



Standard Test Methods for Evaluating Primary Disposable Bag Integrity for Vacuum Cleaners¹

This standard is issued under the fixed designation F494; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon (ε) indicates an editorial change since the last revision or reapproval.

1. Scope

1.1 These test methods cover the evaluation of the integrity of the primary disposable bag used for vacuum cleaners.

1.2 The intent of these test methods is to verify that the design of the primary disposable bag will perform satisfactorily for the consumer in a wide range of normal use conditions. The filtering capability of the disposable bag is not evaluated with the use of these test methods.

1.3 The following tests are included:

Installation and Removal	Section 3
Workmanship	4
Durability	5
Seams and Joints	6

1.4 The values stated in inch-pound units are to be regarded as the standard. The values given in parentheses are for information only.

1.5 *This standard does not purport to address all of the safety problems, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use.*

2. Significance and Use

2.1 These test methods are useful for routine control, design of end-use products, and acceptance testing for conformance to specifications. Good workmanship, seams, and joints that remain strong over a wide range of atmospheric conditions and have the ability to withstand repeated cycles are necessary for satisfactory end use to the consumer.

TEST METHODS

3. Installation and Removal

3.1 *Scope*—These test methods provide guidelines for the installation and removal of the primary disposable bag.

¹ These test methods are under the jurisdiction of ASTM Committee F11 on Vacuum Cleaners and are the direct responsibility of Subcommittee F11.23 on Filtration.

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3.2 *Apparatus*—The vacuum cleaner model for which the primary disposable bag is intended.

3.3 *Test Specimens*—Test specimens shall be representative of the primary disposable bag system being tested.

3.4 *Procedure*—The primary disposable bag shall be installed in accordance with the instructions of the vacuum cleaner manufacturer.

3.4.1 Construction of the primary disposable bag shall be such that no holes or tears will be made when it is prepared for installation.

3.4.2 When installed or removed, in accordance with instructions, the primary disposable bag shall not be damaged or its function impaired.

3.5 *Report*—The report shall include any problems encountered during installation and removal of the primary disposable bag.

4. Workmanship

4.1 *Scope*—This test method provides a means of evaluating workmanship of the primary disposable bag.

4.2 *Test Specimens*—Test specimens shall be representative of the primary disposable bag system being tested.

4.3 *Procedure*—Inspect primary disposable bag for conformance to the following:

4.3.1 Complete sealing or fastening of all seams, tucks, joints, and attachments,

4.3.2 No tears, rips, holes, or other manufacturing type faults,

4.3.3 Printed instructions, when they appear, shall be clear and legible,

4.3.4 Dimensions shall agree with drawing specifications, or the primary disposable bag as defined by the vacuum cleaner manufacturer, and

4.3.5 If adhesives are used for seams and joints, there shall be no bleed through to adjacent plys or misplacements.

4.4 *Report*—The report shall include any defects in workmanship noted in the inspection in 4.3.

5. Durability

5.1 *Scope*—The durability of the primary disposable bag is determined by a life test within the vacuum cleaner for which the bag is intended.

5.2 Apparatus:

5.2.1 Vacuum Cleaner.

5.2.2 *Conditioning Chamber or Cabinet*, in which specimens may individually be exposed to circulating air and conditioning relative humidity and temperature within the limits specified in 5.5.

5.2.3 *Temperature-Measuring Equipment*, accurate to within $\pm 1^\circ\text{F}$ ($\pm 0.5^\circ\text{C}$).

5.2.4 *Humidity-Measuring Equipment*, accurate to within $\pm 2\%$ relative humidity.

5.2.5 *Solenoid*, to control the movement of a spring-loaded plate.

5.2.6 *Timer*, to control the activation of the solenoid on the basis of time.

5.2.7 *Plate*, to seal the intake of the test cleaner. This plate, connected directly to the solenoid shaft, must open sufficiently so as not to restrict air flow and must open and close the intake within 0.1 s. Motion of the plate must not be a sliding action.

5.2.7.1 *Canister Cleaners*—The plate seals the nozzle end of the hose normally supplied with the vacuum cleaner. The hose is attached to the vacuum cleaner in the normal manner with no attempts to seal leaks.

5.2.7.2 *Upright Cleaners*—The plate seals a 1.75 ± 0.02 -in. (44.5 ± 0.5 -mm) diameter hole located in an adapter cover. The adapter cover closes off the nozzle intake opening of the cleaner without interfering with the rotating agitator.

5.2.8 *Voltage Regulator*—The regulator shall be capable of maintaining 120 ± 1 V rms 60 Hz with a wave form that is essentially sinusoidal with 3 % maximum harmonic distortion for the duration of the test.

5.2.9 *Voltmeter*, to measure input to the cleaner and provide measurements accurate to within $\pm 1\%$.

5.3 *Test Specimens*—Test specimens shall be representative of the primary disposable bag being tested.

5.4 *Material*—Coarse grade air cleaner test dust.

NOTE 1—The particle size distribution by volume of the test dust is given in Table 1.

TABLE 1 Analysis of Coarse Grade Air Cleaner F11 Test Dust^{A, B}

Particle Size Distribution by Volume	
Size, μm	Coarse Grade (% less than)
5.5	13 ± 3
11	24 ± 3
22	37 ± 3
44	56 ± 3
88	84 ± 3
176	100

^A The information in Table 1 is contained in “Air Cleaner Test Code,” SAE Technical Report J726b.

^B The sole source of supply of the test dust known to the committee at this time is Powder Technology, Inc., 1119 Riverwood Drive, Burnsville, MN 55337. If you are aware of alternative suppliers, please provide this information to ASTM International Headquarters. Your comments will receive careful consideration at a meeting of the responsible technical committee,¹ which you may attend.

5.5 *Conditioning*—Allow test specimens to age at ambient conditions of 68 to 81°F (20 to 27°C) and 45 to 55 % relative humidity for a minimum of 24 h before starting tests.

5.6 Procedure:

5.6.1 Perform all tests on the vacuum cleaner in a controlled ambient with a dry-bulb temperature of 68 to 81°F (20 to 27°C) and 30 to 55 % relative humidity.

5.6.2 Measure and calculate the total primary disposable bag area excluding seams, joints, treated seal area, mounting means, and multiple thickness of media. Measure multiple thicknesses that are intended for a specific filtering purpose as a single ply.

5.6.3 Prepare 0.0023 oz of coarse grade air cleaner test dust per square inch of primary disposable bag area (0.010 g/cm^2).

5.6.4 Close vacuum bleed control and seal all openings normally closed off with operation of tools.

5.6.5 Install the primary disposable bag in the intended manner in the vacuum cleaner for which it was designed. Energize the cleaner and adjust the voltage regulator to rated voltage ± 1 V.

5.6.5.1 Operate the cleaner at the maximum speed setting provided for the carpet cleaning mode.

5.6.6 Feed the amount of test dust specified in 5.6.3 at the rate of 0.7 ± 0.07 oz (20 ± 2 g)/min into the intake port.

5.6.7 After loading and with the cleaner operating at rated voltage, subject the cleaner to a test of 7.5 s open and 7.5 s closed for a period of 12 h.

5.6.7.1 For the canister cleaner, alternately open and close the nozzle end of the hose with the plate described in 5.2.7, while the cleaner remains running. For an upright cleaner, alternately open and close the intake hole as described in 5.2.7.2, while the cleaner remains running.

5.7 *Report*—The report shall include any failure of the primary disposable bag.

5.7.1 Any rupture of the primary disposable bag material or separation of seams, tucks, joints, or attachments shall constitute a failure. Pinhole leaks are not considered to be ruptures.

6. Seams and Joints

6.1 *Scope*—The evaluation of seams, tucks, joints, and attachments used to fabricate the primary disposable bag is accomplished by means of temperature and humidity cycling followed by visual inspection and durability tests.

6.2 Apparatus:

6.2.1 *Conditioning Chamber or Cabinet*, in which specimens may individually be exposed to circulating air and conditioning relative humidity and temperature within the limits specified in 6.4.

6.2.2 *Oven*, with forced ventilation, that will maintain $156 \pm 2^\circ\text{F}$ ($68.9 \pm 1.1^\circ\text{C}$) at the test conditions where the specimens are located and shielded from direct radiation from the heating element.

6.2.3 *Cold Box*, that will maintain specimens at $-20 \pm 2^\circ\text{F}$ ($-28.9 \pm 1.1^\circ\text{C}$) at the test conditions.

6.2.4 *Temperature-Measuring Equipment*, accurate to within $\pm 1^\circ\text{F}$ ($\pm 0.5^\circ\text{C}$).

6.2.5 *Humidity-Measuring Equipment*, accurate to within $\pm 2\%$ relative humidity.

6.3 *Test Specimens*—Test specimens shall be representative of the primary disposable bag being tested. Use fresh samples for each of the tests in 6.5.1 and 6.5.2, and 6.5.3.

6.4 *Conditioning*—Age all test specimens at least 24 h at ambient conditions of 68 to 81°F (20 to 27°C) and 30 to 55 % relative humidity to prepare them for the hot, cold, and humidity test cycles.

6.4.1 Simultaneously condition specimens for the hot, cold, and humidity test cycles.

6.5 *Procedure*:

6.5.1 *Hot Test Cycle*:

6.5.1.1 Place the test specimens in an oven at $156 \pm 2^\circ\text{F}$ ($68.9 \pm 1.1^\circ\text{C}$) for 4 weeks.

6.5.1.2 Allow test specimens to condition at ambient conditions of 68 to 81°F (20 to 27°C) and 30 to 55 % relative humidity for 30 min minimum after removal from oven.

6.5.1.3 Examine the specimens visually for any obvious failure and subject each of the test specimens to a durability evaluation similar to that in Section 5. For this test, the operating period in 5.6.7 shall be 5 min instead of 12 h.

6.5.2 *Cold Test Cycle*:

6.5.2.1 Place test specimens in a cold box for 24 h at $-20 \pm 2^\circ\text{F}$ ($-28.9 \pm 1.1^\circ\text{C}$).

6.5.2.2 Condition at ambient conditions of 68 to 81°F (20 to 27°C) and 30 to 55 % relative humidity for 30 min minimum after removal from cold box.

6.5.2.3 Repeat the cycle (6.5.2.1 and 6.5.2.2) three times.

6.5.2.4 Examine the specimens visually for any obvious bond failures. If there is no obvious failure, subject each of the test specimens to a durability evaluation similar to that in Section 5. For this test, the operating period in 5.6.7 shall be 5 min instead of 12 h.

6.5.3 *Humidity Test Cycle*:

6.5.3.1 Place test specimens in the conditioning chamber at $89.6 \pm 3.6^\circ\text{F}$ ($32 \pm 2^\circ\text{C}$) and 86 to 90 % relative humidity for 24 h.

6.5.3.2 After removing the test specimens from the conditioning chamber, condition them for 4 h minimum at 68 to 81°F (20 to 27°C) and 30 to 55 % relative humidity.

6.5.3.3 Repeat the cycle (6.5.3.1 and 6.5.3.2) three times.

6.5.3.4 Examine the specimens visually for any obvious bond failures. If there is no obvious failure, subject each of the test specimens to a durability evaluation similar to that in Section 5. For this test, the operating period in 5.6.7 shall be 5 min instead of 12 h.

6.6 *Report*—The report for each of the tests in 6.5 shall include any failure of the primary disposable bag.

6.6.1 Any rupture of the primary disposable bag material or separation of seams, tucks, joints, or attachments shall constitute a failure. Pinhole leaks are not considered to be ruptures.

7. Sampling

7.1 A sample of sufficient size for each primary disposable bag shall be tested until a 90 % confidence interval for the true percent defective is established.

7.2 The minimum number of tests required is defined to be that number which will give a 90 % confidence interval for the true percent defective that is less than 0.20 in width (see Annex A1).

8. Precision and Bias

8.1 Precision and bias do not apply for this test method since this is a procedure for a test that is conducted to a specified end point.

9. Keywords

9.1 vacuum cleaner disposable bag integrity

ANNEX

(Mandatory Information)

A1. DETERMINATION OF 90 % CONFIDENCE INTERVAL (PROPORTION)

A1.1 The most common and ordinarily the best single estimate (p) of the true proportion (or percentage) (P) of items that have a given quality characteristic is simply the number of items (r) that possess this characteristic divided by the total number of items (n).

$$p = r/n \quad (\text{A1.1})$$

When a sample is taken from a population, the sample proportion that possesses the characteristic will seldom be exactly the same proportion as the population. It is hoped to be fairly close so that a statement of the confidence interval will bracket the true proportion.

A1.2 *Glossary of Additional Terms*:

α = probability of being wrong,
 $1 - \alpha$ = probability of being correct,
 P_u = upper limit of the confidence interval for P ,
 P_l = lower limit of the confidence interval for P , and
 A = chosen limit for the width of the confidence interval (in accordance with 7.2, $A = 0.20$).

A1.3 The following procedure gives an interval which is expected to bracket (P), the true proportion, 100 ($1 - \alpha$) % of the time:

A1.3.1 Choose the desired confidence level, $1 - \alpha$.

A1.3.2 Compute $p = r/n$.

A1.3.3 If $n \geq 30$, use Table A1.1.

TABLE A1.1 Confidence Limits for a Proportion (Two-Sided)^A

NOTE 1—Upper limits are in boldface. The observed proportion in a random sample is r/n .

r	90 %	95 %	99 %	r	90 %	95 %	99 %
$n = 1$				$n = 2$			
0	0	0.900	0	0.950	0	0.990	0
1	0.100	1	0.050	1	0.010	1	0
$n = 3$				$n = 4$			
0	0	0.536	0	0.632	0	0.785-	0
1	0.035-	0.804	0.017	0.865-	0.003	0.941	0
2	0.196	0.965 +	0.135 +	0.983	0.059	0.997	0
3	0.464	1	0.368	1	0.215 +	1	0
$n = 5$				$n = 6$			
0	0	0.379	0	0.500	0	0.602	0
1	0.021	0.621	0.010	0.657	0.002	0.778	0
2	0.112	0.753	0.076	0.811	0.033	0.894	0
3	0.247	0.888	0.189	0.924	0.106	0.967	0
4	0.379	0.979	0.343	0.990	0.222	0.998	0
5	0.621	1	0.500	1	0.398	1	0
$n = 7$				$n = 8$			
0	0	0.316	0	0.377	0	0.500	0
1	0.015-	0.500	0.007	0.554	0.001	0.643	0
2	0.079	0.684	0.053	0.659	0.023	0.764	0
3	0.170	0.721	0.129	0.775-	0.071	0.858	0
4	0.279	0.830	0.225 +	0.871	0.142	0.929	0
5	0.316	0.921	0.341	0.947	0.236	0.977	0
6	0.500	0.985 +	0.446	0.993	0.357	0.999	0
7	0.684	1	0.623	1	0.500	1	0
$n = 9$				$n = 10$			
0	0	0.232	0	0.289	0	0.402	0
1	0.012	0.391	0.006	0.443	0.001	0.598	0
2	0.061	0.515 +	0.041	0.558	0.017	0.656	0
3	0.129	0.610	0.098	0.711	0.053	0.750	0
4	0.210	0.768	0.169	0.749	0.105 +	0.829	0
5	0.232	0.790	0.251	0.831	0.171	0.895-	0
6	0.390	0.871	0.289	0.902	0.250	0.947	0
7	0.485-	0.939	0.442	0.959	0.344	0.983	0
8	0.609	0.988	0.557	0.994	0.402	0.999	0
9	0.768	1	0.711	1	0.598	1	0
$n = 11$				$n = 12$			
0	0	0.197	0	0.250	0	0.359	0
1	0.010	0.315 +	0.005-	0.369	0.001	0.500	0
2	0.049	0.423	0.033	0.500	0.014	0.593	0
3	0.105-	0.577	0.079	0.631	0.043	0.660	0
4	0.169	0.685-	0.135 +	0.667	0.084	0.738	0
5	0.197	0.698	0.200	0.750	0.134	0.806	0
6	0.302	0.803	0.250	0.800	0.194	0.866	0
7	0.315 +	0.831	0.333	0.865-	0.262	0.916	0
8	0.423	0.895 +	0.369	0.921	0.340	0.957	0
9	0.577	0.951	0.500	0.967	0.407	0.986	0
10	0.685-	0.990	0.631	0.995 +	0.500	0.999	0
11	0.803	1	0.750	1	0.641	1	0
$n = 13$				$n = 14$			
0	0	0.173	0	0.225 +	0	0.302	0
1	0.008	0.276	0.004	0.327	0.001	0.429	0
2	0.042	0.379	0.028	0.434	0.012	0.523	0
3	0.088	0.470	0.066	0.520	0.036	0.594	0
4	0.142	0.545-	0.113	0.587	0.069	0.698	0
5	0.173	0.621	0.166	0.673	0.111	0.727	0
6	0.246	0.724	0.224	0.740	0.159	0.787	0
7	0.276	0.754	0.260	0.776	0.213	0.841	0

TABLE A1.1 *Continued*

<i>r</i>	90 %	95 %	99 %	<i>r</i>	90 %	95 %	99 %						
8	0.379	0.827	0.327	0.834	0.273	0.889	0.312	0.794	0.249	0.854			
9	0.455 +	0.858	0.413	0.887	0.302	0.931	0.371	0.847	0.286	0.898			
10	0.530	0.912	0.480	0.934	0.406	0.964	0.422	0.869	0.389	0.896			
11	0.621	0.958	0.566	0.972	0.477	0.988	0.500	0.939	0.392	0.967			
12	0.724	0.992	0.673	0.996	0.571	0.999	0.611	0.974	0.500	0.989			
13	0.827	1	0.775-	1	0.698	1	0.739	0.993	0.688	0.996			
14					0.837	1	0.793	1	0.714	1			
<i>n</i> = 15							<i>n</i> = 16						
0	0	0.154	0	0.191	0	0.273	0	0.147	0	0.179	0	0.264	
1	0.007	0.247	0.003	0.302	0.001	0.373	0.007	0.235 +	0.003	0.273	0.001	0.357	
2	0.036	0.326	0.024	0.369	0.010	0.461	0.034	0.305 +	0.023	0.352	0.010	0.451	
3	0.076	0.400	0.057	0.448	0.031	0.539	0.071	0.381	0.053	0.429	0.029	0.525-	
4	0.122	0.500	0.097	0.552	0.059	0.627	0.114	0.450	0.090	0.500	0.055 +	0.579	
5	0.154	0.600	0.142	0.631	0.094	0.672	0.147	0.550	0.132	0.571	0.088	0.643	
6	0.205 +	0.674	0.191	0.668	0.135-	0.727	0.189	0.619	0.178	0.648	0.125 +	0.705-	
7	0.247	0.675-	0.192	0.706	0.179	0.771	0.235 +	0.695-	0.179	0.727	0.166	0.739	
8	0.325 +	0.753	0.294	0.808	0.229	0.821	0.299	0.701	0.272	0.728	0.212	0.788	
9	0.326	0.795-	0.332	0.809	0.273	0.865 +	0.305 +	0.765-	0.273	0.821	0.261	0.834	
10	0.400	0.846	0.369	0.858	0.328	0.906	0.381	0.811	0.352	0.822	0.295 +	0.875-	
11	0.500	0.878	0.448	0.903	0.373	0.941	0.450	0.853	0.429	0.868	0.357	0.912	
12	0.600	0.924	0.552	0.943	0.461	0.969	0.550	0.886	0.500	0.910	0.421	0.945-	
13	0.674	0.964	0.631	0.976	0.539	0.990	0.619	0.929	0.571	0.947	0.475 +	0.971	
14	0.753	0.993	0.698	0.997	0.627	0.999	0.695-	0.966	0.648	0.977	0.549	0.990	
15	0.846	1	0.809	1	0.727	1	0.765-	0.993	0.727	0.997	0.643	0.999	
16					0.853	1	0.821	1	0.736	1			
<i>n</i> = 17							<i>n</i> = 18						
0	0	0.140	0	0.167	0	0.243	0	0.135-	0	0.157	0	0.228	
1	0.006	0.225 +	0.003	0.254	0.001	0.346	0.006	0.216	0.003	0.242	0.001	0.318	
2	0.032	0.290	0.021	0.337	0.009	0.413	0.030	0.277	0.020	0.325-	0.008	0.397	
3	0.067	0.364	0.050	0.417	0.027	0.500	0.063	0.349	0.047	0.381	0.025 +	0.466	
4	0.107	0.432	0.085-	0.489	0.052	0.587	0.101	0.419	0.080	0.444	0.049	0.534	
5	0.140	0.500	0.124	0.544	0.082	0.620	0.135-	0.482	0.116	0.556	0.077	0.603	
6	0.175 +	0.568	0.166	0.594	0.117	0.662	0.163	0.536	0.156	0.619	0.110	0.682	
7	0.225 +	0.636	0.167	0.663	0.155 +	0.757	0.216	0.584	0.157	0.625 +	0.145 +	0.686	
8	0.277	0.710	0.253	0.746	0.197	0.758	0.257	0.651	0.236	0.675 +	0.184	0.772	
9	0.290	0.723	0.254	0.747	0.242	0.803	0.277	0.723	0.242	0.758	0.226	0.774	
10	0.364	0.775-	0.337	0.833	0.243	0.845	0.349	0.743	0.325-	0.764	0.228	0.816	
11	0.432	0.825-	0.406	0.834	0.338	0.883	0.416	0.784	0.375-	0.843	0.314	0.855-	
12	0.500	0.860	0.456	0.876	0.380	0.918	0.464	0.837	0.381	0.844	0.318	0.890	
13	0.568	0.893	0.511	0.915 +	0.413	0.948	0.518	0.865 +	0.444	0.884	0.397	0.923	
14	0.636	0.933	0.583	0.950	0.500	0.973	0.581	0.899	0.556	0.920	0.466	0.951	
15	0.710	0.968	0.663	0.979	0.587	0.991	0.651	0.937	0.619	0.953	0.534	0.975-	
16	0.775-	0.994	0.746	0.997	0.654	0.999	0.723	0.970	0.675 +	0.980	0.603	0.992	
17	0.860	1	0.833	1	0.757	1	0.784	0.994	0.758	0.997	0.682	0.999	
18							0.865 +	1	0.843	1			
<i>n</i> = 19							<i>n</i> = 20						
0	0	0.130	0	0.150	0	0.218	0	0.126	0	0.143	0	0.209	
1	0.006	0.209	0.003	0.232	0.001	0.305 +	0.005 +	0.203	0.003	0.222	0.001	0.293	
2	0.028	0.265 +	0.019	0.316	0.008	0.383	0.027	0.255-	0.018	0.294	0.008	0.375-	
3	0.059	0.337	0.044	0.365-	0.024	0.455 +	0.056	0.328	0.042	0.351	0.023	0.424	
4	0.095 +	0.387	0.075 +	0.426	0.046	0.515 +	0.090	0.367	0.071	0.411	0.044	0.500	
5	0.130	0.440	0.110	0.500	0.073	0.564	0.126	0.422	0.104	0.467	0.069	0.576	
6	0.151	0.560	0.147	0.574	0.103	0.617	0.141	0.500	0.140	0.533	0.098	0.601	
7	0.209	0.613	0.150	0.635 +	0.137	0.695-	0.201	0.578	0.143	0.589	0.129	0.637	
8	0.238	0.614	0.222	0.655 +	0.173	0.707	0.221	0.633	0.209	0.649	0.163	0.707	
9	0.265 +	0.663	0.232	0.688	0.212	0.782	0.255-	0.642	0.222	0.706	0.200	0.726	
10	0.337	0.735-	0.312	0.768	0.218	0.788	0.325	0.675 +	0.293	0.707	0.209	0.791	
11	0.386	0.762	0.345-	0.778	0.293	0.827	0.358	0.745 +	0.294	0.778	0.274	0.800	
12	0.387	0.791	0.365-	0.850	0.305 +	0.863	0.367	0.779	0.351	0.791	0.293	0.837	
13	0.440	0.849	0.426	0.853	0.383	0.897	0.422	0.799	0.411	0.857	0.363	0.871	
14	0.560	0.870	0.500	0.890	0.436	0.927	0.500	0.859	0.467	0.860	0.399	0.902	
15	0.613	0.905-	0.574	0.925-	0.485-	0.954	0.578	0.874	0.533	0.896	0.424	0.931	
16	0.663	0.941	0.635 +	0.956	0.545-	0.976	0.633	0.910	0.589	0.929	0.500	0.956	
17	0.735-	0.972	0.684	0.981	0.617	0.992	0.672	0.944	0.649	0.958	0.576	0.977	
18	0.791	0.994	0.768	0.997	0.695-	0.999	0.745 +	0.973	0.706	0.982	0.625 +	0.992	
19	0.870	1	0.850	1	0.782	1	0.797	0.995-	0.778	0.997	0.707	0.999	

TABLE A1.1 *Continued*

<i>r</i>	90 %	95 %	99 %	<i>r</i>	90 %	95 %	99 %
<i>n</i> = 21				<i>n</i> = 22			
0	0	0.123	0	0	0	0.116	0
1	0.005 +	0.192	0.002	1	0.005-	0.182	0.002
2	0.026	0.245-	0.017	2	0.024	0.236	0.016
3	0.054	0.307	0.040	3	0.051	0.289	0.038
4	0.086	0.353	0.068	4	0.082	0.340	0.065-
5	0.121	0.407	0.099	5	0.115-	0.393	0.094
6	0.130	0.458	0.132	6	0.116	0.444	0.126
7	0.191	0.542	0.137	7	0.181	0.500	0.132
8	0.192	0.593	0.197	8	0.182	0.556	0.187
9	0.245-	0.647	0.213	9	0.236	0.607	0.205 +
10	0.306	0.693	0.276	10	0.289	0.660	0.260
11	0.307	0.694	0.277	11	0.290	0.710	0.264
12	0.353	0.755 +	0.338	12	0.340	0.711	0.326
13	0.407	0.808	0.398	13	0.393	0.764	0.383
14	0.458	0.809	0.449	14	0.444	0.818	0.418
15	0.542	0.870	0.494	15	0.500	0.819	0.424
16	0.593	0.879	0.545-	16	0.556	0.884	0.500
17	0.647	0.914	0.602	17	0.607	0.885 +	0.576
18	0.693	0.946	0.662	18	0.660	0.918	0.611
19	0.755 +	0.974	0.723	19	0.711	0.949	0.674
20	0.808	0.995-	0.787	20	0.764	0.976	0.736
21	0.877	1	0.863	21	0.818	0.995 +	0.795-
				22	0.884	1	0.868
<i>n</i> = 23				<i>n</i> = 24			
0	0	0.111	0	0	0	0.105 +	0
1	0.005-	0.174	0.002	1	0.004	0.165 +	0.002
2	0.023	0.228	0.016	2	0.022	0.221	0.015 +
3	0.049	0.274	0.037	3	0.047	0.264	0.035-
4	0.078	0.328	0.062	4	0.075-	0.317	0.059
5	0.110	0.381	0.090	5	0.105-	0.370	0.086
6	0.111	0.431	0.120	6	0.105 +	0.423	0.115-
7	0.173	0.479	0.127	7	0.165-	0.448	0.122
8	0.174	0.522	0.178	8	0.165 +	0.552	0.169
9	0.228	0.569	0.198	9	0.221	0.553	0.191
10	0.273	0.619	0.247	10	0.259	0.587	0.234
11	0.274	0.672	0.255-	11	0.264	0.630	0.246
12	0.328	0.726	0.317	12	0.317	0.683	0.308
13	0.381	0.727	0.360	13	0.370	0.736	0.339
14	0.431	0.772	0.361	14	0.413	0.741	0.347
15	0.478	0.826	0.409	15	0.447	0.779	0.396
16	0.521	0.827	0.457	16	0.448	0.835-	0.443
17	0.569	0.889	0.543	17	0.552	0.835 +	0.500
18	0.619	0.890	0.591	18	0.577	0.895-	0.557
19	0.672	0.922	0.639	19	0.630	0.895 +	0.604
20	0.726	0.951	0.683	20	0.683	0.925 +	0.653
21	0.772	0.977	0.745 +	21	0.736	0.953	0.692
22	0.826	0.995 +	0.802	22	0.779	0.978	0.754
23	0.889	1	0.873	23	0.835-	0.996	0.809
				24	0.895-	1	0.878
<i>n</i> = 25				<i>n</i> = 26			
0	0	0.102	0	0	0	0.098	0
1	0.004	0.159	0.002	1	0.004	0.152	0.002
2	0.021	0.214	0.014	2	0.021	0.209	0.014
3	0.045-	0.255-	0.034	3	0.043	0.247	0.032
4	0.072	0.307	0.057	4	0.069	0.299	0.054
5	0.101	0.362	0.082	5	0.097	0.343	0.079
6	0.102	0.390	0.110	6	0.098	0.377	0.106
7	0.158	0.432	0.118	7	0.151	0.419	0.114
8	0.159	0.500	0.161	8	0.152	0.460	0.154
9	0.214	0.568	0.185 +	9	0.209	0.540	0.180
10	0.246	0.610	0.222	10	0.233	0.581	0.212
11	0.255-	0.611	0.238	11	0.247	0.623	0.230
12	0.307	0.640	0.296	12	0.299	0.657	0.282

TABLE A1.1 *Continued*

<i>r</i>	90 %		95 %		99 %		<i>r</i>	90 %		95 %		99 %	
13	0.360	0.693	0.317	0.704	0.246	0.755-	13	0.342	0.658	0.283	0.717	0.235-	0.765 +
14	0.389	0.745 +	0.336	0.762	0.305-	0.795-	14	0.343	0.701	0.325 +	0.718	0.298	0.766
15	0.390	0.754	0.384	0.778	0.342	0.825-	15	0.377	0.753	0.374	0.770	0.322	0.805 +
16	0.432	0.786	0.431	0.815-	0.352	0.845-	16	0.419	0.767	0.421	0.788	0.342	0.830
17	0.500	0.841	0.475-	0.839	0.403	0.873	17	0.460	0.791	0.458	0.820	0.393	0.851
18	0.568	0.842	0.525 +	0.882	0.451	0.899	18	0.540	0.848	0.494	0.846	0.438	0.878
19	0.610	0.898	0.569	0.890	0.500	0.923	19	0.581	0.849	0.535-	0.886	0.474	0.903
20	0.638	0.899	0.616	0.918	0.549	0.946	20	0.623	0.902	0.579	0.894	0.513	0.927
21	0.693	0.928	0.664	0.943	0.597	0.966	21	0.657	0.903	0.626	0.921	0.558	0.948
22	0.745 +	0.955 +	0.697	0.966	0.648	0.982	22	0.701	0.931	0.675-	0.946	0.607	0.967
23	0.786	0.979	0.762	0.986	0.695 +	0.994	23	0.753	0.957	0.717	0.968	0.658	0.983
24	0.841	0.996	0.815-	0.998	0.754	1.000	24	0.791	0.979	0.770	0.986	0.702	0.994
25	0.898	1	0.882	1	0.825-	1	25	0.848	0.996	0.820	0.998	0.765 +	1.000
26							26	0.902	1	0.886	1	0.830	1
<i>n</i> = 27							<i>n</i> = 28						
0	0	0.093	0	0.110	0	0.166	0	0	0.090	0	0.106	0	0.162
1	0.004	0.146	0.002	0.175-	0.000	0.225-	1	0.004	0.140	0.002	0.170	0.000	0.218
2	0.020	0.204	0.013	0.223	0.006	0.297	2	0.019	0.201	0.013	0.217	0.005 +	0.273
3	0.042	0.239	0.031	0.270	0.017	0.332	3	0.040	0.232	0.030	0.259	0.016	0.323
4	0.066	0.291	0.052	0.316	0.032	0.384	4	0.064	0.284	0.050	0.307	0.031	0.365-
5	0.093	0.327	0.076	0.364	0.050	0.419	5	0.089	0.312	0.073	0.357	0.048	0.408
6	0.094	0.365 +	0.101	0.415-	0.070	0.461	6	0.090	0.355-	0.098	0.384	0.068	0.449
7	0.145 +	0.407	0.110	0.437	0.093	0.539	7	0.139	0.396	0.106	0.424	0.089	0.500
8	0.146	0.447	0.148	0.500	0.117	0.581	8	0.140	0.435 +	0.142	0.463	0.112	0.551
9	0.204	0.500	0.175-	0.563	0.143	0.587	9	0.197	0.473	0.170	0.537	0.137	0.592
10	0.221	0.553	0.202	0.570	0.166	0.617	10	0.208	0.527	0.192	0.576	0.162	0.635 +
11	0.239	0.593	0.223	0.598	0.185-	0.668	11	0.232	0.565-	0.217	0.616	0.175 +	0.636
12	0.291	0.635-	0.269	0.636	0.224	0.702	12	0.284	0.604	0.258	0.619	0.214	0.677
13	0.326	0.673	0.270	0.684	0.225-	0.716	13	0.310	0.645 +	0.259	0.645 +	0.218	0.727
14	0.327	0.674	0.316	0.730	0.284	0.775 +	14	0.312	0.688	0.307	0.693	0.272	0.728
15	0.365 +	0.709	0.364	0.731	0.298	0.776	15	0.355-	0.690	0.355-	0.741	0.273	0.782
16	0.407	0.761	0.402	0.777	0.332	0.815-	16	0.396	0.716	0.381	0.742	0.323	0.786
17	0.447	0.779	0.430	0.798	0.383	0.834	17	0.435 +	0.768	0.384	0.783	0.364	0.825-
18	0.500	0.796	0.437	0.825 +	0.413	0.857	18	0.473	0.792	0.424	0.808	0.365-	0.838
19	0.553	0.854	0.500	0.852	0.419	0.883	19	0.527	0.803	0.463	0.830	0.408	0.863
20	0.593	0.855-	0.563	0.890	0.461	0.907	20	0.565-	0.860	0.537	0.858	0.449	0.888
21	0.635-	0.906	0.585 +	0.899	0.539	0.930	21	0.604	0.861	0.576	0.894	0.500	0.911
22	0.673	0.907	0.636	0.924	0.581	0.950	22	0.645 +	0.910	0.616	0.902	0.551	0.932
23	0.709	0.934	0.684	0.948	0.616	0.968	23	0.688	0.911	0.643	0.927	0.592	0.952
24	0.761	0.958	0.730	0.969	0.668	0.983	24	0.716	0.936	0.693	0.950	0.635 +	0.969
25	0.796	0.980	0.777	0.987	0.703	0.994	25	0.768	0.960	0.741	0.970	0.677	0.984
26	0.854	0.996	0.825 +	0.998	0.775 +	1.000	26	0.799	0.981	0.783	0.987	0.727	0.995-
27	0.907	1	0.890	1	0.0834	1	27	0.860	0.996	0.830	0.998	0.782	1.000
28							28	0.910	1	0.894	1	0.838	1
<i>n</i> = 29							<i>n</i> = 30						
0	0	0.087	0	0.103	0	0.160	0	0	0.084	0	0.100	0	0.152
1	0.004	0.135-	0.002	0.166	0.000	0.211	1	0.004	0.130	0.002	0.163	0.000	0.206
2	0.018	0.190	0.012	0.211	0.005 +	0.263	2	0.018	0.183	0.012	0.205 +	0.005 +	0.256
3	0.039	0.225-	0.029	0.251	0.015 +	0.316	3	0.037	0.219	0.028	0.244	0.015-	0.310
4	0.062	0.279	0.049	0.299	0.030	0.354	4	0.059	0.266	0.047	0.292	0.028	0.345-
5	0.086	0.303	0.070	0.340	0.046	0.397	5	0.083	0.295-	0.068	0.325-	0.045-	0.388
6	0.087	0.345-	0.094	0.374	0.065 +	0.438	6	0.084	0.336	0.091	0.364	0.063	0.430
7	0.134	0.385 +	0.103	0.413	0.086	0.477	7	0.129	0.376	0.100	0.403	0.083	0.469
8	0.135-	0.425-	0.136	0.451	0.108	0.523	8	0.130	0.416	0.131	0.440	0.104	0.505 +
9	0.189	0.463	0.166	0.500	0.132	0.562	9	0.182	0.455 +	0.163	0.476	0.127	0.538
10	0.190	0.500	0.184	0.549	0.157	0.603	10	0.183	0.492	0.175 +	0.524	0.151	0.570
11	0.225-	0.537	0.211	0.587	0.165 +	0.646	11	0.219	0.524	0.205 +	0.560	0.152	0.612
12	0.276	0.575 +	0.247	0.626	0.206	0.654	12	0.265-	0.554	0.236	0.597	0.198	0.655 +
13	0.294	0.615-	0.251	0.660	0.211	0.684	13	0.266	0.584	0.244	0.636	0.206	0.671
14	0.303	0.655 +	0.299	0.661	0.260	0.737	14	0.295-	0.624	0.292	0.675 +	0.249	0.692
15	0.345-	0.697	0.339	0.701	0.263	0.740	15	0.336	0.664	0.324	0.676	0.256	0.744

TABLE A1.1 *Continued*

<i>r</i>	90 %		95 %		99 %		<i>r</i>	90 %		95 %		99 %	
16	0.385 +	0.706	0.340	0.749	0.316	0.789	16	0.376	0.705 +	0.325–	0.708	0.308	0.751
17	0.425–	0.724	0.374	0.753	0.346	0.794	17	0.416	0.734	0.364	0.756	0.329	0.794
18	0.463	0.775 +	0.413	0.789	0.354	0.835–	18	0.446	0.735 +	0.403	0.764	0.345–	0.802
19	0.500	0.810	0.451	0.816	0.397	0.843	19	0.476	0.781	0.440	0.795–	0.388	0.848
20	0.537	0.811	0.500	0.834	0.438	0.868	20	0.508	0.817	0.476	0.825–	0.430	0.849
21	0.575 +	0.865 +	0.549	0.864	0.477	0.892	21	0.545–	0.818	0.524	0.837	0.462	0.873
22	0.615–	0.866	0.587	0.897	0.523	0.914	22	0.584	0.870	0.560	0.869	0.495–	0.896
23	0.655 +	0.913	0.626	0.906	0.562	0.935–	23	0.624	0.871	0.597	0.900	0.531	0.917
24	0.697	0.914	0.660	0.930	0.603	0.954	24	0.664	0.916	0.636	0.909	0.570	0.937
25	0.721	0.938	0.701	0.951	0.646	0.970	25	0.705 +	0.917	0.675 +	0.932	0.612	0.955 +
26	0.775 +	0.961	0.749	0.971	0.684	0.985	26	0.734	0.941	0.708	0.953	0.655 +	0.972
27	0.810	0.982	0.789	0.988	0.737	0.995	27	0.781	0.963	0.756	0.972	0.690	0.985 +
28	0.865 +	0.996	0.834	0.998	0.789	1.000	28	0.817	0.982	0.795–	0.988	0.744	0.995–
29	0.913	1	0.897	1	0.840	1	29	0.870	0.996	0.837	0.998	0.794	1.000
							30	0.916	1	0.900	1	0.848	1

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A1.3.4 If $n > 30$, look up $Z = Z_1 - \alpha/2$ in **Table A1.2** and compute:

$$P_u = p + Z \frac{p(1-p)}{n} \quad (\text{A1.2})$$

$$P_l = p - Z \sqrt{\frac{p(1-p)}{n}}$$

The interval from P_l to P_u is a $100(1-\alpha)\%$ confidence interval for the true proportion; that is, we may assert with $100(1-\alpha)\%$ confidence that $P_l < P < P_u$. It can be seen that as $n \rightarrow \infty$, $p(1-p)/n \rightarrow 0$. Thus smaller confidence intervals for the true proportion can be obtained by using larger samples.

A1.4 In application, we are interested in a 90% confidence interval if the true proportion ($\alpha = 0.10$) and we desire the width of the interval to be less than some value A . Values of $Z = Z_{0.95}$ will be taken from **Table A1.2** and used in the computation.

A1.4.1 Repeat the test n times to establish a minimum sample size.

A1.4.2 Compute p for the sample.

A1.4.3 If $n \leq 30$, use **Table A1.1** to find values. For example, if $n = 20$ and $r = 6$, at the 90% confidence level, $P_l = 0.141$ and $P_u = 0.500$.

A1.4.4 If $n > 30$, $Z_{0.95} = 1.645$ from **Table A1.2**. Compute:

$$P_u = Z_{0.95} \sqrt{p(1-p)/n} \quad (\text{A1.3})$$

$$P_l = Z_{0.95} \sqrt{p(1-p)/n}$$

For example, if $n = 40$ and $r = 12$; $p = 0.3$, $P_u = 0.419$, and $P_l = 0.181$.

A1.4.5 Compare $(P_u - P_l)$ to A .

A1.4.6 If $(P_u - P_l) > A$, repeat the test that increases the sample size to $n + 1$ and perform **A1.4.2** through **A1.4.5** with the larger sample.

A1.4.7 If $(P_u - P_l) < A$, a desired 90% confidence interval has been obtained.

TABLE A1.2 Cumulative Normal Distribution—Values of P^A

NOTE 1—Values of P corresponding to z_p for the normal curve. z is the standard normal variable. The value of P for $-z_p$ equals one minus the value of P for $+z_p$. For example, the P for -1.62 equals $1 - 0.9474 = 0.0526$.

z_p	0.00	0.01	0.02	0.03	0.04	0.05	0.06	0.07	0.08	0.09
0.0	0.5000	0.5040	0.5080	0.5120	0.5160	0.5199	0.5239	0.5279	0.5319	0.5359
0.1	0.5398	0.5438	0.5478	0.5517	0.5557	0.5596	0.5636	0.5675	0.5714	0.5753
0.2	0.5793	0.5832	0.5871	0.5910	0.5948	0.5987	0.6026	0.6064	0.6103	0.6141
0.3	0.6179	0.6217	0.6255	0.6293	0.6331	0.6368	0.6406	0.6443	0.6480	0.6517
0.4	0.6554	0.6591	0.6628	0.6664	0.6700	0.6736	0.6772	0.6808	0.6844	0.6879
0.5	0.6915	0.6950	0.6985	0.7019	0.7054	0.7088	0.7123	0.7157	0.7190	0.7224
0.6	0.7257	0.7291	0.7324	0.7357	0.7389	0.7422	0.7454	0.7486	0.7517	0.7549
0.7	0.7580	0.7611	0.7642	0.7673	0.7704	0.7734	0.7764	0.7794	0.7823	0.7852
0.8	0.7881	0.7910	0.7939	0.7967	0.7995	0.8023	0.8051	0.8078	0.8106	0.8133
0.9	0.8159	0.8186	0.8212	0.8238	0.8264	0.8289	0.8315	0.8340	0.8365	0.8389
1.0	0.8413	0.8438	0.8461	0.8485	0.8508	0.8531	0.8554	0.8577	0.8599	0.8621
1.1	0.8643	0.8665	0.8686	0.8708	0.8729	0.8749	0.8770	0.8790	0.8810	0.8830
1.2	0.8849	0.8869	0.8888	0.8907	0.8925	0.8944	0.8962	0.8980	0.8997	0.9015
1.3	0.9032	0.9049	0.9066	0.9082	0.9099	0.9115	0.9131	0.9147	0.9162	0.9177
1.4	0.9192	0.9207	0.9222	0.9236	0.9251	0.9265	0.9279	0.9292	0.9306	0.9319
1.5	0.9332	0.9345	0.9357	0.9370	0.9382	0.9394	0.9406	0.9418	0.9429	0.9441
1.6	0.9452	0.9463	0.9474	0.9484	0.9495	0.9505	0.9515	0.9525	0.9535	0.9545
1.7	0.9554	0.9564	0.9573	0.9582	0.9591	0.9599	0.9608	0.9616	0.9625	0.9633
1.8	0.9641	0.9649	0.9656	0.9664	0.9671	0.9678	0.9686	0.9693	0.9699	0.9706
1.9	0.9713	0.9719	0.9726	0.9732	0.9738	0.9744	0.9750	0.9756	0.9761	0.9767
2.0	0.9772	0.9778	0.9783	0.9788	0.9793	0.9798	0.9803	0.9808	0.9812	0.9817
2.1	0.9821	0.9826	0.9830	0.9834	0.9838	0.9842	0.9846	0.9850	0.9854	0.9857
2.2	0.9861	0.9864	0.9868	0.9871	0.9875	0.9878	0.9881	0.9884	0.9887	0.9890
2.3	0.9893	0.9896	0.9898	0.9901	0.9904	0.9906	0.9909	0.9911	0.9913	0.9916
2.4	0.9918	0.9920	0.9922	0.9925	0.9927	0.9929	0.9931	0.9932	0.9934	0.9936
2.5	0.9938	0.9940	0.9941	0.9943	0.9945	0.9946	0.9948	0.9949	0.9951	0.9952
2.6	0.9953	0.9955	0.9956	0.9957	0.9959	0.9960	0.9961	0.9962	0.9963	0.9964
2.7	0.9965	0.9966	0.9967	0.9968	0.9969	0.9970	0.9971	0.9972	0.9973	0.9974
2.8	0.9974	0.9975	0.9976	0.9977	0.9977	0.9978	0.9979	0.9979	0.9980	0.9981
2.9	0.9981	0.9982	0.9982	0.9983	0.9984	0.9984	0.9985	0.9985	0.9986	0.9986
3.0	0.9987	0.9987	0.9987	0.9988	0.9988	0.9989	0.9989	0.9989	0.9990	0.9990
3.1	0.9990	0.9991	0.9991	0.9991	0.9992	0.9992	0.9992	0.9992	0.9993	0.9993
3.2	0.9993	0.9993	0.9994	0.9994	0.9994	0.9994	0.9994	0.9995	0.9995	0.9995
3.3	0.9995	0.9995	0.9995	0.9996	0.9996	0.9996	0.9996	0.9996	0.9996	0.9997
3.4	0.9997	0.9997	0.9997	0.9997	0.9997	0.9997	0.9997	0.9997	0.9997	0.9998

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