



BSI Standards Publication

**Thermal spraying —  
Measurement of the electrical  
conductivity of thermal  
sprayed non-iron metal  
coatings by means of eddy  
current method**

**National foreword**

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English Version

## Thermal spraying - Measurement of the electrical conductivity of thermal sprayed non-iron metal coatings by means of eddy current method

Projection thermique - Mesurage de la conductivité électrique des revêtements métalliques non ferreux obtenus par projection thermique, à l'aide de la méthode par courants de Foucault

Thermisches Spritzen - Messung der elektrischen Leitfähigkeit thermisch gespritzter Nichteisenmetallschichten mittels Wirbelstromverfahren

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<b>Contents</b>		Page
<b>European foreword</b> .....		3
<b>Introduction</b> .....		4
<b>1</b>	<b>Scope</b> .....	5
<b>2</b>	<b>Normative references</b> .....	5
<b>3</b>	<b>Terms and definitions</b> .....	5
<b>4</b>	<b>Measuring process</b> .....	6
<b>4.1</b>	<b>Measuring method</b> .....	6
<b>4.2</b>	<b>Calibration standard</b> .....	7
<b>4.3</b>	<b>Measuring frequency and penetration depth</b> .....	8
<b>4.4</b>	<b>Measuring instruments</b> .....	8
<b>4.5</b>	<b>Factors, which have effects on the uncertainty of the measurement</b> .....	9
<b>4.6</b>	<b>Limit of application</b> .....	9
<b>5</b>	<b>Procedure of the measurement</b> .....	10
<b>5.1</b>	<b>Calibration of the measuring instruments</b> .....	10
<b>5.2</b>	<b>Measurement</b> .....	10
<b>6</b>	<b>Measuring results and their assessment</b> .....	10
<b>7</b>	<b>Test report and documentation</b> .....	11
<b>Annex A (informative) Record for the applied Electrical Conductivity Measurement</b> .....		12
<b>A.1</b>	<b>General</b> .....	12
<b>A.2</b>	<b>Component/part</b> .....	12
<b>A.3</b>	<b>Surface preparation for spraying</b> .....	12
<b>A.4</b>	<b>Spraying procedure for component/part</b> .....	12
<b>A.5</b>	<b>Preparation of measurement</b> .....	13
<b>A.6</b>	<b>Measuring instrument</b> .....	13
<b>A.7</b>	<b>Result of the measured electrical conductivity</b> .....	13
<b>Bibliography</b> .....		14

## European foreword

This document (EN 16813:2016) has been prepared by Technical Committee CEN/TC 240 “Thermal spraying and thermally sprayed coatings”, the secretariat of which is held by DIN.

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## Introduction

In many applications, the electrical conductivity is a relevant technical parameter. For testing of imperfections in components or technological material properties the eddy current method can be very well applied. It can be detected or determined, for example:

- defects in welds;
- imperfections or change in the structure of a component, for example, due to aging processes in structures made out of aluminium;
- change in structure caused by temperature effects;
- thickness;
- physical material properties such as the electrical conductivity.

Due to an interaction between high frequency magnetic fields, emitted from a measuring probe, and the eddy currents induced in the object to be measured the electrical conductivity can be determined, e.g. according to ASTM E 1004 or can be used for fast and contact less measurements of a coating thickness according to EN ISO 21968.

Due to the manufacturing process thermal sprayed coatings contain a layer orientated structure. Dependent on the material used, it can also contain oxides and/or inclusions as well as porosity created due to splat boundary effects during spraying.

Besides the structure with its grain boundaries, dislocations, internal stresses and impurities, e.g. oxide skins, the specific gravity of a material plays an important role for the level of the electrical conductivity. In order to produce the highest possible level of electrical conductivity in the coating, the influencing factors for the thermal spraying process should be minimized.

## 1 Scope

This European standard specifies the procedure of the measurement of the electrical conductivity of non-Ferro-magnetic thermal sprayed coatings. By this measurement the absolute value of the electrical conductivity in the coating sprayed on component can be determined as well as also deviations from the agreed rated value can be used to control a running production. With that, a remarkable contribution can be applied to process and quality assurance measures of a manufacture process.

## 2 Normative references

The following documents, in whole or in part, are normatively referenced in this document and are indispensable for its application. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

EN ISO 21968, *Non-magnetic metallic coatings on metallic and non-metallic basis materials - Measurement of coating thickness - Phase-sensitive eddy-current method (ISO 21968)*

## 3 Terms and definitions

For the purposes of this document, the following terms and definitions apply.

### 3.1

#### electrical conductivity

$\sigma$

physical value, which shows the ability of a material – in this case of a thermal sprayed coating – to conduct the current

Note 1 to entry: It is defined to be the constant of proportionality between the current density and the electrical field intensity within the general Formula (1) of the ohmic law.  $\sigma$  is measured in S/m.

$$J = \sigma \times E \tag{1}$$

where

$J$  is the current density;

$\sigma$  is the electrical conductivity;

$E$  is the field intensity.

### 3.2

#### electrical resistance

$R$

value, which defines the electrical voltage, which is needed that a certain current can flow through an electrical conductor

Note 1 to entry: The unit is ohm ( $\Omega$ ).

### 3.3 specific electrical resistivity

property of material, which is the result of the electrical resistance in a homogenous part with a constant current intensity distribution across the constant cross-section and length of the conductor and an ohmic resistance

Note 1 to entry: The specific electrical resistance, see Formula (2), depends on the temperature of material and is the reciprocal value of the electrical conductivity ( $\rho = 1/\sigma$ ). The unit is ohm metre ( $\Omega \times \text{m}$ ).

$$\rho = R \times \frac{A}{L} \quad (2)$$

where

- $\rho$  is the specific electrical resistivity in  $\Omega \times \text{m}$ ;
- $R$  is the ohmic resistance;
- $A$  is the constant cross-section of the conductor;
- $L$  is the length of the conductor.

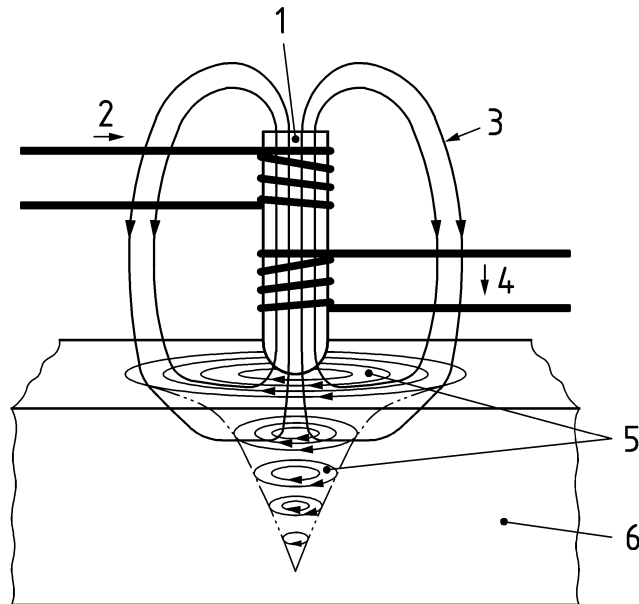
## 4 Measuring process

### 4.1 Measuring method

Measuring of the absolute value of the electrical conductivity takes place usually by a current voltage measurement. However, this method is usually applied in laboratories only.

If the electrical conductivity shall be determined in a component on site, primarily eddy current processes are applied. To measure the electrical conductivity of non-magnetic metals, such as aluminium, copper, brass, titanium, chrome-nickel-steel, etc. Therefore, the phase-sensitive eddy current measurement procedure is very suitable. By that, the measuring probe fed from a generator with alternating current of a certain frequency is to be put to the object to be measured or to be brought into small distance to its surface. This exciter current generates a magnetic field of high frequency, which induces eddy currents in the material to be tested (in this case the coating respectively the base material), their intensity and penetration depth depend on its electrical conductivity. On the other hand the magnetic field induced by eddy currents overlaps the generating field. The generated resulting magnetic field is detected by a measuring coil. By that, the induced voltage is a function of the electrical conductivity of the object to be measured and can be used as a signal for its measuring. See Figure 1.





**Key**

- |   |   |
|---|---|
| 1 ferrite core of the probe                 | 4 measuring signal                          |
| 2 exciting current                          | 5 eddy current induced                      |
| 3 high frequency magnetic alternating field | 6 electrically conductive non-ferrous-alloy |

**Figure 1 — Phase-sensitive eddy current measuring method**

Using the phase-sensitive eddy current measurement procedure the phase changing between exciter current and measuring signal is to be transferred into a conductivity value. This measuring value is independent from the distance between the probe and the coating surface for a certain arrangement, which depends on the type of the probe. By that, a non-contactable determination of the conductivity can be applied also using this method, for example, below a varnish or a synthetic material coat. Using an adequate measuring frequency the influence of the surface roughness remains low.

**4.2 Calibration standard**

Using the phase-sensitive eddy current measurement procedure the measuring value found in the component will be compared to the calibration standard as a reference standard, which conductivity is very well known. Standards for calibration of the measuring instrument are available for the whole conductivity range. Usually, they are also supplied from the measuring instrument producer.

Because the calibration standards are subject to changes in properties due to use they have to be recalibrated at regular time periods or to be replaced.

### 4.3 Measuring frequency and penetration depth

The penetration depth of the eddy current is defined by the conductivity  $\sigma$  and the measuring frequency  $f$ . Generally, the penetration depth  $\sigma_0$  of the eddy current in a non-ferrous-alloy is given by:

$$\sigma_0 = \frac{503}{\sqrt{f \times \sigma \times \mu_R}} \quad (3)$$

where

- $\sigma_0$  is the penetration depth of the eddy current in a non-ferrous-alloy;
- $f$  is the measuring frequency in Hz;
- $\sigma$  is the electrical conductivity in MS/m;
- $\mu_R$  is the permeability = 1 for non-magnetic materials.

The penetration depth of the eddy current is also decisive for the minimally permissible thickness of the object to be measured. In order to achieve complete saturation within the coating to be measured a penetration depth  $\sigma_S$  shall be taken:

$$\sigma_S = 2,5 - 3\sigma_0 \quad (4)$$

where

- $\sigma_S$  is the penetration depth of the eddy current in the coating;
- $\sigma_0$  is the penetration depth of the eddy current in a non-ferrous-alloyl.

Due to the usually low thickness of thermal sprayed coatings, a higher measuring frequency shall be taken, therefore. Usually, such measuring frequencies are in the range of 480 kHz to more than 1 MHz. They are available in commercial instruments.

Due to the increase of the skin effect with increasing frequency, however, the measuring frequency should not be selected unnecessary high, because the measuring result could not be representative for the coating then.

In the case of increasing measuring frequency the negative influence of surface roughness to the measuring result also increases. The higher the frequency the smoother should be the surface. Using the phase-sensitive eddy current measurement procedure the effect remains low.

### 4.4 Measuring instruments

Nowadays, instruments to measure the electrical conductivity are equipped as to be:

- independent instrument for control measurement in the laboratory;
- integrated instrument with an automatic measurement in installations for manufacture;
- hand-operated instrument for measurements in the work shop.

Usually, the attachment contains:

- collection of measuring data and connections to PC, printer and to have the capability of data storing;
- measuring range: e.g. 0,5 MS/m to 65 MS/m respectively 1 % to 112 % IACS (International Annealed Copper Standard).

Often a disturbing effect of distance variations can be suppressed when using a scanning probe. Therefore, measuring tasks can be served successfully, where a direct contact to the metallic surface is not possible or undesirable, such as for varnishes or moved measuring objects.

#### **4.5 Factors, which have effects on the uncertainty of the measurement**

Following influencing factors can lead to deviations of the measuring result:

- distance from the probe to the component surface, also called take-off effect, is too large or not sufficiently compensated or dirt particles are in between;
- distance from the probe to an edge is too small or not sufficiently compensated (necessary distance can be found experimentally or according to EN ISO 21968);
- curvature of the surface, e.g. if the curvature is too low related to the diameter of the probe;
- thickness of the measuring object (coating), when saturation thickness (see 4.3) cannot be kept);
- different measuring temperatures, usually temperature compensation is done by an internal or external temperature sensor with relation to the conductivity at +20 °C;
- surface roughness of the object to be measured. Rough surfaces can cause systematic as well as random errors. A reduction of defects by chance can be achieved using a greater number of measurements at different points. However, the roughness plays only a role using higher measuring frequencies;
- inhomogeneity of the measuring object within the recorded area, e.g. by accumulation of pores, voids, oxides, or by changing of the structure or the chemical composition within the coating.

Using a sufficient calibration of the measuring instrument the effects of distance of the probe to the surface, distance to edges, curvature and temperature effects can be eliminated to the greatest possible extent.

When manipulation and calibration of the measuring instrument is well done a measuring uncertainty of less than 5 % can be achieved.

#### **4.6 Limit of application**

A limit of application is given for the measuring method to measure the absolute value of the electrical conductivity of the coating, when:

- above mentioned factors of influence cannot be compensated by calibration of the measuring instrument or other measures;
- the coating thickness is too small, the necessary saturation depth cannot be achieved, so that the eddy currents penetrate the substrate material.

Limits of application of the measuring method can be given to serve for the manufacturing assurance of the spraying process, when:

- the difference in conductivity between the coating and the base metal is too less and the eddy currents penetrate the substrate material;
- a more and different mixing took place between the conductive coating and non-conductive substrate material at the interface and this zone will be reached by the eddy currents;
- the coating thickness is such small, that the portion for measurement of the substrate material extremely prevails despite highest measuring frequency.

The limits of the application are reached when the measurements of the base material and the coating are equal.

## **5 Procedure of the measurement**

### **5.1 Calibration of the measuring instruments**

Before use the measuring instrument shall be calibrated according to the instructions of the producer using two standards with different conductivity, where the surrounding air is used as one of the standards, normally. At the moment of the calibration the measuring instrument and calibration standard shall possess nearly the temperature of the objects to be measured. The calibration should be checked after a greater number or duration time of measurements according to the instructions of the producer.

The electrical conductivity of the coating shall be between the conductivity values of the two calibration standards.

If the curvature of the coated surface to be measured does not allow calibration on a flat surface, the standards used for the calibration shall contain the same curvature radius, such as the part to be inspected or a specific testing apparatus shall be applied, which compensates the influence of the curvature.

### **5.2 Measurement**

The measuring instruments are to be calibrated and to be used according to the instructions of the producer.

Prior to the execution of the measurements any foreign substances (dirt, oil, grease, corrosive products, etc.) are to be removed from the surface of the calibration standard and the objects to be measured.

It shall be checked, that the measuring frequency and thus the penetration depth of the eddy current is in the scale of the coating thickness. This fact is important for the measurement of the absolute values.

To avoid faulty measuring the necessary distance from the probe to edges shall be kept and in the case of narrow curvatures of the component a probe with a smaller diameter or with adequate geometry is to be used after adequate calibration.

## **6 Measuring results and their assessment**

The necessary number of measurements is given by the type of task. The number of measurement points should be chosen so that a mean value can be calculated from an area representative for a part.

Multiple measurements at different points are required, if the electrical conductivity and its homogeneity in the coating are investigated.

When validating the reproducibility of a manufacturing process, the average of a number of readings is required in order to exclude non-homogenous coating variability on any one sample measured.

When such measurements are required from the customer number and position of the measuring points at the component should be agreed upon between the parties involved in this transaction.

## **7 Test report and documentation**

The test report shall contain following items:

- a) type of task, aim of the measurement;
- b) any instructions for identifying the test specimen or of the part to be tested;
- c) reference to this test standard;
- d) frequency, as in A.6;
- e) size of the surfaces to be tested on each part, e.g. in mm<sup>2</sup>;
- f) position of the measuring points on every part;
- g) number of the measured test specimens/parts;
- h) designation of the test instrument, the measuring probe, the used calibration standard;
- i) results of the measurements, details of the conductivity values measured as single and mean values respectively differences to the rated value in the case of measurements for comparison;
- j) name of the inspector;
- k) deviations from the procedure observed and features during testing, which are expected to may have influence to the results and their validity;
- l) date of testing.



Chemical composition (main elements):.....  
 Preheating: yes / no Preheating temp.:.....°C      Cooling: yes / no Medium:.....  
 Spraying distance:.....mm Surface speed .....m/min (relative speed between spray torch and part)  
 Auxiliary spray device, if applicable, No.:.....  
 Coating thickness: as sprayed:..... Roughness as sprayed:  $R_z$ .....  
 Post treatment: grinding/polishing      Final roughness:  $R_a/R_z$  [ $\mu\text{m}$ ].....  
 Number of specimens sprayed, if applicable:.....  
 Thermal sprayer/operator:.....

### A.5 Preparation of measurement

Measuring instrument calibrated: yes /no  
 Date of calibration: .....

### A.6 Measuring instrument

Measuring instrument:      Type:..... Designation No.: .....

Independent instrument      yes /no  
 Integrated instrument      yes /no  
 Hand-operated instrument      yes /no  
 Measuring frequency:.....Hz  
 Condition: Ambient temperature:..... °C; Humidity:..... %

### A.7 Result of the measured electrical conductivity

Measuring frequency:											
	Rated value	Location for measurement							Mean value	Results	
Location No.	—	1	2	3	4	5	6	7		Passed	Failed
Measured value in MS/m											
Measured value in % IACS											

Date of issue:.....

Verifying:

For inspection body: Name:..... Signature:.....

For manufacturer: Name:..... Signature:.....

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