thicker plates are used.

The ANSI extra heavy series of chains (suffix HE) are now included. The ANSI extra heavy series are dimensionally as the ANSI heavy series (suffix H) but have a higher minimum ultimate tensile strength.

<u>Clause 4</u> covers specification details for K and M attachments, and extended pin attachments for use with short-pitch transmission roller and bush chains conforming with this International Standard.

<u>Clause 5</u>, covering chain sprockets, represents the unification of all the relevant national standards in the world and includes, in particular, complete tolerances relating to tooth form.

The inclusion of the dimensions of the chains specified ensures complete interchangeability of any given size and provides interchangeability of individual links of chains.

## Short-pitch transmission precision roller and bush chains, attachments and associated chain sprockets

#### 1 Scope

This International Standard specifies the characteristics of short-pitch precision roller and bush chains with associated sprockets suitable for the mechanical transmission of power and allied applications. It covers dimensions, tolerances, length measurement, preloading, minimum tensile strengths and minimum dynamic strength.

Although <u>Clause 5</u> applies to chain sprockets for cycles and motor cycles, this International Standard is not applicable to their chains, which are covered by ISO 9633 and ISO 10190, respectively.

#### 2 Normative references

The following documents, in whole or in part, are normatively referenced in this document and are indispensable for its application. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

ISO 286-2:2010, Geometrical product specifications (GPS) — ISO code system for tolerances on linear sizes — Part 2: Tables of standard tolerance classes and limit deviations for holes and shafts

ISO 15654, Fatigue test method for transmission precision roller chains

#### 3 Chains

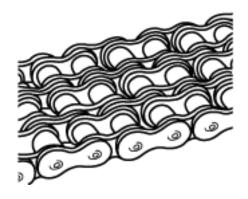
#### 3.1 Nomenclature of assemblies and components

The nomenclature of chain assemblies and their component parts is shown in Figures 1 and  $\frac{2}{2}$  (which do not define the actual form of the chain plates).



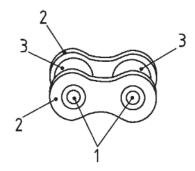
a) Simplex chain

b) Duplex chain



c) Triplex chain

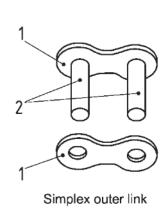
Figure 1 — Types of roller chain assembly

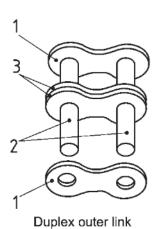


a) Inner link

#### Key for a)

- 1 bush
- 2 inner plate
- 3 roller

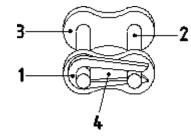


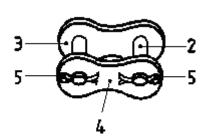


b) Outer links for riveting

#### Key for b)

- 1 outer plate
- 2 bearing pins
- 3 intermediate plate(s)



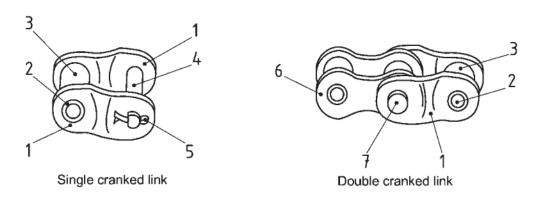


#### c) Detachable connecting links

#### Key for c)

- 1 spring clip fastener
- 2 fixed connecting pin
- 3 outer plate

- 4 detachable plate
- 5 cotter pin fastener



#### d) Cranked links

#### Key for d)

- 1 cranked plate
- 2 bush
- 3 roller
- 4 detachable connecting pin

- 5 cotter pin fastener
- 6 inner plate
- 7 bearing pin, riveted
- NOTE 1 The plate dimensions are specified in <u>Tables 1</u> and <u>2</u>.
- NOTE 2 Fasteners can be of various designs. Drawings indicate examples.

Figure 2 — Types of link

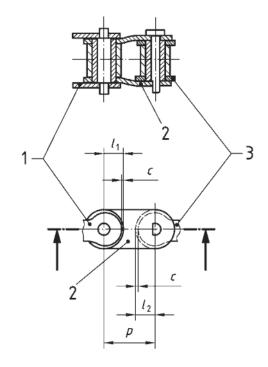
#### 3.2 Designation

Chains are designated by the standard ISO chain number given in <u>Tables 1</u> and <u>2</u>. The ISO chain numbers in <u>Table 1</u> are supplemented by a hyphenated suffix 1 for simplex chain, 2 for duplex chain and 3 for triplex chain, for example, 16B-1, 16B-2, 16B-3, 80-1, 80-2, 80-3. Chains 081, 083, 084 and 41 do not follow this procedure since they are normally available in simplex form only.

The chains designated in <u>Table 2</u> are the ANSI heavy and extra heavy series, which are also supplemented by a hyphenated suffix 1 for simplex chain, 2 for duplex chain and 3 for triplex chain, for example, 80H-1, 80H-2, 80H-3, 80HE-1, 80HE-3.

#### 3.3 Dimensions

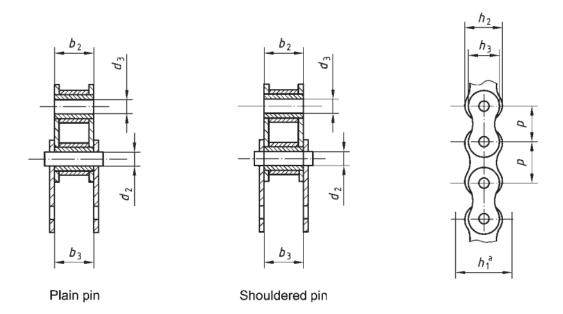
Chains shall conform to the dimensions shown in <u>Figure 3</u> and given in <u>Tables 1</u> and <u>2</u>. Maximum and minimum dimensions are specified to ensure interchangeability of links produced by different makers of chain. They represent limits for interchangeability, but are not the manufacturing tolerances.



a) Cranked link

#### Key for a)

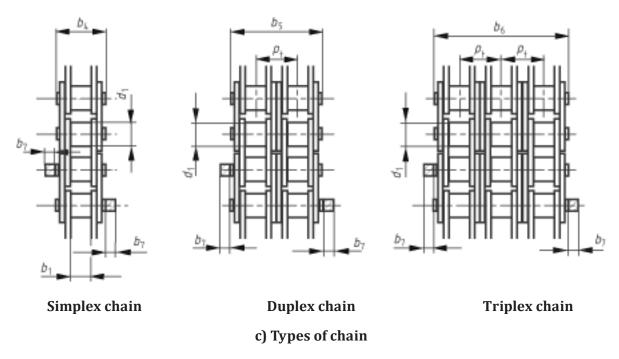
- c clearance between cranked link plates and straight plates available during articulation
- p pitch
- 1 outer plate
- 2 cranked plate
- 3 inner plate



#### b) Sections through chain

#### Key for b)

a Chain path depth is the minimum depth of channel through which the assembled chain will pass



NOTE For the symbols, see <u>Table 1</u>.

Figure 3 — Chains

The overall width of a simplex, duplex or triplex chain with a joint fastener is given by

a) for riveted pin end chains if the fastener is on one side only:

$$(b_4 + b_7)$$
 or  $(b_5 + b_7)$  or  $(b_6 + b_7)$ ;

b) for riveted pin end chains if the fastener is on two sides:

$$[b_4 + (2b_7)]$$
 or  $[b_5 + (2b_7)]$  or  $[b_6 + (2b_7)]$ ;

c) for headed pin end chains if the fastener is on one side only:

$$[b_4 + (1,6b_7)]$$
 or  $[b_5 + (1,6b_7)]$  or  $[b_6 + (1,6b_7)]$ ;

d) for headed pin end chains if the fastener is on two sides:

$$[b_4 + (3,2b_7)]$$
 or  $[b_5 + (3,2b_7)]$  or  $[b_6 + (3,2b_7)]$ .

The overall width of chains wider than triplex is given by

 $b_4 + [p_t \times (\text{number of strands in chain } -1)].$ 

#### 3.4 Performance requirements

#### 3.4.1 General

WARNING — The test requirements are not to be taken as working loads. These loads could be selected, indirectly, using ISO 10823. The test results shall be invalid if the chain has previously been in service or stressed in any way (other than by preloading in accordance with 3.4.3).

The tests given in  $\underline{3.4.2}$  to  $\underline{3.4.5}$  shall only be performed on unused, undamaged chains to determine whether the subject chain complies with the minimum requirements specified in  $\underline{\text{Tables 1}}$  and  $\underline{2}$ .

#### 3.4.2 Tensile testing

**3.4.2.1** The minimum tensile strength is that value which shall be exceeded when a tensile force is applied to a sample tested to destruction in accordance with **3.4.2.2** 

NOTE This minimum tensile strength is not a working load, but is intended primarily as a comparative figure between chains of various constructions.

**3.4.2.2** Apply a tensile force slowly to the ends of a chain length containing at least five free pitches by means of fixtures permitting free movement on both sides of the chain centreline, in the normal plane of articulation. **Annex E** (informative) describes methods to consider using in order to avoid an excessive increase in the rate of stress being applied to the chain during the tensile test.

Failure shall be considered to have occurred at the first point where increasing extension is no longer accompanied by increasing force, i.e. the summit of the force/extension diagram. The force at this point shall exceed the minimum tensile strength stated in <u>Tables 1</u> and <u>2</u>.

Tests in which failures occur adjacent to the shackles shall be disregarded.

- **3.4.2.3** The tensile test shall be considered as a destructive test. Even though a chain might not visibly fail when subjected to a force equivalent to the minimum tensile strength, it will have been stressed beyond the yield point and will be unfit for service.
- **3.4.2.4** These requirements do not apply to cranked links, connecting links or chains with attachments, as their tensile strength could be reduced.

#### 3.4.3 Preloading

Chains manufactured in conformance with this International Standard shall be preloaded by applying a minimum tensile force equivalent to 30 % of the minimum tensile strength given in <u>Tables 1</u> and <u>2</u>.

#### 3.4.4 Length validation

Measurement of chains shall take place after preloading but before lubrication.

The standard length for measurement shall be a minimum of

- a) 610 mm for ISO chain numbers 25 to 12B and 081 to 41 inclusive, or
- b) 1 220 mm for ISO chain numbers 80 to 72B inclusive.

The chain shall be supported throughout its entire length and the measuring force specified in  $\underline{\text{Tables 1}}$  and  $\underline{\text{2}}$  shall be applied.

The measured length shall be the nominal length  ${}^{+0,15}_0\%$ , except for chains with attachments when it shall be the nominal length  ${}^{+0,30}_0\%$ .

The length accuracy of chains which have to work in parallel can be matched within closer tolerances.

#### 3.4.5 Dynamic testing

Chains in conformance with this International Standard shall survive a conformance test, as specified in ISO 15654, using the dynamic strength values given in  $\underline{\text{Tables 1}}$  or  $\underline{\text{2}}$  for the particular chain. These requirements do not apply to cranked links, connecting links or chains with attachments, as their dynamic strength could be reduced. The methods used for calculating the minimum dynamic strength are given in  $\underline{\text{Annex C}}$ . The method for determining the maximum test force for the conformance test is given in  $\underline{\text{Annex D}}$ . The informative  $\underline{\text{Annex F}}$  describes two methods used to approximate the minimum dynamic test values for multiplex chains.

#### 3.5 Marking

The chain shall be marked with the manufacturer's name or trademark. The chain number quoted in <u>Tables 1</u> or <u>2</u> should be marked on the chain, with the exception of chains in the ANSI extra heavy series (suffix HE) where the manufacturer can mark the chains with their own designation.

#### 3.6 Cranked links

Cranked links should not be used with the heavy and extra heavy series chains or on chains which are intended for highly stressed applications. Where a cranked link is used a reduction in performance will occur.

Table 1 — Principal chain dimensions, measuring forces, tensile strengths and dynamic strength values (see Figures 1 and 3)

dynamic strength 1 ,9 , <sup>b</sup> xəlqmi2	niM		$\mathbf{F}_{\mathbf{d}}$	Z	630	1410	820	1 290	2 480	2 480	ı	I	ı	1 340	3 850	3 330	5 490	3 720	9 550	9 530	14 600	13 500	20 500	19 700	27 300
ength		Triplex			10,5	23,7	11,1	24,9	41,7	44,5	1	_	1	_	65,4	66,7	93,9	86,7	166,8	160,0	261,0	250,0	375,0	425,0	510,0
Minimum tensile strength	Chain	Duplex	Fu	ķN	7,0	15,8	7,8	16,9	27,8	31,1	I	I	1	I	43,6	44,5	62,6	57,8	111,2	106,0	174,0	170,0	250,0	280,0	340,0
Minimum		Simplex			3,5	6,7	4,4	8,9	13,9	17,8	8,0	11,6	15,6	6,7	21,8	22,2	31,3	28,9	22,6	0'09	0'28	95,0	125,0	160,0	170,0
4)		Triplex			150	210	150	210	370	370	1	ı	1	1	290	290	840	840	1 490	1 490	2 340	2 340	3 340	3 340	4 540
Measuring force	Chain	Duplex		z	100	140	100	140	250	250	ı	ı	1	1	390	390	260	260	1 000	1 000	1 560	1 560	2 220	2 220	3 020
Meas		Simplex			20	70	50	70	120	120	125	125	125	08	200	200	280	280	200	200	780	780	1 110	1 110	1 510
vimum additional width for joint fastener <sup>C</sup>	æM		b <sub>7</sub>		2,5	3,3	3,1	3,3	3,9	3,9	1,5	1,5	1,5	2,0	4,1	4,1	4,6	4,6	5,4	5,4	6,1	6,1	9'9	9'9	7,4
wer		Triplex	$p_6$		21,8	33,5	19,9	34,0	46,7	44,9	ı	_	1	_	6'29	52,8	72,6	61,7	91,9	6'66	113,0	116,1	141,7	150,2	152,4
Maximum width over bearing pins	Chain	Duplex	p²		15,5	23,4	14,3	23,8	32,3	31,0	ı	-	I	_	6'68	36,2	49,8	42,2	62,7	0,89	0,77	7,67	6'96	101,8	103,6
Maximu bea		Simplex	$\mathbf{b}_4$		9,1	13,2	9,8	13,5	17,8	17,0	10,2	12,9	14,8	14,0	21,8	19,6	26,9	22,7	33,5	36,1	41,1	43,2	50,8	53,4	54,9
nimum width between outer plates	iM		$\mathbf{p}_3$		4,85	7,52	4,90	8,66	11,23	11,43	5,93	8,03	8,93	9,12	13,89	13,41	17,81	15,75	22,66	25,58	27,51	29,14	35,51	38,05	37,24
dmum width over inner Jink	æM		$\mathbf{b}_2$		4,80	7,46	4,77	8,53	11,17	11,30	5,80	2,90	8,80	90'6	13,84	13,28	17,75	15,62	22,60	25,45	27,45	29,01	35,45	37,92	37,18
Transverse pitch			pt		6,40	10,13	5,64	10,24	14,38	13,92	ı	_	ı	_	18,11	16,59	22,78	19,46	29,29	31,88	32,76	36,45	45,44	48,36	48,87
ed .			၁		0,10	0,10	80'0	80'0	80'0	80'0	80'0	80'0	80'0	80'0	0,10	0,10	0,10	0,10	0,13	0,13	0,15	0,15	0,18	0,18	0,20
m crank iensions			$l_2$	ш	3,08	4,60	3,71	4,32	6,10	6,12	5,36	5,36	5,77	5,03	7,62	7,62	9,15	8,33	12,20	11,15	15,24	13,89	18,27	17,55	21,32
Minimum cranked link dimensions			$l_1$	mm	2,65	3,97	3,71	4,32	5,29	99'5	5,36	5,36	5,77	4,35	6,61	7,11	7,90	8,33	10,55	11,15	13,16	13,89	15,80	17,55	18,42
Maximum outer or ermediate plate depth	ıui		h <sub>3</sub>		5,21	7,81	7,11	8,26	10,42	10,92	9,91	10,30	11,15	8,51	13,02	13,72	15,62	16,13	20,83	21,08	26,04	26,42	31,24	33,40	36,45
imum inner plate depth	xsM		$h_2$		6,02	9,05	7,11	8,26	12,07	11,81	9,91	10,30	11,15	9,91	15,09	14,73	18,10	16,13	24,13	21,08	30,17	26,42	36,2	33,4	42,23
ітит сһгіп рәth dерth	niM		$h_1$		6,27	9,30	7,37	8,52	12,33	12,07	10,17	10,56	11,41	10,17	15,35	14,99	18,34	16,39	24,39	21,34	30,48	26,68	36,55	33,73	42,67
Minimum bush bore			d <sub>3</sub>		2,34	3,62	2,36	3,33	4,00	4,50	3,71	4,14	4,14	3,62	5,12	5,13	5,98	5,77	2,96	8,33	92'6	10,24	11,14	14,68	12,74
imum bearing pin body diameter	xsM		$\mathbf{q}_2$		2,31	3,60	2,31	3,28	3,98	4,45	3,66	4,09	4,09	3,60	2,09	5,08	5,96	5,72	7,94	8,28	9,54	10,19	11,11	14,63	12,71
nimum width between inner plates	iM		$\mathbf{b}_1$		3,10	4,68	3,00	5,72	7,85	7,75	3,30	4,88	4,88	6,25	9,40	6,65	12,57	11,68	15,75	17,02	18,90	19,56	25,22	25,40	25,22
ıximum roller diameter	sМ		$d_1$		3,30 g	5,08 g	2,00	6,35	7,92	8,51	7,75	27,75	7,75	77,77	10,16	10,16	11,91	12,07	15,88	15,88	19,05	19,05	22,23	25,40	25,40
Pitch			d		6,35	9,525	8,00	9,525	12,70	12,70	12,70	12,70	12,70	12,70	15,875	15,875	19,05	19,05	25,40	25,40	31,75	31,75	38,10	38,10	44,45
ISO Chain number a					25	35	05B	06B	40	08B	081	880	084	41	20	10B	09	12B	80	16B	100	20B	120	24B	140

Table 1 — (continued)

ile streength imum dynamic str Simplex <sup>d, e,</sup>	Chain	Duplex Triplex	F <sub>u</sub> F <sub>d</sub>	kN N	360,0 530,0 27 100	0'699	450,0 670,0 29 900	562,0 843,0 44500	694,0 1 041,0 53 600	630,0 950,0 41800	000,0 1500,0 73100	1 000,0 1 500,0 63 600	600,0 2 240,0 88 900	000,0 3 000,0 106 900	500,0 3 750,0 132 700			ufacturer.		should not be proportioned from the simplex test value, Appendix F details methods of calculation for when an approximation is required.	ach of 5 free pitches except for 180, 200, 40B, 240, 48B, 56B, 64B and 72B chains which are based on test specimens each of 3 free pitches.	
Minimum tensile strength	Ch	Simplex Duj	F	А	200,0 36		250,0 45	281,0 56	347,0 69	355,0 63	500,0 1 0	560,0 1 0	850,0 1 6	1 120,0 2 00	1 400,0 2 50			The actual dimensions will depend on the type of fastener used, they should not exceed the dimensions given, details of which should be obtained by the purchaser from the manufacturer.		an approxim	cimens each	
93		Triplex			4 540	6 010	6 010	8 010	9 340	9 340	13 340	13 340	20 000	27 000	33 500			urchaser		for when	n test spe	
Measuring force	Chain	Duplex		Z	3 020	4 000	4 000	5 340	6 230	6 230	8 900	8 900	12 190	15 920	20 190			d by the p		alculation	re based o	
		Simplex			1 510	2 000	2 000	2 670	3 110	3 110	4 450	4 450	9 060	7 960	10 100			e obtaine		hods of c	which ar	
dimum additional width for joint fastener C	квМ		b <sub>7</sub>		7,4	7,9	7,9	9,1	10,2	10,2	10,5	10,5	11,7	13,0	14,3			od bluc		ls met	chains	
h over 1s		Triplex	$p_6$		184,3	182,9	184,5	206,0	223,5	227,2	271,3	281,6	327,8	370,7	420,0			thich sho		x F detai	and 72B	
Maximum width over bearing pins	Chain	Duplex	$\mathbf{p}_{5}$		124,7	124,2	126,0	140,0	151,9	154,9	183,4	190,4	221,2	250,8	283,7			tails of w		Appendi	5B, 64B a	
Maxir b		Simplex	$b_4$		65,1	65,5	67,4	73,9	80,3	82,6	95,5	99,1	114,6	130,9	147,4			given, de	ents.	st value,	), 48B, 50	
inimum width between outer plates	M		$\mathbf{b}_3$		46,71	45,26	45,70	50,90	54,94	55,88	67,87	69'02	81,46	92,15	103,94			ensions g	attachm	nplex te	40B, 24(	
ximum width over inner	æM		$\mathbf{b}_2$		46,58	45,21	45,57	50,85	54,88	55,75	67,81	70,56	81,33	92,02	103,81			the dime	ns with	n the sir	30, 200,	
Transverse pitch			$p_{\rm t}$		95'65	58,55	58,55	65,84	71,55	72,29	87,83	91,21	106,60	119,89	136,27			peaced	l links or connecting links or chains with attachments	ned fror	pt for 18	
ıked ns b			C		0,20	0,20	0,20	0,20	0,20	0,20	0,20	0,20	0,20	0,20	0,20		S.	ou plu	g link	portic	ss exce	
Minimum cranked link dimensions			$l_2$	mm	19,51	24,33	22,20	27,36	30,36	27,76	36,40	33,45	40,61	47,07	53,37		icatior	y shou	nectir	be pro	pitche	
Minim link di			$l_1$	-	19,51	21,04	22,20	23,65	26,24	27,76	31,45	33,45	40,61	47,07	53,37	2.	ed appl	sed, tho	s or cor	uld not	of 5 free	
Maximum outer or termediate plate depth	ui		$h_3$		37,08	41,68	42,29	46,86	52,07	52,96	62,49	63,88	77,85	90,17	103,63	ee Table 2	ly stress	stener u	ked link	S	ıs each o	
kimum inner plate depth	квМ		$h_2$		37,08	48,26	42,29	54,30	60,33	52,96	72,39	63,88	77,85	90,17	103,63	hains, s	ofhighl	pe of fa	to cran	iplex ch	pecimer	
nmum chain path depth	niM		$h_1$		37,46	48,74	42,72	54,86	60,93	53,49	73,13	64,52	78,64	91,08	104,67	For details of heavy and extra heavy series chains, see	Cranked links are not recommended for use of highly stressed applications.	on the ty	These dynamic strength values do not apply to cranked	Whilst dynamic test values for duplex and triplex chain	Dynamic strength values are based on test specimens e See Annex C for method of calculation.	
Minimum bush bore			$d_3$		15,95	_	17,86	17,49	19,87	22,94	23,84	29,29	34,37	39,45	44,53	a heavy	nendec	epend	es do n	r duple	based o	
kimum bearing pin body diameter	ksM		$d_2$		15,90	_	17,81	17,46	19,85	22,89	23,81	29,24	34,32	39,40	44,48	nd extra	recomi	s will d	rth valu	alues fo	ues are od of ca	
inimum width between inner plates	M		$\mathrm{b}_1$		30,99	_	30,99	35,48	37,85	38,10	47,35	45,72	53,34	96'09	68,58	ieavy ai	are not	nension	cstreng	c test va	igth vali	e.
aximum roller diameter	?W		$d_1$		27,94	28,58	29,21	35,71	39,68	39,37	47,63	48,26	53,98	63,50	72,39	tails of l	ed links	tual din	dynami	dynami	Dynamic strength values are based on See Annex C for method of calculation	Bush diameter
Pitch			d		44,45	-	50,80	57,15	63,50	63,50	76,20	76,20	88,90	101,60	114,30	For de	Cranke	The ac	These	Whilst	Dynar. See An	Bush d
ISO Chain number a					28B	160	32B	180	200	40B	240	48B	56B	64B	72B	В	q	၁	р	ө	Ţ	ρū

Table 2 — Principal dimensions, measuring forces, tensile strengths and dynamic strength values of ANSI heavy and extra heavy series chains

imum dynamic strength <sup>d, e, f</sup>	niM		$\mathbf{F}_{\mathbf{d}}$	N	6 330	10 700	16 000	22 200	29 200	36 900	46 900	58 700	84 400	6 330	10 700	16 000	22 200	29 200	36 900	46 900	58 700	84 400			
ength		Triplex			6'86	166,8	261,0	375,0	510,0	0'699	843,0	1 041,0	1 500,0	124,5	207,6	312,0	438,0	582,0	750,0	933,0	1 248,0	1 992,0			cturer.
Minimum tensile strength	Chain	Duplex	Fu	ΚΝ	62,6	112,2	174,0	250,0	340,0	446,0	562,0	694,0	1 000,0	83,0	138,4	208,0	292,0	388,0	200,0	622,0	832,0	1328,0			The actual dimensions will depend on the type of fastener used, but they should not exceed the dimensions given, details of which should be obtained by the purchaser from the manufacturer.
Minimum		Simplex			31,3	9'22	0'28	125,0	170,0	223,0	281,0	347,0	500,0	41,5	69,2	104,0	146,0	194,0	250,0	311,0	416,0	664,0			r from th
_		Triplex	1		840	1 490	2 340	3 340	4 540	6 010	8 010	9 340	13 340	840	1 490	2 340	3 340	4 540	6 010	8 010	9 340	13 340			purchase
Measuring force	Chain	Duplex		z	260	1 000	1 560	2 220	3 020	4 000	5 340	6 230	8 900	260	1 000	1 560	2 220	3 020	4 000	5 340	6 230	8 900			d by the
Measi		Simplex			280	200	780	1 110	1 510	2 000	2 670	3 110	4 450	280	200	780	1 110	1 510	2 000	2 670	3 110	4 450			e obtaine
ximum additional width for joint fastener <sup>C</sup>	ьМ Г	03	р <sub>2</sub>		4,6	5,4	6,1	9'9	7,4	6,7	9,1	10,2	10,5	4,6	5,4	6,1	9'9	7,4	6'2	9,1	10,2	10,5			ould b
		Triplex	$p_6$		82,4	102,6	122,7	152,8	163,4	193,2	215,7	243,7	313,8	82,4	102,6	122,7	152,8	163,4	193,2	215,7	243,7	313,8			which sh
Maximum width over bearing pins	Chain	Duplex	p <sub>5</sub>		26,3	70,0	9,58	103,9	111,2	131,3	146,5	165,4	212,6	26,3	70,0	83,6	103,9	111,2	131,3	146,5	165,4	212,6			etails of
Maxim		Simplex	$\mathbf{b}_4$		30,2	37,4	44,5	55,0	29,0	69,4	21,3	87,1	111,4	30,2	37,4	44,5	25,0	29,0	69,4	77,3	87,1	111,4			iven, de
nimum width between outer plates	iΜ		p <sup>3</sup>		19,48	24,33	29,16	37,24	38,91	46,94	52,55	58,34	74,60	19,48	24,33	29,16	37,24	38,91	46,94	52,55	58,34	74,60			nsions g
dimum width over inner link	æM		p <sub>2</sub>		19,43	24,28	29,10	37,18	38,86	46,88	52,50	58,29	74,54	19,43	24,28	29,10	37,18	38,86	46,88	52,50	58,29	74,54			e dimer
Transverse pitch			þţ		26,11	32,59	39,09	48,87	52,20	61,90	69,16	78,31	101,22	26,11	32,59	39,09	48,87	52,20	61,90	69,16	78,31	101,22			exceed th
sed s			ပ		0,10	0,13	0,15	0,18	0,20	0,20	0,20	0,20	0,20	0,10	0,13	0,15	0,18	0,20	0,20	0,20	0,20	0,20			d not e
Minimum cranked link dimensions			$l_2$	c	9,15	12,20	15,24	18,27	21,32	24,33	27,36	30,36	36,40	9,15	12,20	15,24	18,27	21,32	24,33	27,36	30,36	36,40	0 40	oms.	v shoul
Minimu Iink dir			$l_1$	шш	7,90	10,55	13,16	15,80	18,42	21,04	23,65	26,24	31,45	7,90	10,55	13,16	15,80	18,42	21,04	23,65	26,24	31,45	mlicati	Jpiileaei	out the
Maximum outer or ermediate plate depth	ıui		h <sub>3</sub>		15,62	20,83	26,04	31,24	36,45	41,66	46,86	52,07	62,49	15,62	20,83	26,04	31,24	36,45	41,66	46,86	52,07	62,49	secod annlications	essen al	r used, l
Maximum inner plate depth			$h_2$		18,10	24,13	30,17	36,20	42,23	48,26	54,30	60,33	72,39	18,10	24,13	30,17	36,20	42,23	48,26	54,30	60,33	72,39		gilly su	fastene
Minimum chain path dtqab			$h_1$		18,34	24,39	30,48	36,55	42,67	48,74	54,86	60,93	73,13	18,34	24,39	30,48	36,55	42,67	48,74	54,86	60,93	73,13	For details of standard series chains, see Table 1. Cranked links are not recommended for use on highly sti	110 251	e type of
Minimum bush bore			d <sub>3</sub>		2,98	7,96	92'6	11,14	12,74	14,31	17,49	19,87	23,84	5,98	7,96	9,56	11,14	12,74	14,31	17,49	19,87	23,84	ns, see	במ זמו ה	d on the
imum bearing pin body	xsM		$d_2$		2,96	7,94	9,54	11,11	12,71	14,29	17,46	19,85	23,81	2,96	7,94	9,54	11,11	12,71	14,29	17,46	19,85	23,81	ies chai	IIIIIciia	depen
літит width between inner plates	iM		$\mathbf{b}_1$		12,57	15,75	18,90	25,22	25,22	31,55	35,48	37,85	47,35	12,57	15,75	18,90	25,22	25,22	31,55	35,48	37,85	47,35	For details of standard series chains, see Table 1.	וחרוברה	ons will
ıximum roller diameter	sМ		$d_1$		11,91	15,88	19,05	22,23	25,40	28,58	35,71	39,68	47,63	11,91	15,88	19,05	22,23	25,40	28,58	35,71	39,68	47,63	of stand	אס מוכ ז.	limensi
Pitch			d		19,05	25,40	31,75	38,10	44,45	50,80	57,15	63,50	76,20	19,05	25,40	31,75	38,10	44,45	50,80	57,15	63,50	76,20	details o	IIII naui	actual c
ISO Chain number a					H09	H08	100H	120H	140H	160H	180H	200H	240H	60HE	80HE	100HE	120HE	140HE	160HE	180HE	200HE	240HE	a For c		c The

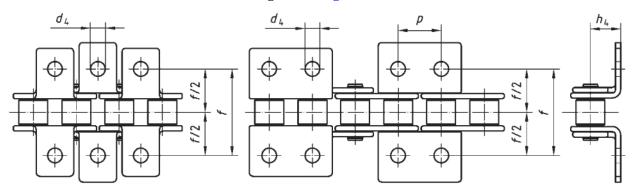
Whilst dynamic test values for duplex and triplex chains should not be proportioned from the simplex test value, Appendix F details methods of calculation for when an approximation is required. These dynamic strength values do not apply to cranked links or connecting links or chains with attachments.

Dynamic strength values are based on test specimens each of 5 free pitches except for 180H, 180HE, 200HE, 200HE, 240H and 240HE chains which are based on test specimens each of 3 free pitches. See Annex C for method of calculation.

#### 4 Attachments

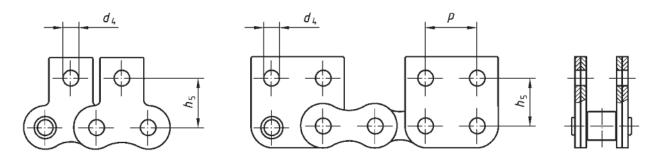
#### 4.1 Nomenclature

The nomenclature for chain attachments is given in Figures 4, 5, 6 and 7, and in Tables 1, 3, 4 and 5.



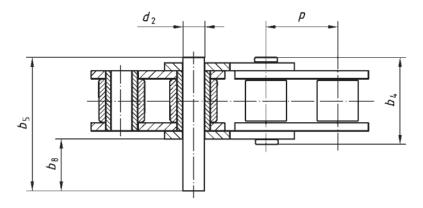
- NOTE 1 For  $d_4$ ,  $h_4$  and f, see <u>Table 3</u>; for p, see <u>Table 1</u>.
- NOTE 2 K attachment plates can be positioned on either outer or inner links.
- NOTE 3 K1 plates could be identical to K2 plates except that they have one hole located centrally.
- NOTE 4 The assembly of K2 plates on adjacent links is not possible.

 $Figure\ 4-K\ attachment\ plates$ 



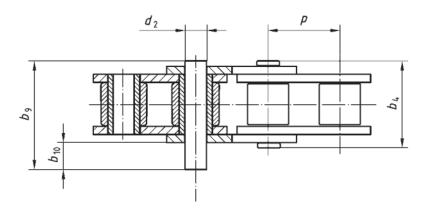
- NOTE 1 For  $d_4$  and  $h_5$ , see <u>Table 4</u>; for p, see <u>Table 1</u>.
- NOTE 2 M attachment plates can be positioned on either outer or inner links.
- NOTE 3 M1 plates could be identical to M2 plates except that they have one hole located centrally.
- NOTE 4 The assembly of M2 plates on adjacent links is not recommended.

Figure 5 — M attachment plates



NOTE For  $b_4$  and p, see <u>Table 1</u>; for  $b_5$ ,  $b_8$  and  $d_2$ , see <u>Table 5</u>.

Figure 6 — Extended bearing pins (based on duplex pin) — Type X



NOTE For  $b_4$  and p, see <u>Table 1</u>; for  $b_9$ ,  $b_{10}$  and  $d_2$ , see <u>Table 5</u>.

Figure 7 — Extended bearing pins (commonly used in "ANSI" series) — Type Y

#### 4.2 General

Except when otherwise stated, the characteristics, dimensions and tests for the chain with attachments shall be in accordance with  $\underline{\text{Clause 3}}$ .

#### 4.3 Designation

Three types of attachment are given, with the common dimensional basis as given in <u>Tables 3</u>,  $\underline{4}$  and  $\underline{5}$ . Their designation and distinguishing features are as follows:

- a) K attachments, as shown in Figure 4:
  - 1) K1, with one attachment hole centrally located in each platform;
  - 2) K2, with two attachment holes longitudinally located;
- b) M attachments, as shown in Figure 5:
  - 1) M1, with one attachment hole centrally located in the plate;

- 2) M2, with two attachment holes longitudinally located;
- c) Extended pin: with the bearing pin extended on one side of the chain as shown in <u>Figures 6</u> and <u>7</u>. Alternative pin extensions are shown, one based on the use of the duplex pin (see <u>Figure 6</u>) and the other based on those extended pins commonly used in "ANSI" series chains (see <u>Figure 7</u>).

#### 4.4 Dimensions

Attachments shall conform to the dimensions given in Tables 3, 4 and 5.

#### 4.5 Manufacture

The actual form of the attachment plates is left to the discretion of the manufacturer. K attachment plates are normally bent from M attachment plates.

The length of the attachment plate is also left to the discretion of the manufacturer, but should be sufficient to accommodate the two attachment holes longitudinally in the case of Type K2 and not interfere with the working of the adjoining links. A common length could be adopted for both Type K1 and K2.

#### 4.6 Marking

It is not a requirement that K and M attachment plates be marked.

The marking of the extended pin chain shall be the same as that which would be shown on a chain with no attachments (see 3.5).

Table 3 — Attachment plate K — Dimensions (see Figure 4)

	Platform height	Minimum hole diameter	Traverse distance between hole centres
ISO chain number	$h_4$	$d_4$	f
	mm	mm	mm
35	6,4	2,6	19,0
40	7,9	3,3	25,4
08B	8,9	4,3	25,4
50	10,3	5,1	31,8
10B	10,3	5,3	31,8
60	11,9	5,1	38,1
12B	13,5	6,4	38,1
80	15,9	6,6	50,8
16B	15,9	6,4	50,8
100	19,8	8,2	63,5
20B	19,8	8,4	63,5
120	23,0	9,8	76,2
24B	26,7	10,5	76,2
140	28,6	11,4	88,9
28B	28,6	13,1	88,9
160	31,8	13,1	101,6
32B	31,8	13,1	101,6
200	42,9	16,3	127,0

Table 4 — Attachment plate M — Dimensions (see Figure 5)

	Height from chain centre line	Minimum diameter of holes
ISO chain number	$h_5$	$d_4$
	mm	mm
35	9,5	2,6
40	12,7	3,3
08B	13,0	4,3
50	15,9	5,1
10B	16,5	5,3
60	18,3	5,1
12B	21,0	6,4
80	24,6	6,6
16B	23,0	6,4
100	31,8	8,2
20B	30,5	8,4
120	36,5	9,8
24B	36,0	10,5
140	44,4	11,4
160	50,8	13,1
200	63,5	16,3

**Table 5 — Extended pin dimensions** (see Figures 6 and 7)

Dimensions in millimetres

	Pin ex	tension	Pin ext	ension <sup>a</sup>	Pin diameter
ISO chain	Тур	e "X"	Тур	e "Y"	Types "X" and "Y"
number	<i>b</i> <sub>8</sub>	<i>b</i> <sub>5</sub>	$b_{10}$	<i>b</i> <sub>9</sub>	$d_2$
	max.	max.	max.	max.	max.
05B	7,1	14,3	_	_	2,31
35	12,3	23,4	10,2	21,9	3,60
06B	12,2	23,8	_	_	3,28
40	16,5	32,3	10,2	26,3	3,98
08B	15,5	31,0	_	_	4,45
50	20,6	39,9	12,7	32,6	5,09
10B	18,5	36,2	_	_	5,08
60	25,7	49,8	15,2	40,0	5,96
12B	21,5	42,2	_	_	5,72
80	32,2	62,7	20,3	51,7	7,94
16B	34,5	68,0	_	_	8,28
100	39,1	77,0	25,4	63,8	9,54
20B	39,4	79,7	_	_	10,19
120	48,9	96,3	30,5	78,6	11,11
24B	51,4	101,8	_	_	14,63
140	_	_	35,6	87,5	12,71
160	_	_	40,6	102,6	14,29
a The pin (	extensions of Type	"Y" are given as alte	rnatives, as they ar	e commonly used i	in "ANSI" series chains.

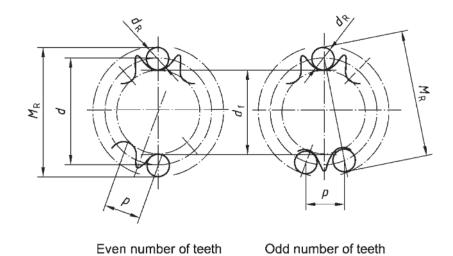
#### 5 Chain sprockets

#### 5.1 General

This clause gives specifications for chain sprockets for use with short-pitch transmission precision roller and bush chains conforming to <u>Clause 3</u> and specifies general criteria for ensuring correct meshing, operation and transmission of load when used under normal operating conditions.

#### 5.2 Nomenclature

The nomenclature for chain sprockets is shown in Figures 8, 9 and 10.



#### Key

p chordal pitch, equal to chain pitch

 $d_{\mathrm{R}}$  measuring-pin diameter

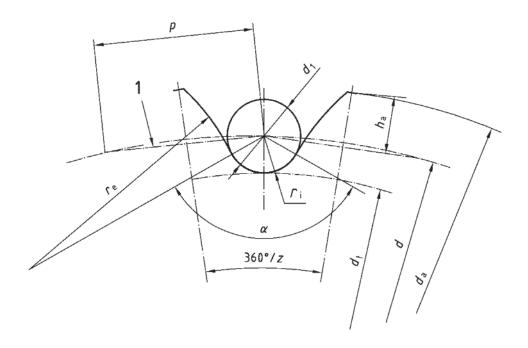
*d* pitch-circle diameter

df root diameter

 $M_{\rm R}$  measurement over pins

NOTE This nomenclature is valid for both roller and bush chains.

Figure~8-Chain~sprocket~diametral~dimensions

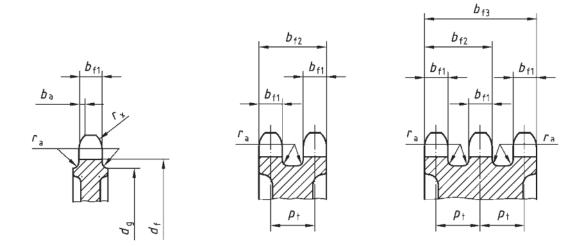


#### Key

- 1 pitch polygon
- p chordal pitch, equal to chain pitch
- d pitch-circle diameter
- $d_1$  maximum roller diameter
- $r_{\rm i}$  roller-seating radius
- $\alpha$  roller-seating angle

- re tooth-flank radius
- *h*<sub>a</sub> height of tooth above pitch polygon
- da tip diameter
- $d_{\rm f}$  root diameter
- z number of teeth

Figure 9 — Tooth gap forms



#### Key

 $b_{
m a}$  tooth side relief  $d_{
m g}$  absolute maximum shroud diameter

 $b_{\mathrm{f1}}$  tooth width  $p_{\mathrm{t}}$  strand transverse pitch  $b_{\mathrm{f2}}, b_{\mathrm{f3}}$  width over teeth  $r_{\mathrm{a}}$  shroud fillet radius  $d_{\mathrm{f}}$  sprocket root diameter  $r_{\mathrm{x}}$  tooth side radius

NOTE For a sprocket rim in the axial plane sectioned through the centre of the tooth gap.

Figure 10 — Sprocket rim profiles

#### 5.3 Diametral dimensions of sprocket rim

#### 5.3.1 Nomenclature

See Figure 8.

#### 5.3.2 Dimensions

#### **5.3.2.1** Pitch-circle diameter, *d*

The chain sprocket pitch-circle diameter, *d*, is given by

$$d = \frac{p}{\sin \frac{180^{\circ}}{7}}$$

Annex A gives the pitch-circle diameter for unit pitch as a function of the number of teeth.

#### **5.3.2.2** Measuring-pin diameter, $d_R$

The chain sprocket measuring-pin diameter  $d_R$  is given by

$$d_{\rm R} = d_1$$

(see Figure 9)

with a tolerance of  ${}^{+0,01}_{0}\,$  mm.

#### **5.3.2.3** Root diameter, $d_{\rm f}$

The chain sprocket root diameter  $d_f$  is given by

$$d_{\rm f} = d - d_1$$

with a tolerance in accordance with Table 6.

Table 6 — Root diameter tolerances

Dimensions in millimetres

Root diameter $d_{ m f}$	Tolerance
<i>d</i> <sub>f</sub> ≤ 127	0 - 0,25
127 < d <sub>f</sub> ≤ 250	0 - 0,3
d <sub>f</sub> > 250	h11a
a See ISO 286-2.	

#### 5.3.2.4 Measurement over pins

For an even number of teeth, the measurement over pins is given by

$$M_{\rm R} = d + d_{\rm R, min}$$

For an odd number of teeth, the measurement over pins is given by

$$M_{\rm R} = d \cos \frac{90^{\circ}}{z} + d_{\rm R, min}$$

The measurement over pins of sprockets with an even number of teeth shall be carried out over pins inserted in opposite tooth gaps.

The measurement over pins of sprockets with an odd number of teeth shall be carried out over pins in the tooth gaps most nearly opposite.

The limits of tolerance for measurement over pins are identical to those for the corresponding root diameters.

#### 5.4 Sprocket tooth gap forms

#### 5.4.1 Nomenclature

See Figure 9.

#### 5.4.2 Dimensions

#### **5.4.2.1** General

The limits of the tooth gap form are determined by the minimum and maximum tooth gap forms. The actual tooth gap form, which is provided by cutting or an equivalent method, shall have tooth flanks of a form lying between the minimum and maximum flank radii and blending smoothly with the roller seating curve subtending the respective angles.

#### 5.4.2.2 Minimum form

The corresponding values for  $r_e$ ,  $r_i$  and  $\alpha$  are given by

$$r_{\rm e,max} = 0.12d_1 (z + 2)$$

$$r_{i,min} = 0.505d_1$$

$$\alpha_{\text{max}} = 140^{\circ} - \frac{90^{\circ}}{z}$$

#### 5.4.2.3 Maximum form

The corresponding values for  $r_e$ ,  $r_i$  and  $\alpha$  are given by

$$r_{\rm e,min} = 0.008d_1 (z^2 + 180)$$

$$r_{i,\text{max}} = 0.505d_1 + 0.069\sqrt[3]{d_1}$$

$$\alpha_{\min} = 120^{\circ} - \frac{90^{\circ}}{z}$$

#### 5.5 Tooth heights and tip diameters

#### 5.5.1 Nomenclature

See Figure 9.

#### 5.5.2 Dimensions

The maximum and minimum values of the tip diameter  $d_a$  are given by

$$d_{a,\text{max}} = d + 1,25p - d_1$$

$$d_{\text{a,min}} = d + p \left(1 - \frac{1.6}{z}\right) - d_1$$

NOTE  $d_{a,min}$  and  $d_{a,max}$  can be applied arbitrarily both to the minimum and maximum gap forms, subject to the limitations imposed on the maximum diameter by the cutter.

To facilitate the construction of the tooth gap form to a large scale, the tooth height above the pitch polygon can be obtained from the following formulae:

$$h_{\text{a,max}} = 0.625p - 0.5d_1 + \frac{0.8p}{z}$$

$$h_{a,\min} = 0.5 (p - d_1)$$

NOTE  $h_{a,\text{max}}$  is related to  $d_{a,\text{max}}$  and  $h_{a,\text{min}}$  to  $d_{a,\text{min}}$ .

#### 5.6 Sprocket rim profiles

#### 5.6.1 Nomenclature

See <u>Figure 10</u>.

#### 5.6.2 Dimensions

#### 5.6.2.1 Tooth width

Tooth width dimensions are given by the following:

a) for  $P \le 12,7$  mm:

1)  $b_{f1} = 0.93b_1 : h14^{1}$  for simplex chain sprockets;

2)  $b_{f1} = 0.91b_1 : h14$  for duplex and triplex chain sprockets;

3)  $b_{f1} = 0.88b_1 : h14$  for quadruplex chain wheels and above.

b) for P > 12,7 mm:

1)  $b_{f1} = 0.95b_1 : h14$  for simplex chain sprockets;

2)  $b_{f1} = 0.93b_1 : h14$  for duplex and triplex chain sprockets;

3) The formulae given in a) for quadruplex chains and above may be used by agreement between user and manufacturer.

#### 5.6.2.2 Other dimensions

For all chains:  $b_{f2}$  and  $b_{f3}$  = (number of strands – 1) ×  $p_t$  +  $b_{f1}$  (tolerance h14<sup>2</sup>) on  $b_{f1}$ )

For all chains:  $r_{x,nom} = p$ 

For chain numbers 081, 083, 084 and <u>41</u>:  $b_{a,nom} = 0.06p$ 

For all other chains:  $b_{a,nom} = 0,13p$ 

For chain numbers <u>25</u> and <u>35</u>:  $d_{\rm g} = p \cot \frac{180^{\circ}}{z} - 1,05h_2 - 1,00 - 2r_{\rm a}$ 

For all other chains:  $d_{\rm g} = p \cot \frac{180^{\circ}}{z} - 1,04h_2 - (0,76 \text{ mm})$ 

#### 5.7 Radial run-out

Radial run-out between the bore and root diameter shall not exceed a total indicator reading of greater than the larger of the two following values:

 $(0,000 \ 8 \ d_{\rm f} + 0,08) \ {\rm mm, or}$ 

0.15 mm.

up to a maximum of 0,76 mm.

<sup>1)</sup> See ISO 286-2.

<sup>2)</sup> See ISO 286-2.

#### 5.8 Axial run-out (wobble)

Axial run-out, measured with reference to the bore and the flat part of the side face of the teeth, shall not exceed a total indicator reading of

 $(0,000 9 d_f + 0,08) mm$ 

up to a maximum of 1,14 mm.

For fabricated (welded) sprockets, 0,25 mm is acceptable if the above formula gives smaller values.

#### 5.9 Pitch accuracy of sprocket teeth

Pitch accuracy of sprocket teeth is important and chain manufacturers should be consulted for details.

#### 5.10 Number of teeth

This International Standard primarily applies to a number of teeth from 9 to 150 inclusive.

The preferred numbers of teeth are 17, 19, 21, 23, 25, 38, 57, 76, 95 and 114.

#### 5.11 Bore tolerance

Unless otherwise agreed between manufacturer and purchaser, bore tolerance shall be H8<sup>3</sup>).

#### 5.12 Marking

Sprockets shall be marked with the following:

- a) manufacturer's name or trademark;
- b) number of teeth;
- c) chain designation (ISO chain number and/or manufacturer's equivalent).

<sup>3)</sup> See ISO 286-2.

## **Annex A** (normative)

### Pitch circle diameters

Table A.1 gives the correct pitch circle diameters for sprockets to suit a chain of unit pitch. The pitch circle diameters for sprockets to suit a chain of any other pitch are directly proportional to the pitch of the chain.

Table A.1 — Pitch circle diameters

Number of teeth	Pitch circle diameter, d, for unit pitch <sup>a</sup> mm	Number of teeth	Pitch circle diameter, d, for unit pitch <sup>a</sup> mm	Number of teeth	Pitch circle diameter, d, for unit pitch a mm
9	2,923 8	32	10,202 3	55	17,516 6
10	3,236 1	33	10,520 1	56	17,834 7
11	3,549 4	34	10,838 0	57	18,152 9
12	3,863 7	35	11,155 8	58	18,471 0
13	4,178 6	36	11,473 7	59	18,789 2
14	4,494 0	37	11,791 6	60	19,107 3
15	4,809 7	38	12,109 6	61	19,425 5
16	5,125 8	39	12,427 5	62	19,743 7
17	5,442 2	40	12,745 5	63	20,061 9
18	5,758 8	41	13,063 5	64	20,380 0
19	6,075 5	42	13,381 5	65	20,698 2
20	6,392 5	43	13,699 5	66	21,016 4
21	6,709 5	44	14,017 6	67	21,334 6
22	7,026 6	45	14,335 6	68	21,652 8
23	7,343 9	46	14,653 7	69	21,971 0
24	7,661 3	47	14,971 7	70	22,289 2
25	7,978 7	48	15,2898	71	22,607 4
26	8,296 2	49	15,607 9	72	22,925 6
27	8,613 8	50	15,926 0	73	23,243 8
28	8,931 4	51	16,244 1	74	23,562 0
29	9,249 1	52	16,562 2	75	23,880 2
30	9,5668	53	16,880 3	76	24,198 5
31	9,884 5	54	17,198 4	77	24,516 7

Table A.1 (continued)

Number of teeth	Pitch circle diameter, d, for unit pitch <sup>a</sup> mm	Number of teeth	Pitch circle diameter, d, for unit pitch <sup>a</sup> mm	Number of teeth	Pitch circle diameter, d, for unit pitch a mm
78	24,334 9	105	33,427 5	132	42,020 9
79	25,153 1	106	33,745 8	133	42,339 1
80	25,471 3	107	34,064 0	134	42,657 4
00	23,1713	107	31,001 0	134	12,037 1
81	25,789 6	108	34,382 3	135	42,975 7
82	26,107 8	109	34,700 6	136	43,294 0
83	26,426 0	110	35,018 8	137	43,612 3
84	26,744 3	111	35,337 1	138	43,930 6
85	27,062 5	112	35,655 4	139	44,248 8
86	27,380 7	113	35,973 7	140	44,567 1
87	27,699 0	114	36,291 9	141	44,885 4
88	28,017 2	115	36,610 2	142	45,203 7
89	28,335 5	116	36,928 5	143	45,522 0
90	28,653 7	117	37,246 7	144	45,840 3
91	28,971 9	118	37,565 0	145	46,158 5
92	29,290 2	119	37,883 3	146	46,476 8
93	29,608 4	120	38,201 6	147	46,795 1
94	29,926 7	121	38,519 8	148	47,113 4
95	30,244 9	122	38,838 1	149	47,431 7
96	30,563 2	123	39,156 4	150	47,750 0
97	30,881 5	123	39,474 6	_	47,730 0
98	31,199 7	125	39,792 9		
70	31,1777	123	37,1727		
99	31,518 0	126	40,111 2	_	_
100	31,836 2	127	40,429 5	_	_
101	32,154 5	128	40,474 8	_	_
102	32,472 7	129	41,066 0		
103	32,791 0	130	41,384 3		
104	33,109 3 etimes referred to as "u	131	41,702 6		

## Annex B

(informative)

### **Equivalent chain designations**

See <u>Table B.1</u>.

Table B.1 — Equivalent chain designations

Chain pitch	ISO chain number	Previous ISO chain number
mm		
6,35	25	04C
9,525	35	06C
12,7	40	08A
12,7	41	085
15,875	50	10A
19,05	60	12A
25,4	80	16A
31,75	100	20A
38,1	120	24A
44,45	140	28A
50,8	160	32A
57,15	180	36A
63,5	200	40A
76,2	240	48A

### Annex C

(informative)

### Method of calculating chain minimum dynamic strength

#### C.1 "ANSI" series chain

For <u>41</u> chain only:

$$F_{\rm d} = K_{\rm S} \times A_{\rm i} \times p(-0.000~8~p)$$

For all other chains:

$$F_{\rm d} = K_{\rm S} \times 0.118 \times p(2-0.0008 \, p)$$

where

 $F_{\rm d}$  is the chain minimum dynamic strength at 3 × 106 cycles, in newtons (N);

 $A_i$  is 12,01 mm<sup>2</sup> for 41 chain only;

 $K_{\rm S}$  is

- 115 N/mm<sup>2</sup> for 41 chain only;
- 134 N/mm<sup>2</sup> for chains up to and including 160;
- 139 N/mm<sup>2</sup> for chains 180 and above;
- *p* is the chain pitch, in millimetres (mm).

NOTE Constant  $K_s$  is increased from 134 N/mm<sup>2</sup> to 139 N/mm<sup>2</sup> to allow for the reduction in the test specimen length from 5 free pitches to 3 free pitches when conducting the dynamic strength test.

#### C.2 "ANSI" series heavy and extra heavy chains

$$F_{\rm d} = K_{\rm s} \times 0.118 \times p^{\left(2 - 0.000 \, 8p\right)} \times \left(\frac{b_{\rm i \, heavy}}{b_{\rm i \, standard}}\right)^{0.5}$$

where

 $b_i$  is the estimated inner plate thickness given by

$$\frac{(b_2-b_1)}{2,11}$$
 mm;

 $b_2$  is the maximum width over inner link, in millimetres (mm);

 $b_1$  is the minimum width between inner plates, in millimetres (mm);

 $K_{\rm S}$  is

- 134 N/mm<sup>2</sup> for chains up to and including 160H and 160HE;
- 139 N/mm<sup>2</sup> for chains 180H and 180HE and above;
- *p* is the chain pitch, in millimetres (mm).

NOTE Constant  $K_s$  is increased from 134 N/mm<sup>2</sup> to 139 N/mm<sup>2</sup> to allow for the reduction in the test specimen length from 5 free pitches to 3 free pitches when conducting the dynamic strength test.

#### C.3 "B" series chain

$$F_{\rm d} = K_{\rm S} \times A_{\rm i} \times p(-0.0009p)$$

where

- $A_i$  is the sectional area of inner plate, given by  $2b_i \times (0.99h_2 d_b)$  mm<sup>2</sup>;
- $b_i$  is the estimated inner plate thickness, given by  $\frac{\left(b_2-b_1\right)}{2.11}\,\text{mm}\;;$
- $d_{\rm b}$  is the estimated bush diameter, given by

$$d_2 imes \left(rac{d_1}{d_2}
ight)^{0,475} \mathrm{mm}$$
 ;

- $b_2$  is the maximum width over the inner link, in millimetres (mm);
- $b_1$  is the minimum width between the inner plates, in millimetres (mm);
- $d_2$  is the maximum pin diameter, in millimetres (mm);
- $d_1$  is the maximum roller diameter, in millimetres (mm);
- $h_2$  is the maximum inner plate depth, in millimetres (mm);
- $K_{\rm S}$  is
  - 134 N/mm<sup>2</sup> for chains up to and including 32B;
  - 139 N/mm<sup>2</sup> for chains 40B and above;
- *p* is the chain pitch, in millimetres (mm).

NOTE Constant  $K_s$  is increased from 134 N/mm<sup>2</sup> to 139 N/mm<sup>2</sup> to allow for the reduction in the test specimen length from 5 free pitches to 3 free pitches when conducting the dynamic strength test.

#### Annex D

(informative)

## Method of determining maximum test force $F_{\text{max}}$ when conducting dynamic strength conformance test

#### D.1 General

The maximum test force  $F_{\text{max}}$  is given by

$$F_{\text{max}} = \frac{F_{\text{d}}F_{\text{u}} + \left[F_{\text{min}}(F_{\text{u}} - F_{\text{d}})\right]}{F_{\text{u}}}$$

where

 $F_{\text{max}}$  is the maximum test force, in newtons (N);

 $F_{\rm d}$  is the minimum dynamic strength as given in <u>Table 1</u> or <u>Table 2</u>, in newtons (N);

 $F_{\rm u}$  is the minimum tensile strength as given in <u>Table 1</u> or <u>Table 2</u>, in newtons (N);

 $F_{\min}$  is the minimum test force, in newtons (N).

#### D.2 Example for Chain 16B

If the chain manufacturer were to choose a minimum test force ( $F_{min}$ ) of 2 700 N (i.e. 4,5 % of the minimum tensile strength according to <u>Table 1</u>). Then, the maximum test force  $F_{max}$  would be determined as follows:

$$F_{\text{max}} = \frac{F_{\text{d}}F_{\text{u}} + \left[F_{\text{min}}(F_{\text{u}} - F_{\text{d}})\right]}{F_{\text{u}}}$$

and from Table 1

$$F_{\rm d}$$
 = 9 530 N,

$$F_{\rm u}$$
 = 60 000 N, and

$$F_{\min} = 2700 \text{ N},$$

then

$$F_{\text{max}} = \frac{(9\ 530 \times 60\ 000) + \left[2\ 700 \times (60\ 000 - 9\ 530)\right]}{60\ 000} = 11\ 800\ \text{N} \ .$$

#### **Annex E**

(informative)

## Examples of methods used to avoid an excessive increase in the rate of stress during the tensile test

#### E.1 Introduction

While the following alternative methods are not universally accepted, they both give an indication as to the rate of loading during the tensile test that could be used to avoid an excessive rate of stress being incurred by the chain.

Please note that as these methods are only intended to be used as a guide and as such do not constitute a mandatory requirement of ISO 606.

#### E.2 Method 1 (Specified in ASME B29.1)

The tensile force is slowly applied at a rate not to exceed 50.8mm/min (2.0 in/min), in a uniaxial direction, to the ends of the chain sample.

#### E.3 Method 2 (Based on and conforming to ISO 6892-1:2009)

#### E.3.1 Procedure

The tensile force is slowly applied at a rate between 2 %  $F_{\rm u \ min}$  / s and 4 %  $F_{\rm u \ min}$  / s, in a uniaxial direction, to the ends of the chain sample.

Using this method the typical length of time during which the chain is subjected to a tensile load would be between 25 s minimum and 50 s maximum.

This method is based on the recommended rate of stress increase as outlined in ISO 6892-1:2009 for conducting a tensile test.

For information, the above rates of testing in Method 2 were established as follows:

According to ISO 6892-1:2009 Para 10.4 Speed of tensile test a recommendation for the rate of stress increase is given in relation to Young's modulus E and is shown in <u>Table E.1</u>.

Table E.1 — Rate of stress increase

Young's modulus E [MPa]	Rate of stress increase ℟ [MPa⋅s <sup>-1</sup> ]
< 150 000	2 - 20
≥ 150 000	6-60

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The inner plate stress for chain 08B-1 would therefore be calculated as follows:

 $b_1 = 7,75 \text{ mm}$  min width between inner plates

 $b_2 = 11,30 \text{ mm}$  max width over inner link

 $d_1 = 8,51 \text{ mm}$  max roller diameter

 $d_2 = 4,45 \text{ mm}$  max pin diameter

 $h_2 = 11,81 \text{ mm}$  max inner plate depth

 $b_i = (b2 - b1) / 2$ , 11 = 1, 68 mm calculated inner plate thickness

 $d_b = d_2 (d_1 / d_2)^{0.475} = 6,05 \text{ mm}$  calculated bush diameter

 $S_{0 IP} = (h_2 - d_b) b_i = 9,68 \text{ mm}^2$  inner plate cross section (one IP)

 $F_u = 17800 \text{ N}$  minimum tensile strength

 $(dF/dt)_{min} = R_{min} \cdot S_{o IP} \cdot 2$  rate of force

 $(dF/dt)_{min} = 6 [MPa / s] \cdot S_{o IP} \cdot 2$ 

 $(dF/dt)_{min} = 6 [N/(s \cdot mm^2)] \cdot 9,68 mm^2 \cdot 2 = 116 N/s$ 

 $(dF/dt)_{max} = \dot{R}_{max} \cdot S_{o IP} \cdot 2$ 

 $(dF/dt)_{max} = 60 [MPa / s] \cdot S_{o IP} \cdot 2$ 

 $(dF/dt)_{max} = 60 [N /(s \cdot mm^2)] \cdot 9,68 mm^2 \cdot 2 = 1,162 N / s$ 

#### E.3.2 Calculation of time

The calculation of time for the tensile test would be as follows:

 $T_{min} = F_u / (dF/dt)_{max}$  min time

 $T_{min} = 17800 \text{ N} / 1162 \text{ N} / \text{s}$ 

 $T_{min} = 15, 3 s$ 

 $T_{max} = F_u / (dF/dt)_{min}$  max time

 $T_{max} = 17800 N / 116 N / s$ 

 $T_{max} = 153 \text{ s}$ 

Now method 2 states: Speed of tensile test to be between 2 % F<sub>u min</sub> / s and 4 % F<sub>u min</sub> / s, which would be:

 $T_{max} = 17800 \text{ N} / 356 \text{ N} / \text{s} = 50 \text{ s}$ 

 $T_{min} = 17800 \text{ N} / 712 \text{ N} / \text{s} = 25 \text{ s}$ 

Both  $T_{min}$  and  $T_{max}$  are within the ISO 6892-1 specification requirements of 15,3 s and 153 s.

#### E.3.3 Procedure using older tensile test equipment

For older tensile test equipment when only certain fixtures speed  $v_c$  [mm / min] can be set, the following procedure should be followed.

The fixture speed or the crosshead separation rate  $v_c$  [mm / min] is set such that the total testing time falls between  $T_{min} = 25$  and  $T_{max} = 50$  s.

A recommended starting point for the crosshead separation rate is

$$v_c = 10 [mm / min]$$

A testing time over 50 s is not critical and provides valid breaking load test results. If the total testing time is below 20 s ( $T_{min}$  - 20 %) the measured breaking load is not valid and the test shall be repeated with a reduced crosshead separation rate.

#### Annex F

(informative)

## Methods used to approximate the minimum dynamic test values for multiplex chains

Currently there is insufficient test data available to give an exact relationship between dynamic values of simplex chains to that of multiplex chains and as such there is no universally agreed method for calculating this relationship. If approximate minimum dynamic strength values are required for the duplex and triplex chains then the methods described in <u>F.1</u> and <u>F.2</u> could be considered:

#### F.1 Method 1 (German origin)

Min. dynamic strength of duplex chain =  $1,50 \times \text{value}$  of corresponding simplex chain.

Min. dynamic strength of triplex chain =  $1.92 \times \text{value}$  of corresponding simplex chain.

Except for the chains shown in Table F.1.

Duplex/simplex Triplex/simplex Chain 06B 1,31 1,57 08B 1,33 1,62 10B 1,48 1,87 16B 1,47 1,90 20B 1.48 1.90

Table F.1 — Factors for multiplex chains

#### F.2 Method 2 (US origin)

For all chain pitches, the multiplex chain would be expected to have a chain strand factor of 0,67, which would then give:

- min. dynamic strength of duplex chain = 1,34 × value of corresponding simplex chain;
- min. dynamic strength of triplex chain = 2,01 × value of corresponding simplex chain.

The 0,67 strand factor requires that loose-fit intermediate plates have at least 80 % of the dynamic strength of the press-fit outer plates.

NOTE Before applying any chain loadings, which are obtained from the use of either of the above two alternative methods, obtain the advice of the chain manufacturer.

### **Bibliography**

- [1] ISO 9633:2001, Cycle chains Characteristics and test methods
- [2] ISO 10190:2008, Motorcycle chains Characteristics and test methods
- [3] ISO 10823:2004, Guidelines for the selection of roller chain drives
- $[4] \hspace{0.5cm} \textbf{ISO 6892-1:2009, } \textit{Metallic materials} \textit{Tensile testing} \textit{Part 1: Method of test at room temperature}$
- [5] ISO 13203:2005, Chains, sprockets and accessories List of equivalent terms

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