BS EN 847-2:2013



BSI Standards Publication

Tools for woodworking — Safety requirements

Part 2: Requirements for the shank of shank mounted milling



BS EN 847-2:2013 BRITISH STANDARD

National foreword

This British Standard is the UK implementation of EN 847-2:2013. It supersedes BS EN 847-2:2001 which is withdrawn.

The UK participation in its preparation was entrusted to Technical Committee MTE/23, Woodworking machines.

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Foreword

This document (EN 847-2:2013) has been prepared by Technical Committee CEN/TC 142 "Woodworking machines - Safety", the secretariat of which is held by UNI.

This European Standard shall be given the status of a national standard, either by publication of an identical text or by endorsement, at the latest by April 2014, and conflicting national standards shall be withdrawn at the latest by April 2014.

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This document supersedes EN 847-2:2001.

The following table contains a list of modifications from the previous edition.

EN 847-2:2001	EN 847-2:2013	Reason
1 Scope	1 Scope:	ed/te
	Precision of the indent	
	New paragraph: applies also for shank tools with a cutting diameter of less than 16 mm	
3 Quantities and units	3 Terms and definitions	ed
5 Tool marking	5 Safety requirements:	te (missing requirements)
	5.1 General requirements for cylindrical shank	
	5.2 Stability of the shank of the shank mounted tools	
	5.3 Stability of HSK mounted tools	
6 Safety requirements	6 Tool marking	te
	Changed symbol for the free shank length	
Annex A: Method of measuring the eccentricity at clamping devices	Annex A: Examples of calculation	ed
Annex B: Example of calculation	Annex B: Method of measuring the eccentricity at clamping devices	ed
	New: Bibliography	ed

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Introduction

The content of this European Standard is aimed at eliminating hazards which can lead to overloading of the shank of shank mounted milling tools for woodworking by excessive rotational speeds.

1 Scope

This European Standard specifies the determination of the maximum speed for given eccentricity at clamping devices for the shank strength of milling tools with cylindrical and taper shank. It also specifies the marking of the tool. Bore mounted tools which are mounted on an arbour should be considered as a shank mounted tool.

This European Standard complements EN 847-1 and applies also for shank tools with a cutting diameter of less than 16 mm.

2 Normative references

The following documents, in whole or in part, are normatively referenced in this document and are indispensable for its application. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

EN 847-1:2013, Tools for woodworking — Safety requirements — Part 1: Milling tools, circular saw blades

EN ISO 12100:2010, Safety of machinery — General principles for design — Risk assessment and risk reduction (ISO 12100:2010)

ISO 1940-1, Mechanical vibration — Balance quality requirements for rotors in a constant (rigid) state — Part 1: Specification and verification of balance tolerances

3 Terms and definitions

For the purposes of this document, the terms and definitions given in EN 847-1:2013 and the following apply.

3.1

7/24 shank

SK

type of toolholder with a 7/24 cone ratio taper that contacts the spindle on two surfaces

Note 1 to entry: Toolholder with a 7/24 cone ratio taper; see Bibliography.

3.2

hollow taper shank

HSK

type of toolholder with a short hollow taper with a high positioning accuracy and high grade of rigidity that contacts the spindle on two surfaces

Note 1 to entry: Toolholder with 1:1,09 cone ratio hollow taper shank; see Bibliography.

3.3

arbour

device to mount in or on the spindle of a machine tool, and which is designed to carry and drive a bore type cutting tool

4 List of significant hazards

Table 1 shows the list of significant hazards.

Table 1 — List of significant hazards

Hazard according to EN ISO 12100:2010	Condition or causes of hazard related to the tool	Corresponding clause of EN 847-2
Mechanical hazards due to:	Breaking of the tool	5
Inadequacy of mechanical strength	breaking of the tool	5
Vibration	Dynamic unbalance of tool	5
Variations in the rotational speed of tools	Breaking of the tool	5

5 Safety requirements

5.1 General requirements for cylindrical shank

The minimum value for the clamping length $l_{e min}$ shall be as given in Table 2.

Table 2 — Minimum clamping length $l_{e min}$

$d_2 \le 10 \text{ mm}$	10 mm < d ₂ < 25 mm	$d_2 \ge 25 \text{ mm}$
$l_{\rm emin}$ = 20 mm	$l_{\text{e min}} = 2 \cdot d_2 \text{ (mm)}$	$l_{\text{e min}}$ = 1,8 · d_2 (mm)

The tolerance of the shank diameter d_2 shall be h6 for $d_2 \ge 12$ mm and h8 for $d_2 < 12$ mm. The method of measuring the eccentricity e_m at clamping devices, as given in Annex B, shall be used.

5.2 Stability of the shank of mounted tools

Every shank of a mounted milling tool shall be calculated with the quantities and units as shown in Figure 1a) (with $d = d_2$).

If the shank mounted milling tool is clamped in a taper holder, the cone strength shall be calculated with the quantities and units as shown in Figure 1b) (with $d = d_3$).

If tools are mounted on a taper shank, the shank strength of the clamping diameter shall be calculated with the quantities and units as shown in Figure 1c) with

$$l_{e} = l_{g}$$

 $l_{0} = 0$

$$d_4 = 1.4 \cdot d_{arbour}$$
 $(d_{arbour} \le 50 \text{mm})$

$$d_4 = 20 + d_{arbour}$$
 $(d_{arbour} > 50 \text{mm})$

NOTE 1 Clamping systems:

- with axial clamping force [Fa] $d = d_4$;
- without axial clamping force [Fa] $d = d_{arbour}$.

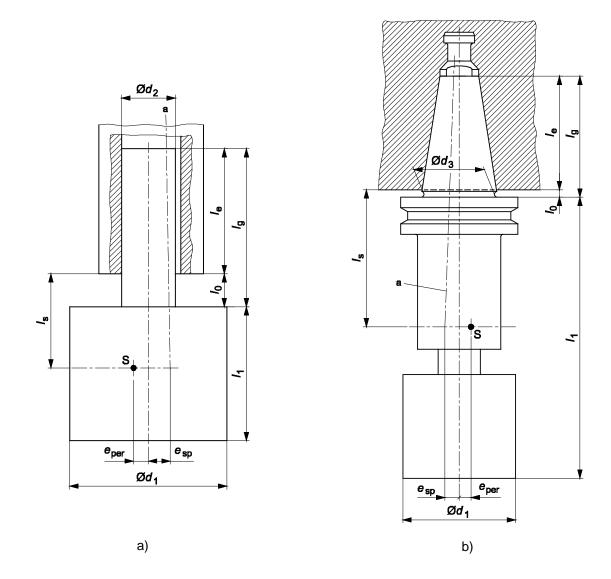
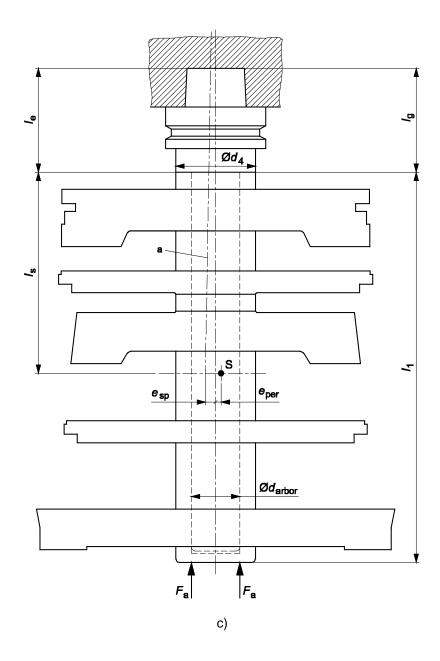


Figure 1 — Quantities for calculation of $n_{\rm shank}$ (1 of 2)



Key

a axis of rotation

Figure 1 — Quantities for calculation of n_{shank} (2 of 2)

For balance quality, see EN 847-1:2013, Table 5.

For calculation of n with a given $e_{\rm sp}$ the following formula applies:

$$n_{\text{shank}} = \frac{30}{\sqrt{f_{\text{S}} \cdot \pi}} \cdot \frac{-G + \sqrt{G^2 + \frac{W \cdot \sigma_{\text{W}}}{m} \cdot l_{\text{S}}} \cdot \left(e_{\text{Sp}} + \frac{W \cdot \sigma_{\text{W}} \cdot l_{\text{S}}^2}{3 \cdot E \cdot I}\right) \cdot 10^6}{e_{\text{Sp}} + \frac{W \cdot \sigma_{\text{W}} \cdot l_{\text{S}}^2}{3 \cdot E \cdot I}}$$
(1)

For calculation of e_{sp} with a given n the following formula applies:

$$e_{SP} = \frac{1}{n} \cdot \left[\left(\frac{30}{\sqrt{f_S \cdot \pi}} \right)^2 \cdot \frac{W \cdot \sigma_W}{m \cdot I_S \cdot n} \cdot 10^6 - \frac{30 \cdot G}{\pi} \right] \cdot \frac{W \cdot \sigma_W \cdot I_S^2}{3 \cdot E \cdot I}$$
 (2)

$$e_{\text{per}} = \frac{30 \cdot G}{\pi \cdot n_{\text{shank}}} \tag{3}$$

The mass $m_{\rm cut}$ of the tool components related to the centre of gravity S in the area of l_0 + l_1 , is given in Figure 1.

$$m^* = f \cdot m_{\text{cut}} \tag{4}$$

$$f = 0.04 + 0.17 \cdot \ln (m_{\text{cut}}) \tag{5}$$

This is an empiric formula of which the result is only valid between 0,6 and 0,9. If the result is less than 0,6 use 0,6, and if the result is greater than 0,9 use 0,9. The form factor takes into account the deviation of the actual form (e.g. gullet; flattening) from the solid body form of the tool without shank.

NOTE 2 The expression "In (m_{cut}) " is the natural logarithm of mass of the tool without shank.

$$I = \pi \cdot \frac{d^4}{64} \tag{6}$$

$$l_0 = l_g - l_e \tag{7}$$

If known the real mass can be used in place of the reduced mass.

$$W = \pi \cdot \frac{d^3}{32} \tag{8}$$

EXAMPLE Figure 2 and Formula (9) give an example for the calculation of the distance l_s .

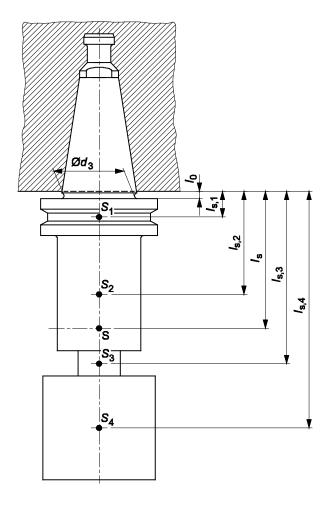


Figure 2 — Distances of the gravity centres of the tool components

$$l_{S} = \frac{m_{1} \cdot l_{S,1} + m_{2} \cdot l_{S,2} + m_{3} \cdot l_{S,3} + m_{4} \cdot l_{S,4}}{m_{1} + m_{2} + m_{3} + m_{4}}$$
(9)

Table 3 — Stability of the shank of the shank mounted tools — Quantities and units

Quantity	Description	Unit
d	diameter	mm
	a) shank diameter d_2	
	b) cone diameter d_3	
	c) with axial force d_4 : calculated; without axial force: d_{arbour}	
d_1	tool diameter	mm
d_2	shank diameter, see Figure 1a)	mm
d_3	cone diameter, see Figure 1b)	mm
d_4	calculated hub diameter, see Figure 1c)	mm
d_{arbour}	shank diameter of the arbour, see Figure 1c)	mm
E	modulus of elasticity	N mm
$e_{\mathrm{pe}r}$	permissible gravity centre displacement	mm
$e_{ m sp}$	eccentricity at clamping device ^a	mm
f	form factor	
f_{s}	safety factor ($f_S = 4$)	./.
F_{a}	axial clamping force, see Figure 1c)	N
G	product of the permissible eccentricity and the angular velocity according to ISO 1940-1	mm s
I	second moment of area	mm ⁴
l_1	height of tool components	mm
l_0	free shank length	mm
$l_{ m s}$	distance of gravity centre measured from the end of the clamping device	mm
$l_{ m e}$	clamping length	mm
l_{g}	total length of shank	mm
$m_{ m cut}$	mass of the tool components related to the centre of gravity S in the area of $l_0 + l_1$, see Figure 1a) to Figure 1c)	
m*	reduced mass of the tool	g
n	operational speed	min ⁻
n_{shank}	maximum permissible rotational speed with regard to shank strength	min ⁻
S	centre of gravity	
W	section modulus	mm ³
$\sigma_{\!\scriptscriptstyle m w}$	fatigue strength under reversed bending stresses of shank material	N mm
ρ	density of shank material	g mm

For general use $n_{\rm shank}$ shall be calculated for $e_{\rm sp}$ = 0,1 mm and for tools used on NC- and CNC-machines $n_{\rm shank}$ shall be calculated for $e_{\rm sp}$ = 0,06. In other cases the value of $e_{\rm sp}$ shall be taken according to the formula.

serial tests in order to provide the designer with safety indications and to reduce hazards.

EN 847-2:2013 (E)

NOTE 3 The safety requirements for the shank strength are fulfilled when, using the given tool sizes and material characteristics with defined free shank length l_0 , gravity centre displacement $e_{\rm per}$ and eccentricity at clamping device $e_{\rm sp}$, the maximum permissible rotational speed for the shank $n_{\rm shank}$ is not exceeded during operation. The cutting force is not significant in comparison with the centrifugal force. Therefore, the cutting force has not been taken into account.

For the operation of complex shank mounted milling tools it has to be considered that the maximum permissible operational speed may not exceed the lower value of the two maximum speed values for the shank strength (n_{shank}) as well as the strength to overspeed load (n_{max}) in accordance with EN 847-1:2013, 5.1.4.1.

5.3 Stability of HSK mounted tools

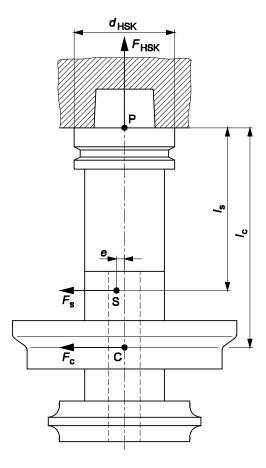


Figure 3 — Quantities for calculation of n_{HSK}

If more than one tool is mounted on an HSK-arbour the tool with the highest value $F_{C} \times l_{C}$ should be used for the calculation of n_{HSK} .

For calculation of n_{HSK} the following formula applies:

$$n_{\rm HSK} = \frac{30}{\sqrt{f_S \cdot \pi}} \cdot 10^3 \cdot \sqrt{\frac{F_{\rm HSK} \cdot \frac{d_{\rm HSK}}{2} - F_{\rm c} \cdot l_{\rm c}}{m \cdot e \cdot l_{\rm s}}}$$
(10)

$$e = e_{\mathsf{HSK}} + e_{\mathsf{M}} + e_{\mathsf{T}} \tag{11}$$

$$e_{\mathsf{HSK}} = \frac{2 \cdot (l_{\mathsf{s}} \cdot t_{\mathsf{p}})}{d_{\mathsf{HSK}}} + t_{\mathsf{r}} \tag{12}$$

$$e_{\mathsf{M}} = \frac{D_{\mathsf{bmax}} - d_{s\min}}{2} \tag{13}$$

$$e_{\mathsf{T}} = \frac{G}{\omega} = \frac{G_{\mathsf{T}} \cdot 30}{\pi \cdot n_{\mathsf{max}}} \tag{14}$$

If F_c is unknown, F_c can be calculated according to EN 847-1:

$$F_{\rm c} = F_{\rm m} \cdot b_{\rm 1}$$

 $F_{\rm m} = 50 \ \text{N/mm}$ (for tools with a cutting radius $r_1 \leq 20 \ \text{mm}$)

$$F_{\rm m} = \frac{30 \cdot P_{\rm Mot}}{r_{\rm l} \cdot h_{\rm max} \cdot \pi} \cdot 10^{6} \text{ (for tools with a cutting radius } r_{\rm l} > 20 \text{ mm)}$$
 (15)

Alternative F_c can be calculated as transmissible force according to the spindle power:

$$F_{\rm C} = \frac{P_{\rm C}}{v_{\rm C}} \approx \frac{30 \cdot P_{\rm Mot}}{\pi \times r_{\rm 1} \cdot n_{\rm max}} \cdot 10^6 \tag{16}$$

Table 4 — Stability of HSK mounted tools — Quantity and units

Quantity	Description	Unit
С	resulting working point of the cutting forces reduced to the tool axis	./.
<i>b</i> ₁	cutting width according to EN 847-1	mm
$D_{b\;max}$	maximum bore diameter (e.g. tool bore)	mm
d_{HSK}	nominal diameter of the HSK (e.g. HSK-F63: d_{HSK} = 63 mm)	mm
$d_{s\;min}$	minimum shaft diameter (e.g. arbour)	mm
е	gravity centre displacement of the complete tool (worst case)	mm
e_{HSK}	eccentricity of the tool caused by the tolerances of the HSK	mm
e_{M}	eccentricity of the tool caused by mounting tolerances between bore and arbour	mm
e_{T}	gravity centre displacement of the mounted tool caused by unbalancing	mm
$F_{\mathtt{C}}$	cutting force	N
F_{m}	specific cutting force	N/mm
F_{HSK}	clamping force of the HSK (guideline values are given in DIN 69893)	N
<i>f</i> s	safety factor ($f_S = 4$)	./.
G	product of the permissible eccentricity and the angular velocity according to ISO 1940-1	mm s ⁻¹
l_{c}	axial distance of the working point of the cutting force from the face stop of the HSK	mm
ls	distance of the gravity centre from the face stop of the HSK	mm
m	total mass of the complete tool (individual tools, arbour, spacers, HSK)	g
n_{HSK}	maximum permissible rotational speed of the HSK interface	min ⁻¹
$n_{\sf max}$	maximum rotational speed of the tool according to EN 847-1	min ⁻¹
R_1	cutting radius according to EN 847-1	mm
S	centre of gravity	./.
t_{p}	planarity tolerance of the face stop of the HSK according to DIN 69893	mm
t_{f}	run-out tolerance of the HSK according to DIN 69893	mm
P	working point of the insertion force on the HSK	./.
P_c	cutting power	kW
P_{Mot}	spindle motor power	kW

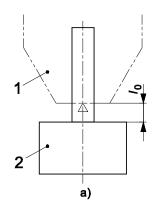
6 Tool marking

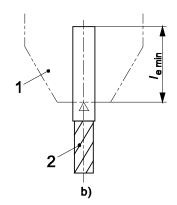
Tool marking shall include the following items:

- a) The maximum rotational speed n_{max} or n_{shank} according to EN 847-1:2013, 5.1.4, whichever is the lower;
- b) the permissible eccentricity e;

EXAMPLE Tool marking example for list items a) and b): " n_{max} 12 000 e 0,06".

- c) the free shank length l_0 or the minimum clamping length $l_{e min}$ according to Figure 4:
 - 1) if $n_{\text{shank}} < n_{\text{max}}$: the free shank length l_0 ,
 - 2) if $n_{\rm shank} \ge n_{\rm max}$: the minimum clamping length $l_{\rm e\,min}$ (see Table 2).





Key

1 chuck2 tool

 l_0 free shank length

 $\it l_{\rm e\,min}$ minimum clamping length

Figure 4 — Marking of the maximum free shank length

Annex A (informative)

Examples of calculation

A.1 Example of a calculation of n_{shank}

See Figure 1a).

Table A.1 — Calculation of n_{shank}

Description	Quantity	Value	Unit
Shank diameter	d_2	25	mm
Total shank length	$l_{ m g}$	80	mm
Free shank length	l_0	25	mm
Tool diameter	d_1	125	mm
Tool height	l_1	40	mm
Form factor	f	0,9	
Mass of cutting part	$f \cdot m_{ ext{cut}}$	3 468,02	g
Reduced total mass	m*	3 492,11	g
Distance of gravity centre	$l_{ m s}$	45	mm
${\it G}$ for balance quality grade ${\it G}$ 40 for complex tools	G	40	mm s ⁻¹
Fatigue strength under reversed stresses	$\sigma_{\!\scriptscriptstyle m W}$	340	N mm ⁻²
Eccentricity at clamping device	$e_{\sf sp}$	0,1	mm
Modulus of elasticity (steel)	E	210 000	N mm ⁻²
Density (steel)	ρ	0,007 85	g mm ⁻³
Permissible maximum rotational speed	$n_{ m shank}$	19 098	min ⁻¹

A.2 Example of a calculation of $n_{\rm HSK}$

See Figure 3.

Table A.2 — Calculation of $n_{\rm HSK}$

Description	Quantity	Value	Unit
Safety factor	fs	4	
Clamping force of HSK	F_{HSK}	11 000	N
Nominal diameter of HSK	d_{HSK}	63,00	mm
Cutting force	F_{c}	500	N
Axial distance of cutting force	l_{c}	250,00	mm
Total mass of tool	m	8 000	g
Gravity centre displacement	e	0,040 0	mm
Axial distance of gravity centre	l_{s}	200,00	mm
Maximum rotational speed of HSK	n_{HSK}	8 883	min ⁻¹

Annex B

(informative)

Method of measuring the eccentricity at clamping devices

The diameter of the test mandrel is the nominal diameter of the clamping device.

For the test mandrel the following shall apply:

a) test mandrel diameter tolerance: h6/h8 in accordance with Clause 5;

b) test mandrel cylindricity: 0,002 mm;

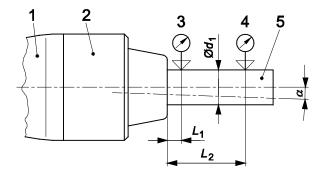
c) test mandrel straightness: 0,002 mm;

d) test mandrel roundness: 0,002 mm;

e) surface without longitudinal marks;

f) surface roughness: max. $R_z = 4 \mu m$;

g) surface hardness: 58 + 3 HRC.



Key

- 1 driving spindle/clamping device shank
- 2 clamping device
- 3 test point 1
- 4 test point 2
- 5 test mandrel

$$L_1 = 10 \text{ mm}$$

$$L_2 = (l_g + l_1) - l_e$$

with l_g , l_1 and l_e , see Figure 1a)

- t₁ run-out at test point 1
- t₂ run-out at test point 2
- α angular deviation

Figure B.1 — Illustration of the measuring method

Eccentricity:
$$em = \frac{t1+t2}{4}$$
 (B.1)

The eccentricity $e_{\rm m}$ shall be $\leq e_{\rm sp}$.

Bibliography

- [1] ISO 297, 7/24 tapers for tool shanks for manual changing
- [2] ISO 7388-1, Tool shanks with 7/24 taper for automatic tool changers Part 1: Dimensions and designation of shanks of forms A, AD, AF, U, UD and UF
- [3] ISO 7388-2, Tool shanks with 7/24 taper for automatic tool changers Part 2: Dimensions and designation of shanks of forms J, JD and JF
- [4] ISO 12164-1, Hollow taper interface with flange contact surface Part 1: Shanks Dimensions





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