Incorporating corrigendum July 2009

# Cylindrical helical springs made of round wire — Quality specifications for cold coiled compression springs

ICS 21.160



# National foreword

This British Standard is the UK implementation of EN 15800:2008. It partially supersedes BS 1726-1:2002, which is being revised to remove conflicting material. In the meantime, where conflict exists between the two standards the provisions of BS EN 15800:2008 take precedence.

The UK participation in its preparation was entrusted by Technical Committee FME/9, Fasteners, to subcommittee FME/9/3, Product standards for fasteners.

A list of organizations represented on this subcommittee can be obtained on request to its secretary.

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31 July 2009	Addition of supersession details, and correction to committee details, in National foreword

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# EUROPEAN STANDARD NORME EUROPÉENNE EUROPÄISCHE NORM

**EN 15800** 

December 2008

ICS 21.160

#### **English Version**

# Cylindrical helical springs made of round wire - Quality specifications for cold coiled compression springs

Ressorts cylindriques hélicoïdaux en fils ronds -Prescriptions de qualité des ressorts de compression façonnés à froid Zylindrische Schraubenfedern aus runden Drähten -Gütevorschriften für kaltgeformte Druckfedern

This European Standard was approved by CEN on 18 October 2008.

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#### **Foreword**

This document (EN 15800:2008) has been prepared by Technical Committee CEN/TC 378 "Project Committee – Springs", the secretariat of which is held by DIN.

This European Standard shall be given the status of a national standard, either by publication of an identical text or by endorsement, at the latest by June 2009, and conflicting national standards shall be withdrawn at the latest by June 2009.

This European Standard has been prepared by the initiative of the Association of the European Spring Federation ESF and is based on the German Standard DIN 2095 "Helical springs made of round wire — Specification for cold coiled compression springs", which is known and used in many European countries.

Attention is drawn to the possibility that some of the elements of this document may be the subject of patent rights. CEN [and/or CENELEC] shall not be held responsible for identifying any or all such patent rights.

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#### 1 Scope

This European Standard applies to cylindrical helical compression springs made of round spring wire. Cold coiled compression springs can be made with wire up to about 16 mm diameter. (See also EN 13906-1).

Cylindrical helical springs made of round wire from European Standard materials are subject to the limiting values in Table 1:

Table 1

Characteristic	Cold coiled compression springs
Wire diameter	0,07 mm ≤ <i>d</i> ≤ 16 mm
Mean coil diameter	0,63 mm ≤ <i>D</i> ≤ 200 mm
Length of unloaded spring	<i>L</i> <sub>o</sub> ≤ 630 mm
Number of active coils	n ≥ 2
Spring index	4 ≤ <i>w</i> ≤ 20

A specification for the parameters of cold formed helical compression springs is given in Annex B.

#### 2 Normative references

The following referenced documents are indispensable for the application of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

EN 10270-1, Steel wire for mechanical springs — Part 1: Patented cold drawn unalloyed spring steel wire

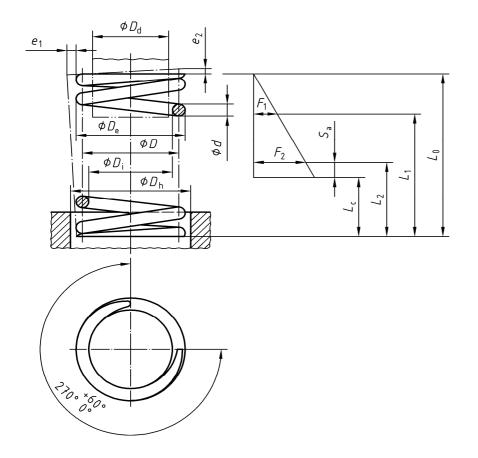
EN 10270-2, Steel wire for mechanical springs — Part 2: Oil hardened and tempered spring steel wire

EN 10270-3, Steel wire for mechanical springs — Part 3: Stainless spring steel wire

EN 12166, Copper and copper alloys — Wire for general purposes

# 3 Representation

Dimensions in millimetres



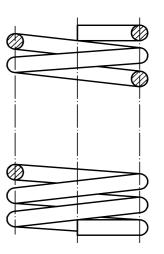


Figure 1 — Type 1 Spring ends closed and ground (with theoretical characteristic)

Figure 2 — Type 2 Spring ends closed

# 4 Definitions, symbols, units and terms

Table 2

Symbols	Units	Terms
$a_{ m F}$	N	Value for determining variations of spring force and spring length (effect of geometry and dimensions)
$A_{ m D}$	mm	Permissible variation of coil diameter $(D_e, D_i, D)$ of unloaded spring
$A_{ m F}$	N	Permissible variation of spring force $F$ at given spring length $L$
$A_{ m L0}$	mm	Permissible variation of length $L_0$ of unloaded spring
d	mm	Nominal diameter of wire (or bar)
$d_{\sf max}$	mm	Upper deviation of d
$D_{\mathrm{e}}$	mm	Outside diameter of spring
$D_{d}$	mm	Mandrel diameter (inner guide)
$D_{ m h}$	mm	Sleeve diameter (outer guide)
$D_{\mathrm{i}}$	mm	Inside diameter of spring
$D = \frac{D_{\rm e} + D_{\rm i}}{2}$	mm	Mean diameter of spring
e <sub>1</sub>	mm	Permissible variation of squareness of the unloaded ground spring
$e_2$	mm	Permissible variation in parallelism of the ground spring bearing surfaces, measured for $D_{\rm e}$
F	N	Spring force
$F_{1,}F_{2}$	N	Spring forces for the spring lengths $L_1$ , $L_2$ (at ambient temperature of 20 °C)
$F_{ m c\ th}$	N	Theoretical spring force at solid length $L_{\rm c}$ NOTE — The actual spring force at the solid length is as a rule greater than the theoretical force.
$k_{ m f}$	_	Factor for determining variations of spring force and spring length (effect of active coils)
L	mm	Spring length
$L_0$	mm	Nominal free length of spring
$L_1$	mm	Length at smallest test load $F_1$
$L_1, L_2$	mm	Spring lengths for the spring forces $F_1$ , $F_2$
$L_{\mathrm{c}}$	mm	Solid length
$L_{n}$	mm	Minimum permissible spring length (depending upon S <sub>a</sub> )
n	_	Number of active coils
$n_{\rm t}$	_	Total number of coils
Q		Coefficient of quality grade
$R = \frac{\Delta F}{\Delta s}$	N/mm	Spring rate
s <sub>1</sub> , s <sub>2</sub>	mm	Spring deflections, for the spring forces $F_1$ , $F_2$
$S_{\mathbf{c}}$	mm	Spring deflection for the solid length $L_{ m c}$
S <sub>h</sub>	mm	Deflection of spring (stroke) between two positions
$S_{\mathrm{a}}$	mm	Sum of minimum gaps between adjacent active coils at spring length L <sub>n</sub>
$w = \frac{D}{d}$	_	Spring index
$\lambda = \frac{L_0}{d}$		Slenderness ratio

#### 5 Requirements

#### 5.1 Coiling direction

Compression springs are generally made with right-hand coiling, or with alternating right-hand and left-hand coiling for nested spring assemblies; in this case the outer spring is usually right-hand coiled. If left-hand coiling for springs is required, this shall be obvious from the note "left-hand coiled" which shall appear in drawings or enquiries and order documents. See Annex B.

#### 5.2 Spring ends

The spring ends whereby the spring force is transmitted to the connecting components shall be designed so that the deflection of the spring is as nearly axial as possible in every position of the spring. This is generally achieved by reducing the pitch of one finishing coil at each end. To obtain adequate bearing surfaces perpendicular to the spring axis, the wire ends are ground in accordance with Figure 1.

If grinding of the spring ends is found to be inexpedient, the spring should be made according to Figure 2, that means without ground wire ends. In all cases the type of finish for the spring ends shall be stated in one of the contractual documents: descriptive, drawings or enquiries and order documents. See Annex B.

If unground spring ends are acceptable for the particular use concerned, e.g. when the compression springs are made of wire having a diameter less than approximately 1 mm or with a spring index over 15, grinding of the wire ends should be omitted for economic reasons. See Annex B.

When the compression springs are made of wire having a diameter under 0,3 mm the wire ends should not be ground.

With regard to the simultaneous grinding of the spring ends of compression springs having a wire diameter from 0,3 mm up to about 5 mm it should be noted that only springs which allow adequate contact pressure can be ground flat.

Tests so far carried out indicate that this contact pressure shall amount to approximately

$$\frac{R}{D} \ge 0.03 \text{ N/mm}^2 \tag{1}$$

The spring ends should only be deburred if this is required for proper functioning, and shall be agreed between the spring manufacturer and the customer. This information shall be included in enquiries, drawings, and orders. See Annex B.

#### 5.3 Solid length $L_{\rm c}$

(all coils are closed)

For springs with ground ends according to Figure 1, the solid length is:

$$L_{\rm c} \le n_{\rm t} \cdot d_{\rm max} \tag{2}$$

For springs without ground ends according to Figure 2, the following applies:

$$L_c \le (n_t + 1.5) \cdot d_{\text{max}}$$
 (3)

where

$$n_{\rm t} = n + 2$$

2 = Number of non-active coils

Springs have  $n \ge 2$  coils

#### 5.4 Material

The material selection shall be done in line with loading and function of the spring.

The materials covered by this standard are:

- a) Patented cold drawn unalloyed spring steel wire to EN 10270-1.
- b) Oil hardened and tempered spring steel wire to EN 10270-2.
- Stainless spring steel wire to EN 10270-3.
- d) Wire from copper and copper alloys to EN 12166.

#### 5.5 Surface Treatment

#### 5.5.1 Shot-peening

Springs may be shot peened, if agreed between manufacturer and customer.

#### 5.5.2 Surface protection

Either organic or inorganic coatings may be applied, if agreed between manufacturer and customer.

#### 6 Quality grades

#### 6.1 Permissible variations of Quality Grades

For springs the quality grades 1, 2 and 3 are specified (for coefficients Q see Table 4).

All the permissible variations listed below apply only to material given in EN 10270. For materials in EN 12166, permissible variations shall be agreed between manufacturer and customer.

The choice between quality grades 1, 2 and 3 is governed by operational requirements. The quality grade required and the permissible variations shall be expressly agreed or stated in the drawing.

In the absence of information, quality grade 2 shall apply.

In the interests of rationalized production quality grade 1 should be specified only when the particular use calls for it. For this purpose not all the quantities in Subclauses 6.2 to 6.6 necessarily belong to a **single** quality grade. If variations smaller then "1" are required, agreements shall be made between manufacturer and customer.

#### 6.2 Permissible variations of wire diameters d

The permissible variations for wire diameter d are specified in the corresponding material standards see 5.4.

#### 6.3 Permissible variations $A_{\rm D}$ for coil diameter D of unloaded spring

For mean coil diameters D up to 200 mm, see Table 3.

In drawings and in enquiries and order documents the inner diameter  $D_{\rm i}$ , or the external diameter  $D_{\rm e}$  and the mean coil diameter D shall be stated.

The permissible variations specified for the mean coil diameter D apply to both the corresponding inner diameter  $D_{\rm e}$  and the external diameter  $D_{\rm e}$ .

In the case of springs working in a sleeve or on a mandrel, it is recommended that the smallest sleeve diameter or largest mandrel diameter also shall be stated.

Table 3

		Permissible variations $A_{ m D}$								
1	D		mm							
m	m		ality grad spring ind			ality grad spring ind			ality grad spring ind	
above	to	4 to 8	above <b>8</b> to <b>14</b>	above 14 to 20	4 to 8	above 8 to 14	above 14 to 20	4 to 8	Above <b>8</b> to <b>14</b>	above 14 to 20
0,63	1	± 0,05	± 0,07	± 0,1	± 0,07	± 0,1	± 0,15	± 0,1	± 0,15	± 0,2
1	1,6	± 0,05	± 0,07	± 0,1	± 0,08	± 0,1	± 0,15	± 0,15	± 0,2	± 0,3
1,6	2,5	± 0,07	± 0,1	± 0,15	± 0,1	± 0,15	± 0,2	± 0,2	± 0,3	± 0,4
2,5	4	± 0,1	± 0,1	± 0,15	± 0,15	± 0,2	± 0,25	± 0,3	± 0,4	± 0,5
4	6,3	± 0,1	± 0,15	± 0,2	± 0,2	± 0,25	± 0,3	± 0,4	± 0,5	± 0,6
6,3	10	± 0,15	± 0,15	± 0,2	± 0,25	± 0,3	± 0,35	± 0,5	± 0,6	± 0,7
10	16	± 0,15	± 0,2	± 0,25	± 0,3	± 0,35	± 0,4	± 0,6	± 0,7	± 0,8
16	25	± 0,2	± 0,25	± 0,3	± 0,35	± 0,45	± 0,5	± 0,7	± 0,9	± 1,0
25	31,5	± 0,25	± 0,3	± 0,35	± 0,4	± 0,5	± 0,6	± 0,8	± 1,0	± 1,2
31,5	40	± 0,25	± 0,3	± 0,35	± 0,5	± 0,6	± 0,7	± 1,0	± 1,2	± 1,5
40	50	± 0,3	± 0,4	± 0,5	± 0,6	± 0,8	± 0,9	± 1,2	± 1,5	± 1,8
50	63	± 0,4	± 0,5	± 0,6	± 0,8	± 1,0	± 1,1	± 1,5	± 2,0	± 2,3
63	80	± 0,5	± 0,7	± 0,8	± 1,0	± 1,2	± 1,4	± 1,8	± 2,4	± 2,8
80	100	± 0,6	± 0,8	± 0,9	± 1,2	± 1,5	± 1,7	± 2,3	± 3,0	± 3,5
100	125	± 0,7	± 1,0	± 1,1	± 1,4	± 1,9	± 2,2	± 2,8	± 3,7	± 4,4
125	160	± 0,9	± 1,2	± 1,4	± 1,8	± 2,3	± 2,7	± 3,5	± 4,6	± 5,4
160	200	± 1,2	± 1,5	± 1,7	± 2,1	± 2,9	± 3,3	± 4,2	± 5,7	± 6,6

#### 6.4 Permissible variations $A_{\rm F}$ for spring force F at given spring length L

The permissible variation for spring force is

$$A_{\rm F} = \pm \left( \mathbf{a}_{\rm F} \cdot k_{\rm f} + \frac{1,5 \, F}{100} \right) \cdot Q \tag{4}$$

The value  $a_F$  can be found from Figures 3 and 4 or can be calculated by the respective equation in Annex A.

The factor  $k_f$  is obtainable from Figure 5 and the coefficient Q from Table 4 or can be calculated by the respective equation in Annex A.

The  $a_F$  quantities specified in Figures 3 and 4 for springs according to Figure 1 apply only to springs which are resistant to buckling (see also EN 13906-1).

#### 6.5 Permissible variations $A_{\rm L0}$ for length $L_0$ of unloaded spring

The length of the unloaded spring shall be up to 630 mm.

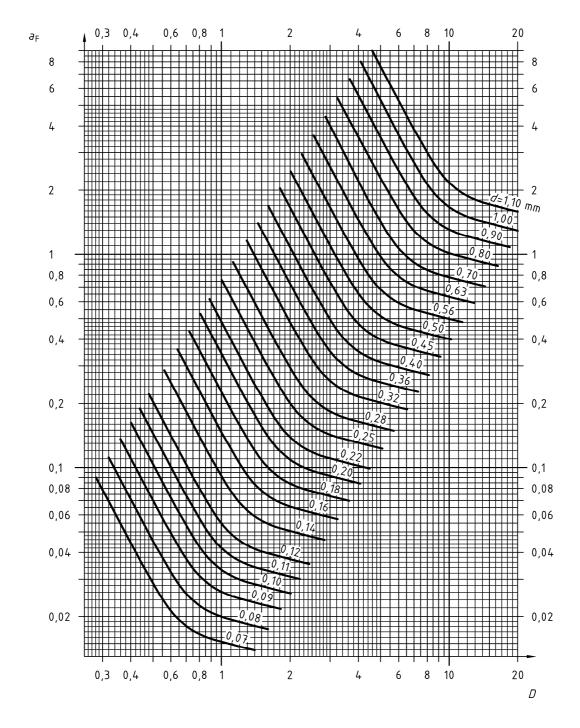
 $L_{o}$  is only toleranced in accordance with the requirements of 6.7.

The permissible variation is

$$A_{L0} = \pm \frac{\mathbf{a}_{F} \cdot k_{f} \cdot Q}{R} \tag{5}$$

Table 4

Quality grade	Q
1	0,63
2	1,00
3	1,60



 $a_F$  in N D in mm

Figure 3 — Value  $a_{\rm F}$ ; influence of geometry and dimensions on variations of spring force and spring length for wire diameters from 0,07 mm to 1,1 mm

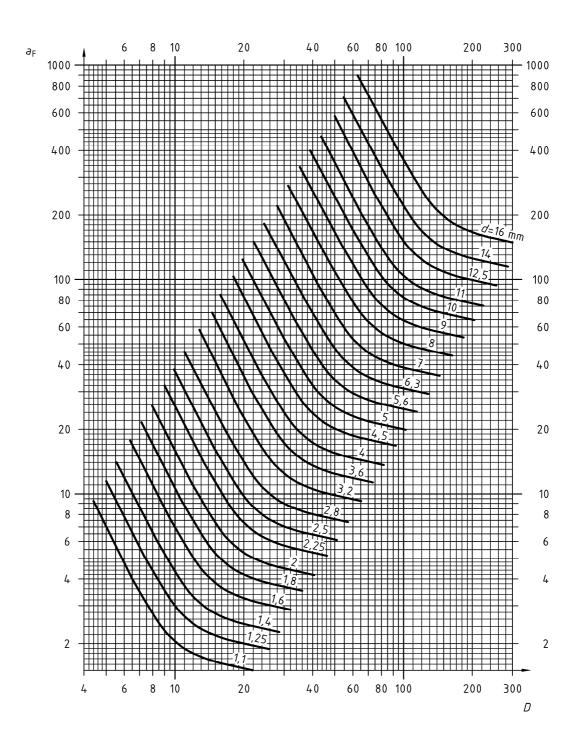


Figure 4 — Value  $a_{\rm F}$ ; influence of geometry and dimensions on variations of spring force and spring length for wire diameters from 1,1 mm to 16 mm

in N

in mm

 $\boldsymbol{a}_{\mathrm{F}}$ 

D

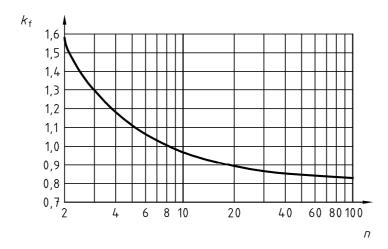


Figure 5 — Factor  $k_{\rm f}$ ; influence of active coils on variations of spring force and spring length

#### 6.6 Permissible variations $e_1$ and $e_2$ of unloaded springs with ends closed and ground

Table 5

Quality grade	1	2	3
Variation $e_1$ of squareness from the vertical	0,03 L <sub>0</sub>	0,05 <i>L</i> <sub>0</sub>	0,08 L <sub>0</sub>
Variation $e_2$ from parallelism	0,015 <i>D</i> <sub>e</sub>	0,03 <i>D</i> <sub>e</sub>	0,06 <i>D</i> <sub>e</sub>

Values should only be specified for  $e_1$  and  $e_2$  (see Figure 1), if vital for the functioning of the spring.

Quality grade 1 can only be achieved with springs having a spring index  $w \le 12$  and a slenderness ratio  $\lambda \le 5$ .

#### 6.7 Production margin

The spring manufacturer needs a production margin in order to meet the permitted tolerances specified, see Table 6.

Table 6

Quantities specified	Production margin provided by:
One spring force and the corresponding length of the loaded spring	$L_0$
One spring force and the corresponding length of the loaded spring and the length of the unloaded spring ${\cal L}_0$	$n$ and $d$ or $n$ and $D_{ m e},D_{ m i}$
Two spring forces and the corresponding lengths of the loaded spring	$L_0$ , $n$ and $d$ or $L_0$ , $n$ and $D_{ m e}$ , $D_{ m i}$

The numerical values of the items thus available as a production margin shall be stated in the drawings, enquiries and order documents and count only as reference values.

In the event of a production margin being utilized, care must be taken to ensure that the permissible shear stress is not exceeded (see EN 13906-1).

#### 7 Testing

#### 7.1 Static load testing

The testing is carried out on the spring in the upright position in the direction of loading. For this propose the given spring length L shall be attained in the increasing force direction only, and the corresponding force F read off. The maximum design force shall not be exceeded during the load testing. Permissible variation in the spring load indication shall be  $\pm$  1 %.

In the case of preset springs it is essential in all cases that prior to static testing they shall be compressed to the solid length or to an agreed spring length; in the case of nonpreset springs compression to the minimum length occurring in service or during installation is performed. This length shall be stated.

Springs which are not resistant to buckling (see EN 13906-1) shall be tested on a mandrel or in a sleeve, the diameters of the mandrel or sleeve and the test method being agreed.

#### 7.2 Characteristic

The characteristic (force-deflection curve) calculated according to EN 13906-1 is a straight line for the helical compression spring. In practice, the characteristic is not linear at the start and finish. If it is desired to test the spring rate R by determining the spring characteristic, the testing shall be carried out in the range from 0,3  $F_{\rm n}$  to 0,7  $F_{\rm n}$  to make sure to cover the linear portion, in doing so  $F_{\rm n}$  has to be associated with the smallest permissible test length  $L_{\rm n}$ .

The spring rate R is therefore:

$$R = \frac{\Delta F}{\Delta L} = \frac{\Delta F}{\Delta s} = \frac{F_2 - F_1}{L_1 - L_2} = \frac{F_2 - F_1}{s_2 - s_1}$$
 (6)

where  $\Delta F$  is the increase in force corresponding to a reduction in length  $\Delta L$  or the increase in deflection  $\Delta s$  (see Figure 6).

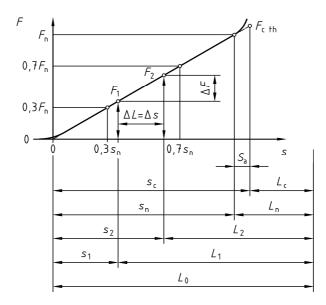


Figure 6 — Test diagram

#### 7.3 Test load for pressing to solid length (settling testing)

Testing to solid length  $L_c$  shall be performed with not more than 1,5 times the theoretical spring force  $F_{c\,th}$  corresponding to the solid length  $L_c$ .

Any testing of solid length is to be agreed between manufacturer and customer.

# Annex A (informative)

#### **Declaration and formulas**

This European Standard contains the agreements reached, in the present state of the art, between the branches of industry concerned regarding design, requirements and testing of cold coiled compression springs within the limits given in table 1. The permissible variations have been specified in a way that the manufacture and acceptance of relatively small quantities can also be performed with economically acceptable effort. For compression springs the quality grades 1, 2 and 3 are specified, the permissible variations being, for quality grade 1, 0,63 times, and for quality grade 3, 1,6 times those of the medium quality grade 2. Compression springs with force and length variations corresponding to quality grade 1 can be made with an average 1 % reject rate by utilizing ordinary production facilities and applying the measuring methods prevailing at the present day. Springs of this kind shall be 100 % tested and this entails increased expenditure in production. Quality grade 2 should therefore be specified as preferred because this quality grade can be guaranteed by adopting properly organized in-manufacture spot testing instead of 100 % testing. Quality grade 2 will usually yield the most favourable cost-quality ratio.

The average failure rate of 1 % for tolerances of force and lengths for quality grade 1 corresponds statistically to a spread of  $\pm$  2,58 s (s = standard deviation of the normal distribution, see ISO 16269-6).

The equations for figures 3, 4 and 5 are as follows:

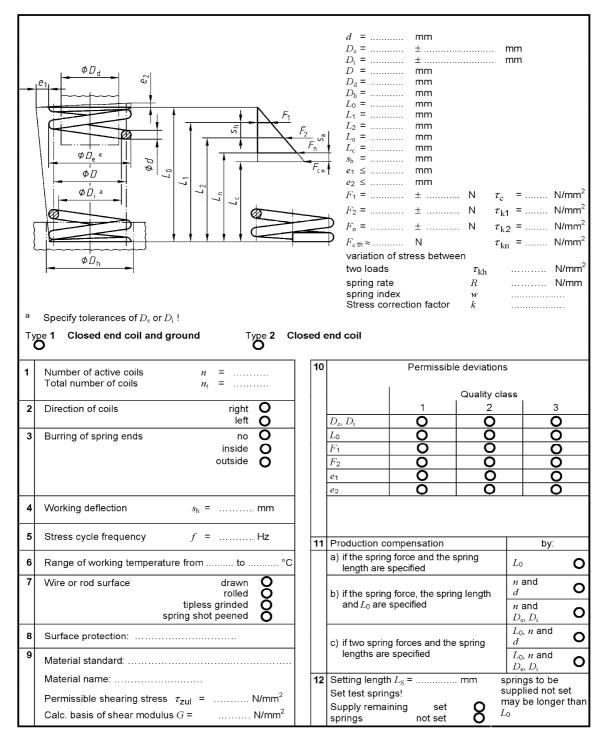
$$k_{\rm f} = -\frac{1}{3 \cdot n^2} + \frac{8}{5 \cdot n} + 0,803 \tag{A.1}$$

$$a_{\rm F} = 65,92 \cdot \frac{d^{3,3}}{D^{1,6}} \cdot \left[ -0,84 \left( \frac{w}{10} \right)^3 + 3,781 \left( \frac{w}{10} \right)^2 - 4,244 \frac{w}{10} + 2,274 \right]$$
(A.2)

$$w = \frac{D}{d} \tag{A.3}$$

Applying these equations the spring index shall be  $4 \le w \le 20$  (see Table 1).

### **Example - Specification for a Cylindrical Helical Compression Spring**



The user of this form is allowed to copy this present form.

The terms  $\emph{k},~\tau_{c},~\tau_{k1},~\tau_{k2},~\tau_{kn},~\tau_{kh}$  and  $~\tau_{zul}$  detailed in Table B.1 are taken from EN 13906-1.

Table B.1

Symbol	Unit	Name
k	_	Stress correction factor (depending on <i>D</i> / <i>d</i> )
$ au_{ m c}$	N/mm <sup>2</sup>	Uncorrected torsional stress, for the solid length $L_{ m c}$
$\tau_{\mathrm{k1}},~\tau_{\mathrm{k2}}~\dots$	N/mm <sup>2</sup>	Corrected torsional stress, for the spring forces $F_1, F_2 \dots$
$ au_{ m kh}$	N/mm <sup>2</sup>	Corrected torsional stress range, for the stroke $s_{ m h}$
$ au_{ m kn}$	N/mm <sup>2</sup>	Corrected torsional stress, for the spring force $F_n$
$ au_{zul}$	N/mm <sup>2</sup>	Permissible torsional stress

# **Bibliography**

- [1] ISO 16269-6, Statistical interpretation of data Part 6: Determination of statistical tolerance intervals
- [2] EN 13906-1, Cylindrical helical springs made from round wire and bar Calculation and design Part 1: Compression springs

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