BS EN ISO 3506-1:2009

Mechanical properties of corrosion-resistant stainless steel fasteners

Part 1: Bolts, screws and studs

ICS 21.060.10



National foreword

This British Standard is the UK implementation of EN ISO 3506-1:2009. It supersedes BS EN ISO 3506-1:1998 which is withdrawn.

The UK participation in its preparation was entrusted to Technical Committee FME/9/1, Mechanical properties of fasteners.

A list of organizations represented on this committee can be obtained on request to its secretary.

This publication does not purport to include all the necessary provisions of a contract. Users are responsible for its correct application.

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Caractéristiques mécaniques des éléments de fixation en acier inoxydable résistant à la corrosion - Partie 1: Vis et goujons (ISO 3506-1:2009)

Mechanische Eigenschaften von Verbindungselementen aus nichtrostenden Stählen - Teil 1: Schrauben (ISO 3506-1:2009)

This European Standard was approved by CEN on 24 October 2009.

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EUROPEAN COMMITTEE FOR STANDARDIZATION COMITÉ EUROPÉEN DE NORMALISATION EUROPÄISCHES KOMITEE FÜR NORMUNG

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Foreword

This document (EN ISO 3506-1:2009) has been prepared by Technical Committee ISO/TC 2 "Fasteners" in collaboration with Technical Committee CEN/TC 185 "Fasteners", the secretariat of which is held by DIN.

This European Standard shall be given the status of a national standard, either by publication of an identical text or by endorsement, at the latest by May 2010, and conflicting national standards shall be withdrawn at the latest by May 2010.

Attention is drawn to the possibility that some of the elements of this document may be the subject of patent rights. CEN [and/or CENELEC] shall not be held responsible for identifying any or all such patent rights.

This document supersedes EN ISO 3506-1:1997.

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Endorsement notice

The text of ISO 3506-1:2009 has been approved by CEN as a EN ISO 3506-1:2009 without any modification.

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Foreword

ISO (the International Organization for Standardization) is a worldwide federation of national standards bodies (ISO member bodies). The work of preparing International Standards is normally carried out through ISO technical committees. Each member body interested in a subject for which a technical committee has been established has the right to be represented on that committee. International organizations, governmental and non-governmental, in liaison with ISO, also take part in the work. ISO collaborates closely with the International Electrotechnical Commission (IEC) on all matters of electrotechnical standardization.

International Standards are drafted in accordance with the rules given in the ISO/IEC Directives, Part 2.

The main task of technical committees is to prepare International Standards. Draft International Standards adopted by the technical committees are circulated to the member bodies for voting. Publication as an International Standard requires approval by at least 75 % of the member bodies casting a vote.

Attention is drawn to the possibility that some of the elements of this document may be the subject of patent rights. ISO shall not be held responsible for identifying any or all such patent rights.

ISO 3506-1 was prepared by Technical Committee ISO/TC 2, Fasteners, Subcommittee SC 1, Mechanical properties of fasteners.

This second edition cancels and replaces the first edition (ISO 3506-1:1997), which has been technically revised.

ISO 3506 consists of the following parts, under the general title *Mechanical properties of corrosion-resistant stainless steel fasteners*:

- Part 1: Bolts, screws and studs
- Part 2: Nuts
- Part 3: Set screws and similar fasteners not under tensile stress
- Part 4: Tapping screws

Introduction

In the preparation of this part of ISO 3506, special attention has been given to the fundamentally different property characteristics of the stainless steel fastener grades compared with those of carbon steel and low-alloy steel fasteners. Ferritic and austenitic stainless steels are strengthened only by cold working and consequently, the components do not have as homogeneous local material properties as hardened and tempered parts. These special features have been recognized in the elaboration of the property classes and the test procedures for mechanical properties. The latter differ from the carbon steel and low-alloy steel fastener test procedures with regard to the measurement of the stress at 0,2 % permanent strain (yield stress) and ductility (total elongation after fracture).

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ISO 3506-1:2009(E)

Mechanical properties of corrosion-resistant stainless steel fasteners —

Part 1:

Bolts, screws and studs

1 Scope

This part of ISO 3506 specifies the mechanical properties of bolts, screws and studs made of austenitic, martensitic and ferritic steel grades of corrosion-resistant stainless steels, when tested over an ambient temperature range of 10 °C to 35 °C. Properties vary at higher or lower temperatures.

This part of ISO 3506 applies to bolts, screws and studs

- with nominal thread diameter $d \leq 39$ mm,
- of triangular ISO metric threads with diameters and pitches in accordance with ISO 68-1, ISO 261 and ISO 262, and
- of any shape.

It does not apply to screws with special properties, such as weldability.

NOTE The designation system of this part of ISO 3506 can be used for sizes outside the limits given in this clause (e.g. d > 39 mm), provided that all applicable mechanical and physical requirements of the property classes are met.

This part of ISO 3506 does not define corrosion or oxidation resistance in particular environments. However, some information on materials for particular environments is given in Annex E. Regarding definitions of corrosion and corrosion resistance, see ISO 8044.

The aim of this part of ISO 3506 is the classification of corrosion-resistant stainless steel fasteners $^{1)}$ into property classes. Some materials can be used at temperatures down to $-200\,^{\circ}$ C, while some can be used at temperatures up to $+800\,^{\circ}$ C in air. Information on the influence of temperature on mechanical properties is found in Annex F.

Corrosion and oxidation performances and mechanical properties for use at elevated or sub-zero temperatures can be agreed on between the user and the manufacturer in each particular case. Annex G shows how the risk of intergranular corrosion at elevated temperatures depends on the carbon content.

All austenitic stainless steel fasteners are normally non-magnetic in the annealed condition; after cold working, some magnetic properties can be evident (see Annex H).

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¹⁾ The term "fasteners" is used when bolts, screws and studs are considered all together.

Normative references

The following referenced documents are indispensable for the application of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

- ISO 68-1, ISO general purpose screw threads Basic profile Part 1: Metric screw threads
- ISO 261, ISO general purpose metric screw threads General plan
- ISO 262, ISO general purpose metric screw threads Selected sizes for screws, bolts and nuts
- ISO 898-1, Mechanical properties of fasteners made of carbon steel and alloy steel Part 1: Bolts, screws and studs with specified property classes — Coarse thread and fine pitch thread
- ISO 3651-1, Determination of resistance to intergranular corrosion of stainless steels Part 1: Austenitic and ferritic-austenitic (duplex) stainless steels — Corrosion test in nitric acid medium by measurement of loss in mass (Huey test)
- ISO 3651-2, Determination of resistance to intergranular corrosion of stainless steels Part 2: Ferritic, austenitic and ferritic-austenitic (duplex) stainless steels — Corrosion test in media containing sulfuric acid
- ISO 6506-1, Metallic materials Brinell hardness test Part 1: Test method
- ISO 6507-1, Metallic materials Vickers hardness test Part 1: Test method
- ISO 6508-1, Metallic materials Rockwell hardness test Part 1: Test method (scales A, B, C, D, E, F, G, H, K, N, T)
- ISO 6892-1, Metallic materials Tensile testing Part 1: Method of test at room temperature
 - ISO 16048, Passivation of corrosion-resistant stainless-steel fasteners
 - ISO 16426, Fasteners Quality assurance system

elongation after fracture

Symbols 3

	•
$A_{\mathrm{S,nom}}$	nominal stress area
d	nominal thread diameter
d_1	basic minor diameter of external thread
d_2	basic pitch diameter of external thread
d_3	minor diameter of external thread (for stress calculation)
H	height of the fundamental triangle of the thread
L_1	total length of fastener
L_2	total length of fastener after fracture
L_3	distance between the underside of the head and the threaded adapter
1	nominal length of the fastener
l_{S}	plain shank length

 M_{B} breaking torque

P pitch of the thread

*R*_{eL} lower yield stress

*R*_m tensile strength

 $R_{p0,2}$ stress at 0,2 % permanent strain

lpha wedge angle

 $\mu_{\rm r}$ permeability value in a magnetic field

4 Designation, marking and finish

4.1 Designation

The designation system for stainless steel grades and property classes for bolts, screws and studs is given in Figure 1. The designation of the material consists of two blocks, which are separated by a hyphen. The first block designates the steel grade and the second block, the property class.

The designation of the steel grade (first block) consists of one of the letters

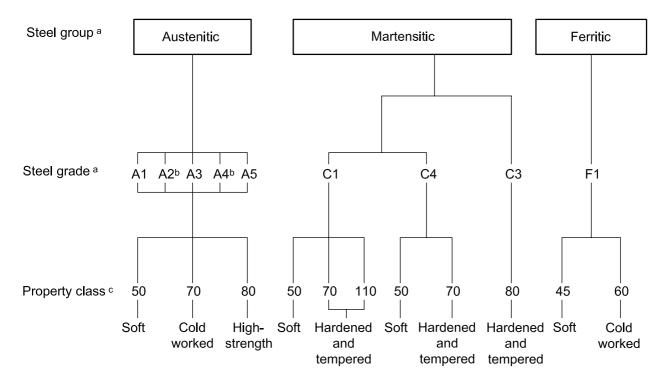
- A for austenitic steel,
- C for martensitic steel, or
- F for ferritic steel

which indicates the group of steel and a digit, which indicates a range of chemical compositions within this steel group (see Table 1).

The designation of the property class (second block) consists of two or three digits representing 1/10 of the tensile strength of the fastener, according to Table 2 or Table 3.

EXAMPLE 1 A2-70 indicates: austenitic steel, cold worked, minimum 700 MPa tensile strength.

EXAMPLE 2 C4-70 indicates: martensitic steel, hardened and tempered, minimum 700 MPa tensile strength.



- ^a The steel groups and steel grades classified in Figure 1 are described in Annex B and specified by the chemical composition given in Table 1.
- b Low-carbon austenitic stainless steels with carbon content not exceeding 0,03 % may additionally be marked with an "L".

EXAMPLE A4L-80

Fasteners passivated in accordance with ISO 16048 may additionally be marked with a "P".

EXAMPLE A4-80P

Figure 1 — Designation system for stainless steel grades and property classes for bolts, screws and studs

4.2 Marking

4.2.1 General

Fasteners manufactured according to the requirements of this part of ISO 3506 shall be designated in accordance with the designation system described in 4.1 and marked in accordance with 4.2.2 and 4.2.3 or 4.2.4, as applicable. However, the designation system described in 4.1 and the provisions for marking according to 4.2.3 or 4.2.4 shall be used only if all relevant requirements of this part of ISO 3506 are met.

Unless otherwise specified in the product standard, the height of embossed markings on the top of the head shall not be included in the head height dimensions.

NOTE For marking of left-hand threads, see ISO 898-1.

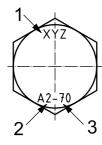
4.2.2 Manufacturer's identification mark

A manufacturer's identification mark shall be included during the manufacturing process on all fasteners which are marked with a property class symbol. Manufacturer's identification marking is also recommended on fasteners which are not marked with a property class symbol.

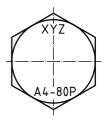
ISO 3506-1:2009(E)

4.2.3 Bolts and screws

All hexagon head bolts and screws, and hexagon or hexalobular socket head cap screws of nominal thread diameter $d \ge 5$ mm shall be clearly marked in accordance with 4.1, Figure 1, Figure 2 and Figure 3. The marking is mandatory and shall include the steel grade and property class.







Key

- 1 manufacturer's identification mark
- 2 steel grade
- 3 property class

Figure 2 — Marking of hexagon head bolts and screws

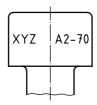




Figure 3 — Marking of hexagon and hexalobular socket head cap screws — Alternative forms

Other types of bolts and screws can be marked in the same way, where it is possible to do so and on the head portion only. Additional marking is allowed, provided it does not cause confusion.

Fasteners that do not fulfil the tensile or torsional requirements because of the geometry (see Clause 6) may be marked with the steel grade, but shall not be marked with the property class (see Figure 4).

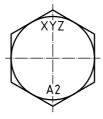


Figure 4 — Marking of fasteners not fulfilling tensile or torsional requirements because of the geometry

4.2.4 Studs

Studs of nominal thread diameter $d \ge 6$ mm shall be clearly marked in accordance with 4.1, Figure 1 and Figure 5. The marking shall be on the unthreaded part of the stud and shall contain the steel grade and property class. If marking on the unthreaded portion is not possible, marking of steel grade only on the nut end of the stud is allowed (see Figure 5).

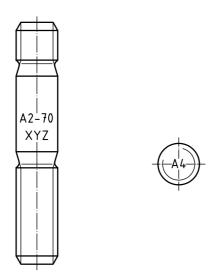


Figure 5 — Marking of studs — Alternative forms

4.2.5 Packages

All packages for all types of fasteners of all sizes shall be marked (e.g. through labelling). The marking or labelling shall include the manufacturer's and/or distributor's identification and the marking symbol for the steel grade and property class according to Figure 1 and the manufacturing lot number, as defined in ISO 16426.

4.3 Finish

Unless otherwise specified, fasteners in accordance with this part of ISO 3506 shall be supplied clean and bright. For maximum corrosion resistance, passivation is recommended. When passivation is required, it shall be performed in accordance with ISO 16048. Fasteners that are passivated may additionally be marked with the symbol "P" after the symbols for steel grade and property class (see footnote c of Figure 1).

For fasteners manufactured to a specific order, the additional marking should be applied to both the fastener and the label. For fasteners delivered from stock, the additional marking should be applied to the label.

5 Chemical composition

The chemical compositions of stainless steels suitable for fasteners in accordance with this part of ISO 3506 are given in Table 1.

The final choice of the chemical composition within the specified steel grade is at the discretion of the manufacturer, otherwise by prior agreement between the purchaser and the manufacturer.

In applications where risk of intergranular corrosion is present, testing in accordance with ISO 3651-1 or ISO 3651-2 is recommended. In such cases, stabilized stainless steels of grades A3 and A5 or stainless steels of grades A2 and A4 with carbon content not exceeding 0,03 % are recommended.

Table 1 — Stainless steel grades — Chemical composition

Steel	Steel grade		Chemical composition ^a mass fraction, %												
group	grade	С	Si	Mn	Р	S	Cr Mo		Ni	Cu					
Austenitic	A1	0,12	1	6,5	0,2	0,15 to 0,35	16 to 19	0,7	5 to 10	1,75 to 2,25	bcd				
	A2	0,10	1	2	0,05	0,03	15 to 20	_е	8 to 19	4	fg				
	A3	0,08	1	2	0,045	0,03	17 to 19	_e	9 to 12	1	h				
	A4	0,08	1	2	0,045	0,03	16 to 18,5	2 to 3	10 to 15	4	gi				
	A5	0,08	1	2	0,045	0,03	16 to 18,5	2 to 3	10,5 to 14	1	hi				
Martensitic	C1	0,09 to 0,15	1	1	0,05	0,03	11,5 to 14	_	1	_	i				
	C3	0,17 to 0,25	1	1	0,04	0,03	16 to 18	_	1,5 to 2,5	_	_				
	C4	0,08 to 0,15	1	1,5	0,06	0,15 to 0,35	12 to 14	0,6	1	_	bi				
Ferritic	F1	0,12	1	1	0,04	0,03	15 to 18	_j	1	_	kl				

NOTE 1 A description of the groups and grades of stainless steels also entering into their specific properties and applications is given in Annex B.

NOTE 2 Examples of stainless steels standardized in accordance with ISO 683-13 and ISO 4954 are given in Annexes C and D, respectively.

NOTE 3 Certain materials for specific application are given in Annex E.

- a Values are maximum, unless otherwise indicated.
- b Sulfur may be replaced by selenium.
- ^c If the nickel content is below 8 %, the minimum manganese content shall be 5 %.
- d There is no minimum limit to the copper content, provided that the nickel content is greater than 8 %.
- ^e Molybdenum may be present at the discretion of the manufacturer. However, if for some applications limiting of the molybdenum content is essential, this shall be stated at the time of ordering by the purchaser.
- f If the chromium content is below 17 %, the minimum nickel content should be 12 %.
- g For austenitic stainless steels having a maximum carbon content of 0,03 %, nitrogen may be present to a maximum of 0,22 %.
- ^h This shall contain titanium $\geqslant 5 \times C$ up to 0,8 % maximum for stabilization and be marked appropriately as specified in this table, or shall contain niobium (columbium) and/or tantalum $\geqslant 10 \times C$ up to 1,0 % maximum for stabilization and be marked appropriately as specified in this table.
- ¹ At the discretion of the manufacturer, the carbon content may be higher where required in order to obtain the specified mechanical properties at larger diameters, but shall not exceed 0,12 % for austenitic steels.
- Molybdenum may be present at the discretion of the manufacturer.
- This may contain titanium $\geq 5 \times C$ up to 0,8 % maximum.
- This may contain niobium (columbium) and/or tantalum $\geq 10 \times C$ up to 1 % maximum.

6 Mechanical properties

The mechanical properties of bolts, screws and studs in accordance with this part of ISO 3506 shall conform to the values given in Tables 2, 3 and 4.

For bolts and screws made of martensitic steel, the strength under wedge loading shall not be below the minimum values for tensile strength shown in Table 3.

For acceptance purposes, the mechanical properties specified in this clause apply and shall be tested according to the test programme in Clause 7.

Even if the material of the fasteners meets all relevant requirements, it is possible that certain fasteners would not fulfil the tensile or torsional requirements because of the geometry of the head, which reduces the shear

area in the head compared to the stress area in the thread such as countersunk, raised countersunk and cheese heads.

NOTE Although a great number of property classes are specified in this part of ISO 3506, this does not mean that all classes are appropriate for all fasteners. Further guidance for application of the specific property classes is given in the relevant product standards.

For non-standard fasteners, the choice already made for similar standard fasteners should be followed as closely as possible.

Table 2 — Mechanical properties for bolts, screws and studs — Austenitic steel grades

Steel group	Steel grade	Property class	Tensile strength $R_{ m m}^{\ \ a}$ min. MPa	Stress at 0,2 % permanent strain $R_{\rm p0,2}{}^{\rm a}$ min. MPa	Elongation after fracture Ab min. mm
Austenitic	A1, A2,	50	500	210	0,6 <i>d</i>
	A3, A4,	70	700	450	0,4 <i>d</i>
	A5	80	800	600	0,3 <i>d</i>

The tensile stress is calculated on the stress area (see Annex A).

Table 3 — Mechanical properties for bolts, screws and studs — Martensitic and ferritic steel grades

Steel group	Steel grade	Property class	Tensile strength $R_{\rm m}^{\rm a}$ min.	Stress at 0,2 % permanent strain $R_{\rm p0,2}{}^{\rm a}$ min.	Elongation after fracture A ^b min.		Hardness	
			MPa	MPa	mm	НВ	HRC	HV
Martensitic		50	500	250	0,2 <i>d</i>	147 to 209	_	155 to 220
	C1	70	700	410	0,2 <i>d</i>	209 to 314	20 to 34	220 to 330
		110 ^c	1 100	820	0,2 <i>d</i>	_	36 to 45	350 to 440
	C3	80	800	640	0,2 <i>d</i>	228 to 323	21 to 35	240 to 340
	C4	50	500	250	0,2 <i>d</i>	147 to 209	_	155 to 220
	C 4	70	700	410	0,2 <i>d</i>	209 to 314	20 to 34	220 to 330
Ferritic	F1 ^d	45	450	250	0,2 <i>d</i>	128 to 209	_	135 to 220
		60	600	410	0,2 <i>d</i>	171 to 271	_	180 to 285

The tensile stress is calculated on the stress area (see Annex A).

This is determined according to 7.2.4, on the actual screw length and not on a prepared test piece.

This is determined according to 7.2.4, on the actual screw length and not on a prepared test piece.

C Hardened and tempered at a minimum tempering temperature of 275 °C.

Nominal thread diameter $d \leq 24$ mm.

Table 4 — Minimum breaking torque, $M_{\rm B,min.}$, for austenitic steel grade bolts and screws M1,6 to M16 (coarse thread)

Thread	Breaking torque, M _B min. Nm Property class									
	50 70 80									
M1,6	0,15	0,2	0,24							
M2	0,3	0,4	0,48							
M2,5	0,6	0,9	0,96							
M3	1,1	1,6	1,8							
M4	2,7	3,8	4,3							
M5	5,5	7,8	8,8							
M6	9,3	13	15							
M8	23	32	37							
M10	46	65	74							
M12	80	110	130							
M16	210	290	330							

Minimum breaking torque values for martensitic and ferritic steel grade fasteners shall be agreed upon between the manufacturer and the user.

7 Testing

7.1 Test programme

The tests that shall be performed, depending on steel grade and bolt, screw or stud length, are given in Table 5.

Table 5 — Test programme

Steel grade	Tensile strength ^a	Breaking torque ^b	Stress at 0,2 % permanent strain $R_{\rm p0,2}^{\rm a}$	Elongation after fracture A^a	Hardness	Strength under wedge loading
A1	$l \geqslant 2,5d^{\text{c}}$	<i>l</i> < 2,5 <i>d</i>	<i>l</i> ≥ 2,5 <i>d</i> ^c	<i>l</i> ≥ 2,5 <i>d</i> ^c	_	_
A2	<i>l</i> ≥ 2,5 <i>d</i> ^c	l < 2,5d	<i>l</i> ≥ 2,5 <i>d</i> ^c	<i>l</i> ≥ 2,5 <i>d</i> ^c	_	_
А3	<i>l</i> ≥ 2,5 <i>d</i> ^c	l < 2,5d	<i>l</i> ≥ 2,5 <i>d</i> ^c	<i>l</i> ≥ 2,5 <i>d</i> ^c	_	_
A4	$l \geqslant 2,5d^{\text{c}}$	<i>l</i> < 2,5 <i>d</i>	<i>l</i> ≥ 2,5 <i>d</i> ^c	<i>l</i> ≥ 2,5 <i>d</i> ^c	_	_
A5	<i>l</i> ≥ 2,5 <i>d</i> ^c	l < 2,5d	<i>l</i> ≥ 2,5 <i>d</i> ^c	<i>l</i> ≥ 2,5 <i>d</i> ^c	_	_
C1	$l \geqslant 2,5d^{cd}$	_	<i>l</i> ≥ 2,5 <i>d</i> ^c	<i>l</i> ≥ 2,5 <i>d</i> ^c	Required	$l_s \geqslant 2d$
С3	$l \geqslant 2,5d^{\text{cd}}$	_	<i>l</i> ≥ 2,5 <i>d</i> ^c	<i>l</i> ≥ 2,5 <i>d</i> ^c	Required	$l_{s}\geqslant 2d$
C4	$l \geqslant 2,5d^{cd}$	_	<i>l</i> ≥ 2,5 <i>d</i> ^c	<i>l</i> ≥ 2,5 <i>d</i> ^c	Required	$l_s \geqslant 2d$
F1	$l \geqslant 2,5d^{cd}$	_	<i>l</i> ≥ 2,5 <i>d</i> ^C	<i>l</i> ≥ 2,5 <i>d</i> ^c	Required	_

a For all sizes ≥ M5.

b For sizes M1,6 \leq *d* < M5, the test applies to all lengths.

For studs, the requirement is $l \ge 3.5d$.

For l < 2,5d, testing shall be agreed on between the manufacturer and the purchaser.

7.2 Test methods

7.2.1 General

All length measurements shall be made with an accuracy of \pm 0,05 mm or better.

All tensile tests except under wedge loading (7.2.6) shall be performed with testing machines equipped with self-aligning grips in order to prevent any non-axial loading (see Figure 6). The lower adapter shall be hardened and threaded for tests according to 7.2.2, 7.2.3 and 7.2.4. The hardness of the lower adapter shall be 45 HRC minimum. Internal thread tolerance class shall be 5H6G.

7.2.2 Tensile strength, R_m

The tensile strength, $R_{\rm m}$, shall be determined on fasteners with $l \geqslant 2,5d$ in accordance with ISO 6892-1 and ISO 898-1.

A free threaded length at least equal to the nominal diameter shall be subject to the tensile load.

In order to meet the requirements of this test, the fracture shall occur in the free threaded length or in the unthreaded shank. The fracture shall not occur in the head.

For fasteners with unthreaded shanks, the fracture shall not occur in the transition section between the head and the shank.

For screws threaded to the head, the fracture which causes failure may extend or spread into the transition section between the head and the thread or into the head before separation, provided that it originates in the free threaded length.

The obtained value for $R_{\rm m}$ shall meet the values given in Tables 2 and 3.

7.2.3 Stress at 0,2 % permanent strain, $R_{p0.2}$

The stress at 0,2 % permanent strain, $R_{p0,2}$, shall be determined only on complete bolts and screws in the finished condition. This test is applicable only to fasteners with $l \ge 2,5d$.

The test shall be carried out by measuring the extension of the bolt or screw when subjected to axial tensile loading (see Figure 6).

The component under test shall be screwed into a hardened threaded adapter to a depth of one thread diameter, *d* (see Figure 6).

A curve of load against elongation shall be plotted as shown in Figure 7.

The clamping length from which $R_{p0,2}$ is calculated is taken as the distance between the underside of the head and the threaded adapter, L_3 (see Figure 6 and also footnote b of Tables 2 and 3). Of this value, 0,2 % is applied to scale to the horizontal (strain) axis of the load-elongation curve, OP, and the same value is plotted horizontally from the straight-line portion of the curve as QR. A line is drawn through P and R and the intersection, S, of this line with the load-elongation curve, corresponds to a load at point T on the vertical axis. This load, when divided by the thread stress area, gives the stress at 0,2 % permanent strain, $R_{p0,2}$.

The value of elongation is determined between the bearing face of the bolt head and the end of the adapter.

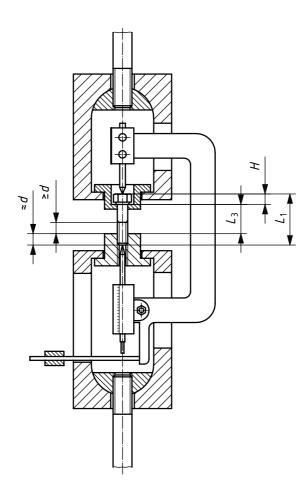
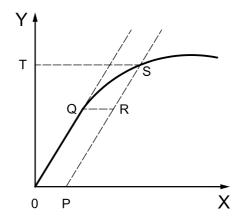


Figure 6 — Bolt extensiometer with self-aligning grips



Key

X elongation

Y load

Figure 7 — Load-elongation curve for determination of stress at 0,2 % permanent strain, $R_{\rm p0,2}$

7.2.4 Elongation after fracture, A

The elongation after fracture, A, shall be determined on fasteners with $l \ge 2.5d$.

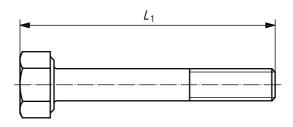
The total length of the fastener, L_1 , shall be measured (see Figure 8). The fastener shall be screwed into the threaded adapter to a depth of one nominal thread diameter, d (see Figure 6).

After the fastener has been fractured, the pieces shall be fitted together and the length, L_2 , measured again (see Figure 8).

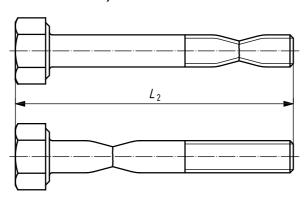
The elongation after fracture, A, is then calculated using Equation (1):

$$A = L_2 - L_1 \tag{1}$$

The obtained value for A shall not be less than the values given in Tables 2 and 3.



a) Before fracture



b) After fracture

Figure 8 — Determination of elongation after fracture, A

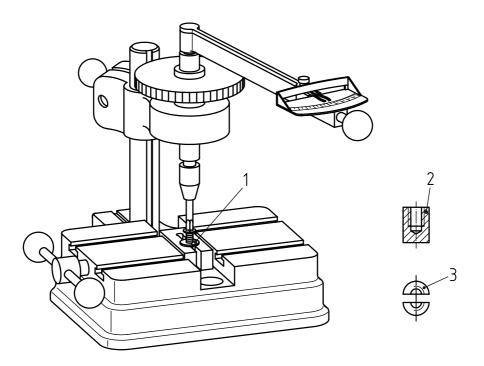
7.2.5 Breaking torque, M_{B}

The breaking torque, $M_{\rm B}$, shall be determined using an apparatus as shown in Figure 9. The torque-measuring device shall have an accuracy of within \pm 6 % of the minimum values being measured.

The thread of the screw shall be clamped in a mating split blind hole die for a length of one nominal thread diameter, exclusive of the point and so that at least two full threads project above the clamping device.

The torque shall be applied to the screw until failure occurs. The screw shall meet the minimum breaking torque requirements given in Table 4.





Key

- 1 split threaded die or threaded insert
- 2 threaded insert with a blind hole
- 3 split threaded die

Figure 9 — Apparatus for determination of the breaking torque, M_B

7.2.6 Test for strength under wedge loading of full size martensitic bolts and screws (not studs)

This test shall be performed in accordance with ISO 898-1 with wedge dimensions as given in Table 6.

Table 6 — Wedge dimensions

Naminal thread diameter	Wedge angle $lpha$								
Nominal thread diameter d mm	Bolts and screws with plain shank lengths	Bolts and screws threaded to the head or with plain shank lengths							
	$l_{s} \geqslant 2d$	$l_s < 2d$							
<i>d</i> ≤ 20	10° ± 30'	6° ± 30'							
20 < <i>d</i> ≤ 39	6° ± 30'	4° ± 30'							

7.2.7 Hardness HB, HRC or HV

On martensitic and ferritic fasteners, the hardness test shall be carried out in accordance with ISO 6506-1 (HB), ISO 6508-1 (HRC) or ISO 6507-1 (HV). In case of doubt, the Vickers hardness test is decisive for acceptance.

The hardness tests on bolts shall be made at the end of the bolt, mid-radius position between the centre and the circumference. For reference purposes, this zone shall be 1*d* from the end.

The hardness values shall be within the limits given in Table 3.

External thread - Calculation of stress area

The nominal stress area, $A_{s,nom}$, is calculated using Equation (A.1):

$$A_{s,nom} = \frac{\pi}{4} \left(\frac{d_2 + d_3}{2} \right)^2$$
 (A.1)

where

 d_2 is the basic pitch diameter of external thread (see ISO 724);

 d_3 is the minor diameter of the external thread (for stress calculation)

$$d_3 = d_1 - \frac{H}{6} \tag{A.2}$$

where

 d_1 is the basic minor diameter of external thread (see ISO 724);

H is the height of the fundamental triangle of the thread (see ISO 68-1).

Table A.1 — Nominal stress areas for coarse and fine pitch threads

Coarse pitch thread	Nominal stress area $A_{ m s, nom}$ ${ m mm}^2$
M1,6	1,27
M2	2,07
M2,5	3,39
M3	5,03
M4	8,78
M5	14,2
M6	20,1
M8	36,6
M10	58
M12	84,3
M14	115
M16	157
M18	192
M20	245
M22	303
M24	353
M27	459
M30	561
M33	694
M36	817
M39	976

Fine pitch thread	Nominal stress area $A_{ m s,\ nom}$
$d \times P$	mm ²
M8 × 1	39,2
M10 × 1	64,5
M10 × 1,25	61,2
$M12 \times 1,25$	92,1
$M12 \times 1,5$	88,1
$M14 \times 1,5$	125
M16 × 1,5	167
M18 × 1,5	216
M20 × 1,5	272
M22 × 1,5	333
M24 × 2	384
M27 × 2	496
M30 × 2	621
M33 × 2	761
M36 × 3	865
M39×3	1 030
	ters, there is an increasing

NOTE With small diameters, there is an increasing difference between the nominal stress area compared to the effective stress area.

BS EN ISO 3506-1:2009 ISO 3506-1:2009(E)

Annex B (informative)

Description of the groups and grades of stainless steels

B.1 General

In ISO 3506 (all parts), reference is made to steel grades A1 to A5, C1 to C4 and F1, covering steels of the following groups:

Austenitic steel A1 to A5;

Martensitic steel C1 to C4;

Ferritic steelF1.

The characteristics of the above-mentioned steel groups and steel grades are described in this annex.

This annex also gives some information on the non-standardized steel group FA. Steels of this group have a ferritic-austenitic structure.

B.2 Steel group A (austenitic structure)

B.2.1 General

Five main grades of austenitic steels, A1 to A5, are included in ISO 3506 (all parts). They cannot be hardened and are usually non-magnetic. In order to reduce the susceptibility to work hardening, copper may be added to the steel grades A1 to A5, as specified in Table 1.

For non-stabilized steel grades A2 and A4, the following applies.

 As chromic oxide makes steel resistant to corrosion, low carbon content is of great importance to non-stabilized steels. Due to the high affinity of chrome to carbon, chrome carbide is obtained instead of chromic oxide, which is more likely at elevated temperature (see Annex G).

For stabilized steel grades A3 and A5, the following applies.

— The elements Ti, Nb or Ta affect the carbon, and chromic oxide is produced to its full extent.

For offshore or similar applications, steels with Cr and Ni content of about 20 % and Mo of 4,5 % to 6,5 % are required.

When risk of corrosion is high, experts should be consulted.

B.2.2 Steel grade A1

Steels of grade A1 are specially designed for machining. Due to high sulfur content, the steels within this grade have lower resistance to corrosion than corresponding steels with normal sulfur content.

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B.2.3 Steel grade A2

Steels of grade A2 are the most frequently used stainless steels. They are used for kitchen equipment and apparatus for the chemical industry. Steels within this grade are not suitable for use in non-oxidizing acid and agents with chloride content, i.e. in swimming pools and sea water.

B.2.4 Steel grade A3

Steels of grade A3 are stabilized "stainless steels" with properties of steels of grade A2.

B.2.5 Steel grade A4

Steels of grade A4 are "acid proof steels", which are molybdenum alloyed and give a considerably better resistance to corrosion. A4 is used to a great extent by the cellulose industry, as this steel grade is developed for boiling sulfuric acid (hence the name "acid proof") and is, to a certain extent, also suitable in an environment with chloride content. A4 is also frequently used by the food industry and by the shipbuilding industry.

B.2.6 Steel grade A5

Steels of grade A5 are stabilized "acid proof steels" with properties of steels of grade A4.

B.3 Steel group F (ferritic structure)

B.3.1 General

One ferritic steel grade, F1, is included in ISO 3506 (all parts). The steels within F1 cannot normally be hardened and should not be hardened even if possible in certain cases. The F1 steels are magnetic.

B.3.2 Steel grade F1

Steels of grade F1 are normally used for simpler equipment with the exception of the superferrites, which have extremely low C and N contents. The steels within grade F1 can, if need be, replace steels of grades A2 and A3 and be used in an environment with a higher chloride content.

B.4 Steel group C (martensitic structure)

B.4.1 General

Three types of martensitic steel grades, C1, C3 and C4, are included in this part of ISO 3506. They can be hardened to an excellent strength and are magnetic.

B.4.2 Steel grade C1

Steels of grade C1 have limited resistance to corrosion. They are used in turbines, pumps and knives.

B.4.3 Steel grade C3

Steels of grade C3 have limited resistance to corrosion, though better resistance than C1. They are used in pumps and valves.

ISO 3506-1:2009(E)

B.4.4 Steel grade C4

Steels of grade C4 have limited resistance to corrosion. They are intended for machining, otherwise they are similar to steels of grade C1.

B.5 Steel group FA (ferritic-austenitic structure)

Steel group FA is not included in ISO 3506 (all parts), but will probably be included in a future edition.

Steels of this steel group are the so-called duplex steels. The FA steels first developed had several drawbacks which were eliminated in the steels developed later. FA steels have better properties than steels of grades A4 and A5, especially where strength is concerned. They also exhibit superior resistance to pitting and crack corrosion.

Examples of composition are given in Table B.1.

Table B.1 — Examples of composition of steels with ferritic-austenitic structure

Steel group			Ch	emical comp mass fraction			
	C max.	Si	Mn	Cr	Ni	Мо	N
Ferritic-austenitic	0,03	1,7	1,5	18,5	5	2,7	0,07
remiic-austemiic	0,03	< 1	< 2	22	5,5	3	0,14

Annex C (informative)

Stainless steel composition specifications

[Extract from ISO 683-13:1986²⁾]

²⁾ International Standard withdrawn.

Table C.1 — Stainless steel composition specifications

Steel grade	p		F1	Ŧ	F1	F1		C1	2	ნ	ខ	ဌ	C1		A2 ^h	A2	A3 ⁱ	A3i	A1	A2	A4	A4	A5 ⁱ	A5 ⁱ	A4	A4	A2	A4 ^h	A4 ^h
	Cn		1	1	1	1		1							l			1		١	1		١		١	1			
	Ι		I	$7\times\%~C\leqslant1,10$	_	_ t		Ι	1	I	1	1	l		Ι	I	$5\times\%~C\leqslant0,80$	I	l	_	-	I	$5\times\%~C\leqslant0,80$	l	-	1	1	I	I
	Se min.			I	-	1		I							I			l			-	I	١			1		I	1
	Z		1,0 max.	1,0 max.	1,0 max.	0,60 max.		1,0 max.	1,0 max.	1,0 max.	1,0 max.	1,5 to 2,5	1,0 max.		9,0 to 12,0	8,0 to 11,0	9,0 to 12,0	9,0 to 12,0	8,0 to 10,0 ^k	11,0 to 13,0	11,0 to 14,0	10,5 to 13,5	11,0 to 14,0	11,0 to 14,0	11,5 to 14,5	11,0 to 14,0	8,5 to 11,5	10,5 to 13,5	11,5 to 14,5
	Nb ^c		I	I	1	_f		-	1	I	ı	1	_		I	I	1	10 × % C ≤ 1,0	_	_	1	ı	I	$10\times\%~C\leqslant1,0$	-	_	ı	I	1
qu	Мо		I	I	0,90 to 1,30	1,75 to 2,50	ls	1	0,60 max. ⁹	I	0,60 max. ⁹	ı	I	s	I	I	ı	I	ij	-	2,0 to 2,5	2,0 to 2,5	2,0 to 2,5	2,0 to 2,5	2,5 to 3,0	2,5 to 3,0	I	2,0 to 2,5	2,5 to 3,0
Chemical composition ^b mass fraction, %	Cr	Ferritic steels	16,0 to 18,0	16,0 to 18,0	16,0 to 18,0	17,0 to 19,0	Martensitic steels	11,5 to 13,5	12,0 to 14,0	12,0 to 14,0	15,5 to 17,5	15,0 to 17,5	12,0 to 14,0	Austenitic steels	17,0 to 19,0	17,0 to 19,0	17,0 to 19,0	17,0 to 19,0	17,0 to 19,0	17,0 to 19,0	16,5 to 18,5	16,5 to 18,5	16,5 to 18,5	16,5 to 18,5	16,5 to 18,5	16,5 to 18,5	17,0 to 19,0	16,5 to 18,5	16,5 to 18,5
emic mas	₹	_	1	1	1	1	Ma	1						Ą	I			I		١	1	1	١		١	1	I	I	
Ö	z		I	I	Ι	0,025 max. ^e		1	I	I	I	I	I		I	I	I	I	I		Ι	I	I	I	I	Ι	0,12 to 0,22	0,12 to 0,22	0,12 to 0,22
	S		0,030 max.	0,030 max.	0,030 max.	0,030 max.		0,030 max.	0,15 to 0,35	0,030 max.	0,15 to 0,35	0,030 max.	0,030 max.		0,030 max.	0,030 max.	0,030 max.	0,030 max.	0,15 to 0,35	0,030 max.	0,030 max.	0,030 max.	0,030 max.	0,030 max.	0,030 max.	0,030 max.	0,030 max.	0,030 max.	0,030 max.
	P max.		0,040	0,040	0,040	0,040		0,040	090'0	0,040	090'0	0,040	0,040		0,045	0,045	0,045	0,045	0,060	0,045	0,045	0,045	0,045	0,045	0,045	0,045	0,045	0,045	0,045
	Mn max.		1,0	1,0	1,0	1,0		1,0	1,5	1,0	1,5	1,0	1,0		2,0	2,0	2,0	2,0	2,0	2,0	2,0	2,0	2,0	2,0	2,0	2,0	2,0	2,0	2,0
	Si max.		1,0	1,0	1,0	1,0		1,0	1,0	1,0	1,0	1,0	1,0		1,0	1,0	1,0	1,0	1,0	1,0	1,0	1,0	1,0	1,0	1,0	1,0	1,0	1,0	1,0
	С		0,08 max.	0,07 max.	0,08 max.	0,025 max. ^e		0,09 to 0,15	0,08 to 0,15	0,16 to 0,25	0,10 to 0,17	0,14 to 0,23	0,26 to 0,35		0,030 max.	0,07 max.	0,08 max.	0,08 max.	0,12 max.	0,10 max.	0,030 max.	0,07 max.	0,08 max.	0,08 max.	0,030 max.	0,07 max.	0,030 max.	0,030 max.	0,030 max.
Type ^a	steel		8	8b	၁6	F1		3	7	4	9a	q6	5		10	<u></u>	15	16	17	13	19	20	21	23	19a	20a	10N	19N	19aN

Table C.1 (continued)

b Elements not quoted shall not be intentionally added to the steel without the agreement of the purchaser, other than for the purpose of finishing the heat. All reasonable precautions shall be taken to prevent the addition, from scrap or other material used in manufacture, of such elements which affect the hardenability, mechanical properties and applicability. The type numbers are tentative and subject to alteration once the relevant International Standards are established

Tantalum determined as niobium.

This is not a part of ISO 683-13.

Maximum mass fraction (C + N) is 0,040 %.

Mass fraction $8 \times (C + N) \le \text{mass fraction (Nb + Ti)} \le 0.80 \%$.

Following agreement at the time of enquiry and order, the steel may be supplied with a mass fraction of Mo between 0,20 % and 0,60 %.

Description of the second o

Stabilized steels.

The manufacturer has the option of adding a mass fraction of Mo < 0,70 %.

The maximum mass fraction of Ni of semi-finished products for fabrication into seamless tubes may be increased by 0,5 %.

Annex D (informative)

Stainless steels for cold heading and extruding

(Extract from ISO 4954:1993)

21

Table D.1 — Stainless steels for cold heading and extruding

	Type of steel Designation ^a						ပ	Chemical composition ^b mass fraction, %	osition ^b , "			Steel grade
, N	Name	In accordance with	O	Si	Mn	ъ	S	ప	Mo	ïZ	Other	identification c
		ISO 4954:1979		3			3					
					ш	Ferritic steels	teels					
71	X3 Cr 17 E	I	< 0,04	1,00	1,00	0,040	0,030	16,0 to 18,0		< 1,0		F1
72	X 6 Cr 17 E	D 1	< 0,08	1,00	1,00	0,040	0,030	16,0 to 18,0		< 1,0		Т
73	X 6 CrMo 17 1 E	D 2	< 0,08	1,00	1,00	0,040	0,030	16,0 to 18,0	0,90 to 1,30	< 1,0		ЬТ
74	X 6 CrTi 12 E	l	< 0,08	1,00	1,00	0,040	0,030	10,5 to 12,5		< 0,50	Ti: 6 × % C ≤ 1,0	F1
75	X 6 CrNb 12 E	_	< 0,08	1,00	1,00	0,040	0,030	10,5 to 12,5		< 0,50	Nb: 6 × % C ≤ 1,0	F1
					Ма	Martensitic steels	steels					
9/	X 12 Cr 13 E	D 10	0,90 to 0,15	1,00	1,00	0,040	0,030	11,5 to 13,5		< 1,0		C1
77	X 19 CrNi 16 2 E	D 12	0,14 to 0,23	1,00	1,00	0,040	0,030	15,0 to 17,5		1,5 to 2,5		C3
					Au	Austenitic steels	steels					
78	X 2 CrNi 18 10 E	D 20	00'030	1,00	2,00	0,045	0,030	17,0 to 19,0		9,0 to 12,0		A2 ^d
79	X 5 CrNi 18 9 E	D 21	< 0,07	1,00	2,00	0,045	0,030	17,0 to 19,0		8,0 to 11,0		A2
8	X 10 CrNi 18 9 E	D 22	≤ 0,12	1,00	2,00	0,045	0,030	17,0 to 19,0		8,0 to 10,0		A2
8	X 5 CrNi 18 12 E	D 23	< 0,07	1,00	2,00	0,045	0,030	17,0 to 19,0		11,0 to 13,0		A2
82	X 6 CrNi 18 16 E	D 25	< 0,08	1,00	2,00	0,045	0,030	15,0 to 17,0		17,0 to 19,0		A2
83	X 6 CrNiTi 18 10 E	D 26	< 0,08	1,00	2,00	0,045	0,030	17,0 to 19,0		9,0 to 12,0	Ti: $5 \times \%$ C \leqslant 0,80	A3 ^e
8	X 5 CrNiMo 17 12 2 E	D 29	< 0,07	1,00	2,00	0,045	0,030	16,5 to 18,5	2,0 to 2,5	10,5 to 13,5		A4
82	X 6 CrNiMoTi 17 12 2 E	D 30	< 0,08	1,00	2,00	0,045	0,030	16,5 to 18,5	2,0 to 2,5	11,0 to 14,0	Ti: 5 × % C ≤ 0,80	A5e
86	X 2 CrNiMo 17 13 3 E	I	≤ 0,030	1,00	2,00	0,045	0,030	16,5 to 18,5	2,5 to 3,0	11,5 to 14,5		A4 ^d
87	X 2 CrNiMoN 17 13 3 E	l	< 0,030	1,00	2,00	0,045	0,030	16,5 to 18,5	2,5 to 3,0	11,5 to 14,5	N: 0,12 to 0,22	A4 ^d
88	X 3 CrNiCu 18 9 3 E	D 32	0,04	1,00	2,00	0,045	0,030	17,0 to 19,0		8,5 to 10,5	Cu: 3,00 to 4,00	A2

The designations given in the first column are consecutive numbers. The designations given in the second column are in accordance with the system proposed by ISO/TC 17/SC 2. The designations given in the third column represent the antiquated numbers of ISO 4954:1979 (revised by ISO 4954:1993).

b Elements not quoted in this table should not be intentionally added to the steel without the agreement of the purchaser, other than for finishing the heat. All reasonable precautions should be taken to prevent the addition, from scrap or other materials used in manufacture, of elements which affect mechanical properties and applicability.

This is not a part of ISO 4954.

Excellent resistance to intergranular corrosion.

Stabilized steels.

Annex E (informative)

Austenitic stainless steels with particular resistance to chloride induced stress corrosion

(Extract from EN 10088-1:2005)

The risk of failure of bolts, screws and studs by chloride induced stress corrosion (for example in indoor swimming pools) can be reduced by using the materials given in Table E.1.

Table E.1 — Austenitic stainless steels with particular resistance to chloride induced stress corrosion

Austenitic stainless steel					Ch	emical cor mass fract	•			
(Symbol/material number)	C max.	Si max.	Mn max.	P max.	S max.	N	Cr	Мо	Ni	Cu
X2CrNiMoN17-13-5 (1.4439)	0,030	1,00	2,00	0,045	0,015	0,12 to 0,22	16,5 to 18,5	4,0 to 5,0	12,5 to 14,5	
X1NiCrMoCu25-20-5 (1.4539)	0,020	0,70	2,00	0,030	0,010	≤ 0,15	19,0 to 21,0	4,0 to 5,0	24,0 to 26,0	1,20 to 2,00
X1NiCrMoCuN25-20-7 (1.4529)	0,020	0,50	1,00	0,030	0,010	0,15 to 0,25	19,0 to 21,0	6,0 to 7,0	24,0 to 26,0	0,50 to 1,50
X2CrNiMoN22-5-3 ^a (1.4462)	0,030	1,00	2,00	0,035	0,015	0,10 to 0,22	21,0 to 23,0	2,5 to 3,5	4,5 to 6,5	
a Ferritic-austenitic stainless steel.										

Annex F (informative)

Mechanical properties at elevated temperatures; application at low temperatures

NOTE If the bolts, screws or studs are properly calculated, the mating nuts automatically meet the requirements. Therefore, in the case of application at elevated or low temperatures, it is sufficient to consider the mechanical properties of bolts, screws and studs only.

F.1 Lower yield stress or stress at 0,2 % permanent strain at elevated temperatures

The values given in this annex are for guidance only. Users should understand that the actual chemistry, the loading of the installed fastener and the environment can cause significant variation. If loads are fluctuating and operating periods at elevated temperatures are great or the possibility of stress corrosion is high, the user should consult the manufacturer.

For values for lower yield stress, R_{eL} , and stress at 0,2 % permanent strain, $R_{p0,2}$, at elevated temperatures in % of the values at room temperature, see Table F.1.

Table F.1 — Influence of temperature on R_{eL} and $R_{p0.2}$

Steel grade	R _{eL} and R _{p0,2} % Temperature						
	+100 °C	+200 °C	+300 °C	+400 °C			
A2, A3, A4, A5	85	80	75	70			
C1	95	90	80	65			
C3	90	85	80	60			
NOTE This applies to property classes 70 and 80 only.							

F.2 Application at low temperatures

For application of stainless steel bolts, screws and studs at low temperatures, see Table F.2.

Table F.2 — Application of stainless steel bolts, screws and studs at low temperatures (austenitic steel only)

Steel grade	Lower limits of operational temp	perature at continuous operation	
A2, A3	-20	O °C	
A4. A5	bolts and screws ^a	−60 °C	
A4, A0	studs	−200 °C	

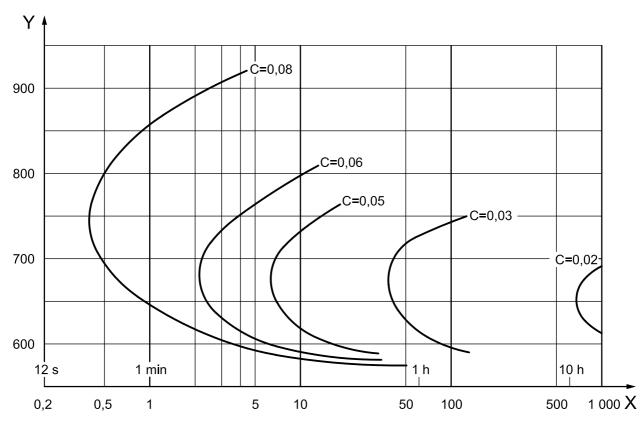
^a In connection with the alloying element Mo, the stability of the austenite is reduced and the transition temperature is shifted to higher values, if a high degree of deformation during the manufacture of the fastener is applied.

Annex G (informative)

Time-temperature diagram of intergranular corrosion in austenitic stainless steels, grade A2 (18/8 steels)

Figure G.1 gives the approximate time for austenitic stainless steels, grade A2 (18/8 steels), with different carbon contents in the temperature zone between 550 °C and 925 °C before risk of intergranular corrosion occurs.

NOTE With lower carbon contents, the resistance against intergranular corrosion is improved.



Key

- X time, expressed in minutes
- Y temperature, expressed in degrees Celsius

Figure G.1 — Time-temperature diagram of intergranular corrosion in austenitic stainless steels, grade A2

Annex H (informative)

Magnetic properties for austenitic stainless steels

Where specific magnetic properties are required, an experienced metallurgist should be consulted.

All austenitic stainless steel fasteners are normally non-magnetic; after cold working, it is possible for some magnetic properties to be evident.

Each material is characterized by its ability to be magnetized, which applies even to stainless steel. It is only possible for a vacuum to be entirely non-magnetic. The measure of the material's permeability in a magnetic field is the permeability value μ_{Γ} for that material in relation to a vacuum. The material has low permeability if μ_{Γ} becomes close to 1.

EXAMPLE 1 A2: $\mu_r \approx 1.8$

EXAMPLE 2 A4: $\mu_r \approx 1,015$

EXAMPLE 3 A4L: $\mu_r \approx 1,005$

EXAMPLE 4 F1: $\mu_r \approx 5$

ISO 3506-1:2009(E)

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³⁾ International Standard withdrawn.

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