

Standard Test Methods for Security of Swinging Door Assemblies¹

This standard is issued under the fixed designation F476; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon (ε) indicates an editorial change since the last revision or reapproval.

1. Scope

- 1.1 These test methods cover door assemblies of various materials and types of construction for use in wall openings to deter unwanted intruders.
- 1.2 Door assemblies, covered by these test methods, also include individual components such as the hinge, lock, door, strike, and jamb.
- 1.3 These test methods are designed to measure the capability of a swinging door assembly to restrain or delay and frustrate the commission of "break-in" crimes.
- 1.4 These test methods apply primarily to typical entry door assemblies.
- 1.5 This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use.

2. Referenced Documents

2.1 ASTM Standards:²

F471 Terminology Relating to Combination Locks (Withdrawn 2011)³

3. Terminology

- 3.1 Definitions:
- 3.1.1 *bolt, n*—any movable projection that blocks the movement of one object relative to another.
- 3.1.2 *bolt projection (or bolt throw), n*—distance from the edge of the door, at the bolt center line, to the farthest point on the bolt in the projected position, when subjected to end pressure.
- ¹ These test methods are under the jurisdiction of ASTM Committee F12 on Security Systems and Equipment and are the direct responsibility of Subcommittee F12.50 on Locking Devices.
- Current edition approved Feb. 1, 2014. Published March 2014. Originally approved in 1976 as F476-76. Last previous edition approved in 2002 as F476-84 (2002) which was withdrawn July 2011 and reinstated February 2014. DOI: 10.1520/F0476-14.
- ² For referenced ASTM standards, visit the ASTM website, www.astm.org, or contact ASTM Customer Service at service@astm.org. For *Annual Book of ASTM Standards* volume information, refer to the standard's Document Summary page on the ASTM website.
- ³ The last approved version of this historical standard is referenced on www.astm.org.

- 3.1.3 *component*, n—as distinguished from a part, a subassembly that combines with other components to make up a total door assembly.
- 3.1.3.1 *Discussion*—The prime components of a door assembly include: door, lock, hinges, jamb, strike, and wall.
- 3.1.4 *cylinder*, *n*—complete operating unit that usually consists of the plug shell, tumblers, springs, plug retainer, a cam/tailpiece or other actuating device, and all other necessary operating parts.
- 3.1.5 *cylinder core* (*or cylinder plug*), *n*—central part of a cylinder, containing the keyway, that is rotated by the key to operate the lock mechanism.
- 3.1.6 *deadbolt, n*—bolt, which requires a deliberate action to extend, and resists end pressure in the unlocking direction when fully extended.
- 3.1.7 *dead latch (or dead locking latch bolt)*, *n*—latchbolt with a deadlocking mechanism.
- 3.1.8 *door assembly, n*—any combination of a door, frame, hardware, and other accessories that is placed in an opening in a wall that is intended primarily for access or for human entrance or exit.
- 3.1.9 *jamb*, *n*—vertical members of a door frame (such as, those fixed members to which the door is secured).
- 3.1.10 *key-in-knob lockset*, *n*—any lockset with a key operated cylinder in one or more knobs.
- 3.1.11 *key-in-lever lockset*, *n*—any lockset with a key operated cylinder in one or more level handles.
 - 3.1.12 *latch*:
- 3.1.12.1 *n*—mechanical or magnetic door fastener that can automatically keep a door, gate, and so forth, closed.
- 3.1.12.2 *v*—engagement of a latch when a door, gate, and so forth, is pushed or pulled closed.
- 3.1.13 *latch bolt, n*—spring-actuated bolt, normally with one or more beveled surfaces, that, when aligned with the strike, engages it automatically.
- 3.1.14 *lock*, *n*—any device that prevents access or use by requiring special knowledge or equipment.
- 3.1.15 *lock front, n*—outer plate through which the locking bolt projects and which is usually flush with the edge of the door.



- 3.1.16 *part*, *n*—as distinguished from component, a unit (or subassembly) that combines with other units to make up a component.
- 3.1.17 *strike*, *n*—bolt receptacle typically mounted in the door jamb or the floor.
 - 3.1.18 swinging door, n—stile (side)-hinged door.
- 3.1.19 *Type A lock*, *n*—lock that uses a single bolt or separate latch and lock bolts that are mechanically interconnected.

4. Apparatus

- 4.1 Test equipment suitable for use in evaluating the physical security of door assemblies and components is described in this section. While certain commercial instruments are identified to adequately describe the test equipment, in no case does such identification imply recommendation or endorsement, nor does it imply that the material or equipment described is necessarily the best for the purpose.
- 4.2 *Door Ram*—The door ram is a pendulum system with a cylindrical weight capable of delivering horizontal impacts of 200 J (148 ft·lbf). Fig. 1 is a photograph of such a system. A sketch of the ram is shown in Fig. 2. It is a steel cylinder 152.4 mm (6 in.) in diameter, 393.7 mm (15.5 in.) long, with a hemispherical impact nose. It weighs 45 kg (99.2 lb). The impact nose used in this equipment is made from cast epoxypolyamide resin; however, any durable impact-resistant material is satisfactory. The suspension system for the door ram

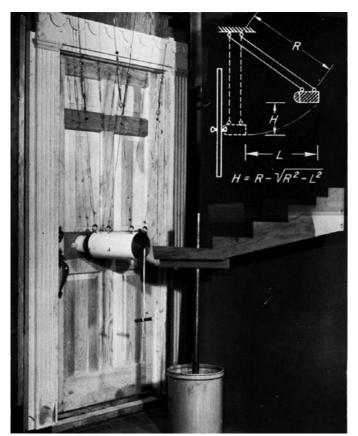


FIG. 1 Door Ram Pendulum System

- consists of four flexible steel cables providing a swing radius of 1.71 m (5.61 ft), as shown in Fig. 3. These cables are adjusted to equal length with turnbuckles such that the ram swings in a straight, true arc and are attached to a steel frame that can be adjusted to be level. Fig. 1 also includes a diagram of the pendulum system when elevated and at rest, and the measurements required to calculate the impact energy of the system. Table 1 presents the potential energy of a pendulum system with a 45-kg (99.2-lb) weight as a function of various elevations of the weight.
- 4.2.1 The use of a calibrated elevation stand, as shown in Fig. 1, is a convenient means of quickly and reproductively establishing the proper ram elevation for each required impact.
- 4.3 Component Ram—The component ram is a pendulum system capable of delivering impacts of 100 J (74 ft·lbf). A sketch of the pendulum system is shown in Fig. 4. The pendulum weight has a diameter of 56 mm (2 ³/16 in.), a length of 838 mm (33 in.), and weighs 16 kg (35.3 lb). The impact nose is made from a 6-mm (¹/4-in.) carriage bolt with the square shank removed. The vacuum release mechanism also shown in Fig. 4 is a convenient means of holding the component ram in the elevated position and releasing it to deliver the required impact.
- 4.3.1 The height of drop of the pendulum for an impact of 100 J (74 ft·lbf) is 637 mm (2.09 ft).
- 4.3.2 The vertical pendulum system shall use a steel weight and be capable of delivering vertical (downward) impacts of up to 100 J (74 ft·lbf) to a door knob installed in a door assembly.
- 4.4 *Vertical Impactor*—The vertical impactor is a rigid pendulum system capable of delivering downward impacts of 100 J (74 ft·lbf). Fig. 5 shows a photograph of the system. The construction of the pendulum is shown in Fig. 6, and the construction of the pivot assembly is shown in Fig. 7.
- 4.4.1 The effective weight of the flat-nosed steel weight is 10 kg (22 lb). An impact of 100 J (74 ft·lbf) is provided by a drop height of 1.02 m (3.35 ft).
- 4.4.2 *Torque Applicator*—The portable torque applicator shall be capable of delivering and measuring up to 160 N·m (118 lbf·ft) of torque to both door knobs and lock cylinders. The torque loading adapters shall be designed to grip the knobs and cylinders.
- 4.4.3 *Tension-Loading Device*—The tension-loading device shall be capable of delivering and measuring tensile forces of up to 18 kN (4000 lbf).
- 4.4.4 *Compression-Loading Device*—The compression-loading device shall be capable of delivering and measuring compressive forces of up to 900 N (200 lbf).
- 4.4.5 Jamb-Spreading Device—The jamb-spreading device shall be capable of delivering to door jambs and measuring spreading forces of up to 22 kN (4950 lbf) with a means of measuring up to 13 mm ($\frac{1}{2}$ in.) of increase in lock-front to strike distance. The device shall have on each end either a load bearing plate or pressure foot that provides a minimum contact surface of 40 by 120 mm ($\frac{1}{2}$ by 5 in.).
- 4.4.6 *Instrument Accuracy*—The tension loading and jamb-spreading devices shall have a combined calibration and reading error no greater than 200 N (45 lbf). The compression-loading device shall have a combined calibration and reading

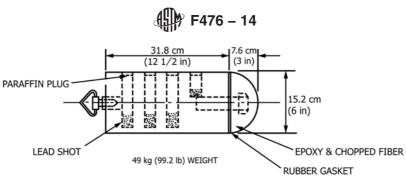


FIG. 2 Door Ram

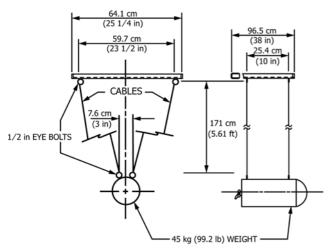


FIG. 3 Door Ram Suspension System

TABLE 1 Potential Energy of Pendulum^A Used in Door Assembly and Component Tests

Potential Energy, J (ft·lbf)	Height Of Drop (<i>H</i>), mm (ft) ^B	Horizontal Swing Distance (L), mm (ft)
60 (44.3)	136 (0.45)	668 (2.19)
80 (59.0)	181 (0.59)	765 (2.51)
100 (73.8)	227 (0.74)	851 (2.79)
120 (88.5)	272 (0.89)	925 (3.04)
140 (103.3)	317 (1.04)	992 (3.26)
160 (118.0)	363 (1.19)	1053 (3.46)
180 (132.8)	408 (1.34)	1108 (3.64)
200 (147.5)	454 (1.49)	1160 (3.81)

 $^{^{}A}\!$ The pendulum weighed 45 kg (99.2 lb) and was suspended with a wing radius (*R*) of 1710 mm (5.61 ft).

$$(H) = R - \sqrt{R^2 - L^2}$$

error of no greater than 40 N (9 lbf). The torquemeter shall have a combined error no greater than 3.4 N·m (2.5 lbf·ft). The impact energy of each pendulum system shall be controlled to within ± 1 %.

5. Construction and Size

- 5.1 The construction and size of the test door assemblies, consisting of single doors, doors in pairs, special-purpose doors (such as Dutch doors), jambs and headers, and all hardware components shall be representative of the classification or rating that is desired.
- 5.2 The door assembly support fixture shall simulate the rigidity normally provided to a door assembly in a building by the ceiling, floor, and walls. Fig. 8 shows an acceptable fixture.

- 5.3 The test fixture for door, door jamb, hinge, lock, strike, and other components shall consist of a vertical wall section constructed from 2 by 4 wood studs, 410 mm (16 in.) on center, with a rough entry door opening, and shall be covered with 13-mm (½-in.) exterior grade plywood sheathing on the exterior and ½-in. gypsum board on the interior. It shall be constructed as shown in Fig. 9 and shall be secured to the wall support fixture (at the sides and top) and to the laboratory floor. For tests of door, lock, strike, and hinge components, the fixture wall section shall also include a door jamb.
- 5.4 The alternative test fixture for lockset components shall consist of a small door assembly, as shown in Figs. 10 and 11. The frame shall be fabricated from steel angle and plate at least 5 mm ($\frac{3}{16}$ in.) thick. The test panel shall be 600 mm (24 in.) square and 45 mm (13/4 in.) thick, made by bonding three pieces of plywood together or by cutting a section from a 45-mm (1³/₄-in.) solid wood core door (such as, glued block core construction NWMA IS-1). A 50 by 50 by 3-mm (2 by 2 by \(\frac{1}{8}\)-in.) steel angle shall be bolted to the hinge edge of the door panel, and a removable steel strike plate shall be bolted to the frame at the lock position of the door panel. The alternate lockset component test fixture shown in Figs. 10 and 11 may be used in lieu of the lockset component test fixture shown. The use of steel plates and expendable wood blocks as shown in the drawing may be used on the full size test fixture as described in 5.3 when testing lock and hinge components.
- 5.5 The test fixture for static bolt load tests (9.2) shall consist of a vertical panel fabricated from wood attached to a stable horizontal base, as shown in Fig. 12. The top edge of the panel shall be parallel to the bottom surface of the base. The panel shall be about 45 mm (13/4 in.) thick and the top edge shall be prepared to permit the lock set which is being tested to be mounted in the panel in accordance with the manufacturer's instructions.

6. Sampling

6.1 Specimens shall be representative and adequately identified for future reference. Complete manufacturer or fabricator installation instructions and full-size templates for all items of hardware shall be included.

7. Mounting for Test

- 7.1 Swinging doors shall be mounted so as to open away from the working area, except when testing an out-swinging door assembly.
- 7.2 Prepare doors and door jambs for the installation of locksets and hinges in conformance with the manufacturer's

^BHeight of drop.



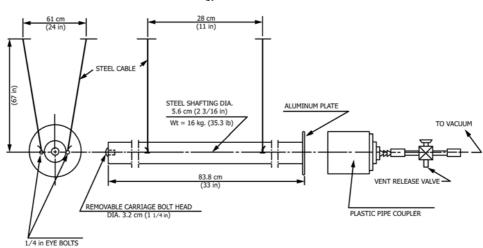


FIG. 4 Vacuum Release Mechanism

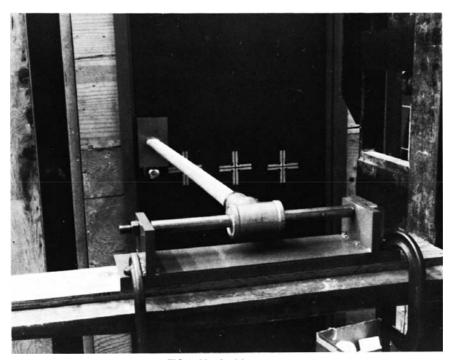


FIG. 5 Vertical Impactor

instructions. Follow the manufacturer's instructions for fastening the jamb to the support fixture described in 5.2.

7.3 Install components such as test doors, door jambs, hinges, and jamb/strikes in the component test fixture described in 5.3. Except when testing hinges, hinge the door with $1\frac{1}{2}$ pairs of 115-mm ($4\frac{1}{2}$ -in.) steel butt hinges, and fix it in the closed-locked position (at the normal lock point) with a real or simulated latch bolt having sufficient strength and stiffness to prevent it from failing during test. In the absence of other construction specifications, make the clearances on the lock side, hinge side, and top of the door 3.2 ± 0.4 mm ($\frac{1}{8} \pm \frac{1}{64}$ in.). Clearance at the threshold is not considered critical in these tests.

7.4 To test locksets as components, install them in the alternative component test fixture described in 5.4. Fix the test

panel in the closed locked position at the normal locking point. Hinge the test panel with two 115-mm ($4\frac{1}{2}$ -in.) steel butt hinges.

7.5 To test lock sets for static bolt load, install them in the test fixture described in 5.5.

8. Procedure

8.1 One complete assembly shall be used to conduct the tests. Tests shall be given in the sequence of Sections 9-20. Tests under Sections 9, 11, 12, 13, 14, and 15, if conducted in the test panel, shall not be repeated in the door assembly being tested. These tests need not be repeated for successive tests of other door assemblies where the same lock model is being used.



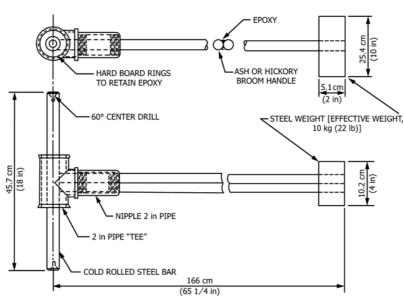


FIG. 6 Vertical Impactor Pendulum System

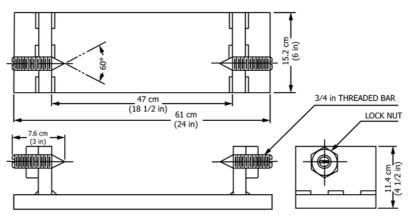


FIG. 7 Vertical Impactor Pivot Assembly

9. Static Bolt Load Test

- 9.1 To test Type A and B locks and all door assembly locks, mount the lock in the test fixture described in 5.5. Lock the door lock with the dead bolt or dead latch in the fully projected position. If the lock incorporates a dead-latch plunger, attach a 6.5-mm (1/4-in.) spacer to the lock front. Allow the dead-latch plunger to project flush with the top of the spacer, and hold it in that position with a piece of tape, or by another suitable means.
- 9.2 Place the lock, in the test fixture, in a compression testing machine, or mount it on a firm, level surface with the compression loading device directly above it with the loading face parallel to the lock front, and the axis of the hydraulic ram perpendicular to the lock front. Apply an increasing compressive load to the end of the latch bolt or the dead bolt. Note the maximum force required to depress the latch bolt or the dead bolt to where the farthest point on the bolt is 6 mm (1/4 in.) from the lock front surface.
- 9.3 To test for bolt projection, apply end pressure to the projected dead bolt or dead latch and measure the distance

from the lock front surface to the farthest point on the bolt or latch at the center line.

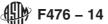
9.3.1 Following the test of a lock incorporating a dead latch, place the strike plate provided with the lock over the latch of a dead latch to determine whether it is possible for both the dead latch and the dead plunger to enter the hold in the strike simultaneously.

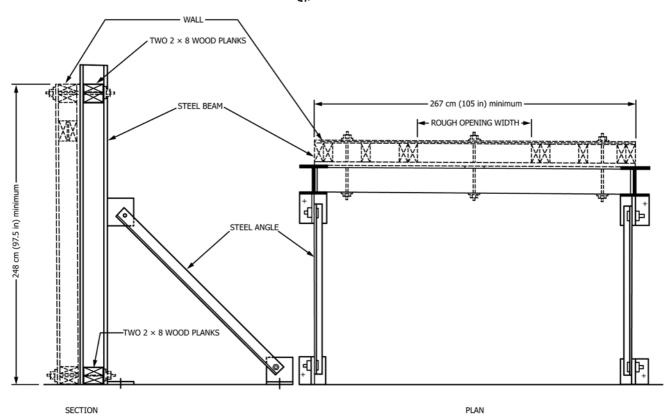
10. Jamb Stiffness Test

- 10.1 Prepare the test specimen in accordance with 7.3. Position the jamb spreading device (4.4.5) between the door jambs, at lock height. Apply increasing force as required and measure the space between the lock front and strike.
- 10.2 While the required load is being applied, or the lock front-to-strike distance is increased, push or pull on the door to determine whether the dead bolt or dead latch is engaged with the strike.

11. Knob Impact Test

11.1 Prepare the test specimen in accordance with 7.3 or 7.4 and lock the door or test panel in the closed position. Position





NOTE 1—Vertical members are equivalent to, or better in bending than, W8 imes 10 steel beam.

NOTE 2—Horizontal members are equivalent to, or better in bending than, a 2 by 8-ft wood plank.

NOTE 3—Diagonal members are equivalent to, or better than, 2 by 2 by 1/4 in.-steel angle.

NOTE 4—Adequate floor anchorage of the entire wall support fixture is essential.

FIG. 8 Wall Support Fixture

the vertical impactor (4.4) so that the pendulum arm is horizontal when the striking weight contacts the top of the door knob, and its center of gravity is in the vertical center-line through the knob. Raise the weight to the height necessary to deliver the required impact and release it. Deliver the required number of impacts to the knob. After each impact, attempt to open the door or test panel by turning the knob. If the knob is broken off, manipulate the exposed lock mechanism by hand or with the aid of a screwdriver.

11.2 With the door or test panel open, and the dead bolt or dead latch in the projected, locked position, attempt to (a) depress the dead bolt by applying hand pressure to its end or (b) depress the latch and dead-latch plunger fully, allow the latch to extend, then slowly allow the plunger to project until the last point of dead locking is reached.

12. Cylinder-Core Tension Test

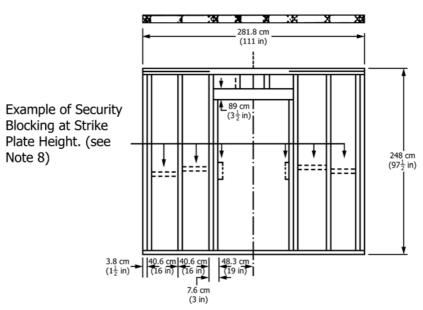
12.1 Prepare the test specimen in accordance with 7.3 or 7.4 and lock the door or test panel in the closed position. Drill a

hole in the cylinder core using a No. 21 drill, adjacent to the keyway to a minimum depth of 13 mm (½ in.). Tap this hole with a 10-32 thread. Attach the tensile loading device (4.4.3) to a rigid load-bearing support in front of the cylinder, and align the pulling axis with that of the hole in the cylinder. Attach the pulling adapter to the cylinder with a 10-32 hardened cap screw fully threaded into the tapped hole. Connect the cylinder tensile loading device to the adapter, and apply the required tensile force to the cylinder. Following this test, release the load and attempt to open the door or test panel by manipulating an exposed lock mechanism by hand or with the aid of a screwdriver. If the core or cylinder is not damaged, open the door, and test the dead latch or dead bolt for end pressure resistance as in 11.2.

13. Cylinder-Body Tension Test

13.1 Prepare the test specimen in accordance with 7.3 or 7.4 and lock the door or test panel in the closed position. Drill a hole in the cylinder body using a No. 3 drill, near the center of





Note 1-All studs, plates, and headers are 2-by-4s.

Note 2—Nail sole plate and lower member of top plate to each stud with 2—16d end nails.

Note 3—Nail upper member of top plate to the lower member with 16d nails, one nail near each stud and two near each end.

Note 4—Nail the double studs together with 16d nails not more than 610 mm (24 in.) on centers.

Note 5-Nail the header (two 2-by-4s) to each full length stud with 4-16d end nails.

Note 6-Nail 1/2-in. gypsum drywall to all supports with threaded drywall nails at 200 mm (8 in.) on centers.

Note 7—Security blocking may be necessary to achieve successful jamb stiffness test results. If blocking is used, it shall be reported in the test report. The nature of the blocking shall be indicated.

FIG. 9 Door, Door Jamb, Hinge, and Lock-Strike Component Fixture

the cylinder face, to a minimum depth of 13 mm ($\frac{1}{2}$ in.). If the lock is constructed such that only the cylinder core is exposed, drill through the material covering the face of the cylinder body, into the cylinder. Tap this hole with a 1/4-28 thread. Attach the cylinder tensile loading device (4.4.3) to a rigid load-bearing support in front of the cylinder, and align the pulling axis with that of the hole in the cylinder. Attach the pulling adapter to the cylinder with a 1/4-28 hardened cap screw fully threaded into the tapped hole, or other appropriate devices. Connect the cylinder pulling device to the adapter, and apply the required tensile force to the cylinder. Following this test, release the load and attempt to open the door or test panel by manipulating an exposed lock mechanism by hand or with the aid of a screwdriver. If the cylinder is not damaged, open the door, and test the dead latch or dead bolt for end pressure resistance as in 11.2.

14. Knob Torque Test

14.1 Prepare the specimen test in accordance with 7.3 or 7.4 and lock the door or test panel in the closed position. Attach the torque-loading adapter to the knob and connect the torque applicator to it (4.4.2). Alternately subject the knob to the required torque in both the clockwise and counter-clockwise directions, applying the torque as rapidly as possible. Inspect the lock to determine whether the bolt is retracted from the strike when the torque is applied. If the knob is broken off, attempt to open the door or test panel by manipulating the lock mechanism by hand or with the aid of a screwdriver. If the

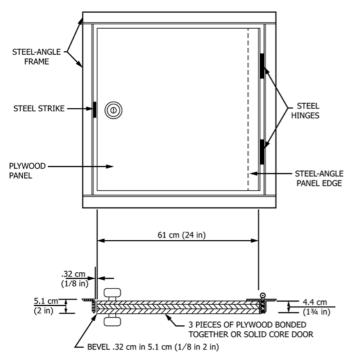
knob is not broken off, test the dead bolt or dead latch for end pressure resistance as in 11.2.

15. Cylinder Torque Test

15.1 Prepare the test specimen in accordance with 7.3 or 7.4 and lock the door or test panel in the closed position. Attach the torque loading adapter to the cylinder and connect the torque applicator to it (4.4.2). Alternatively subject the cylinder to the required torque in both the clockwise and counter-clockwise directions, applying the torque as rapidly as possible. Inspect the lock when the torque is applied to determine whether the bolt is withdrawn from the strike. If the cylinder is loose, attempt to open the door or test panel by manipulating the lock mechanism by hand or with the aid of a screwdriver. If the cylinder is not damaged, test the dead bolt or dead latch for end pressure resistance as in 11.2.

16. Cylinder Impact Test

16.1 Prepare the test specimen in accordance with 7.3 or 7.4 and lock the door or test panel in the closed position. Position the component ram pendulum weight (4.3) so that, at rest, its axis is horizontal and coincides with the major axis of the cylinder and its striking nose just touches the face of the cylinder. Pull back the pendulum weight to the height necessary to produce the required impact and release it. Repeat this to deliver the required number of impacts. After each impact, attempt to open the door or test panel by manipulating the lock mechanisms by hand or with the aid of a screwdriver if the



Note 1—The door panel consists of three pieces of plywood [610 mm (24 in.) square] bonded together (1 piece, 19 mm ($\frac{3}{4}$ in.) thick, between two pieces, each 13 mm ($\frac{1}{2}$ in.) thick); or a glued block core door with premium or good grade hardwood veneer (NWMA I.S. 1-74).

 ${\it Note}$ 2—The door panel shall have a steel angle bolted to the hinge edge.

Note 3—The steel angle frame and panel edge shall be 51 by 51 by 3 mm (2 by 2 by $\frac{1}{8}$ in.) thick.

FIG. 10 Lockset Component Test Fixture

cylinder is damaged. If the cylinder is not damaged, test the dead bolt or dead latch for end pressure resistance as in 11.2.

17. Door Impact Test

17.1 Prepare the test specimen in accordance with 7.3 and lock the door in the closed position. Set up the door ram pendulum weight (4.2) so that its axis is horizontal and perpendicular to the face of the door at a point defined by the intersection of the vertical center line of the door and a line from the center of the bolt to the center of the mid-height hinge (or the midpoint between hinges, when the door is hung with two hinges).

17.2 Attach to the door, centered on the impact point, a rigid foamed polystyrene impact buffer that has a diameter of 150 mm (6 in.), a thickness of 50 mm (2 in.), and a density of 32 kg/m³ (2 lb/ft³). Position the door ram such that its striking nose just touches the surface of the buffer when at rest. Pull back the pendulum weight to the height necessary to produce the required impact, and release it. Subject the door to two impacts at each required impact level, attaching a new buffer for each impact. If the door is forced open by the test, without damaging the jamb/strike or lock component, the door specimen fails the test. If the door surface is broken, attempt to reach inside the door, and unlock it from the inside.

17.3 If the door has one or more recessed panels, subject the one closest to the lock to two impacts at each required impact

level. Locate the impact point on the corner of the panel closest to the lock, 75 mm (3 in.) in from the vertical and horizontal edges of the panel. Perform the test as in 17.1 and 17.2 attaching a new impact buffer for each impact. If the panel is broken, attempt to open the door by reaching through the opening and unlocking the door from the inside.

17.4 To test glazing panels, set up the component ram pendulum weight (4.3) so that, at rest, its striking nose just touches the front surface of the panel at a point 40 mm (1.6 in.) from the horizontal and vertical edges of the panel closest to the lock. Pull back the pendulum weight to the height necessary to produce the required impact, and release it. Repeat this to deliver the required number of impacts. If the panel is broken, reach through the opening and attempt to open the door by unlocking it from the inside. Whether to use glazing impacts as described in Table 1 under Grade 10, shall be determined by the authorities using this test procedure. Such authority may eliminate this portion of the test.

17.5 Following the door impact test, inspect the door to determine whether there is enough damage to invalidate the subsequent tests; and if so, replace it.

18. Hinge Impact Test

18.1 Prepare the test specimen in accordance with 7.3 and lock the door in the closed position. When testing hinges incorporating a mechanical interlock between the leaves in the closed position, and door assemblies using such hinges, remove the hinge pin during this test. Set up the door ram pendulum weight so that its axis is horizontal and perpendicular to the face of the door at a point 200 mm (8 in.) from the bottom hinge, on a horizontal line through the mid point of the hinge.

18.2 Attach an impact buffer, as described in Section 17, to the face of the door, centered on the impact point, and position the pendulum so that its striking nose just touches the surface of the buffer, when at rest. Pull back the pendulum weight to the height necessary to produce the required impact, and release it. Subject the door to two impacts at each required impact level, attaching a new buffer for each impact. After each impact, try to open the door.

18.3 A door component failure consists of any splitting or fracture of the door which allows it to be opened. A jamb component failure consists of any splitting, fracture, or pullout of the attachment screws which allows the door to be opened. A hinge component failure consists of any damage to the leaves or pin of the hinge which allows the door to be opened.

18.4 Following the hinge impact test, inspect the components to determine whether there is sufficient damage to invalidate the subsequent test, and if so, replace the damaged components.

19. Hinge Pin Tensile Load

19.1 Drill a hole into the end of the exposed hinge pin with a No. 21 drill, centered on and aligned with the axis of the pin to a depth of 13 mm (0.5 in.). Tap the hole with a 10-32 tap, and attach the tensile loading adapter (Fig. 13) to it with a hardened cap screw. Clamp one leaf of the hinge in a vice, such



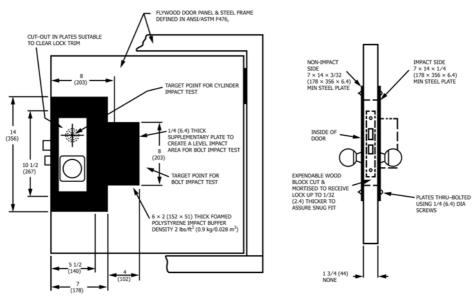
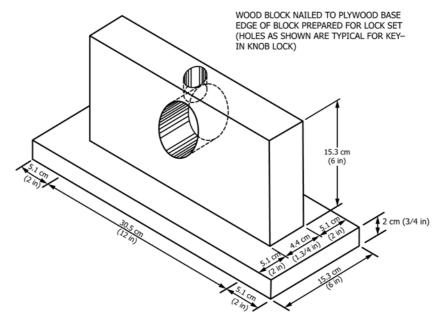


FIG. 11 Alternate Lockset Component Test Fixture



Note 1—The wood block is nailed to the plywood base edge of block prepared for lock set. (The holes as shown are typical for key-in knob lock.)

FIG. 12 Static Bolt Load Test Fixture

that the hinge pin is in the horizontal plane. Attach the tensile loading device (4.4.3) to a rigid load-bearing support in front of the hinge, and align the pulling axis with the axis of the hinge pin. Attach the tensile loading adapter to the tensile device and apply the required load.

20. Bolt Impact Test

20.1 Prepare the test specimen in accordance with 7.3 or 7.4 and lock the door in the closed position. Set up the door ram pendulum weight (4.2) so that its axis is horizontal, and perpendicular to the face of the door at a point defined by the

intersection of a vertical line 200 mm (8 in.) from the lock edge, and a line from the center of the bolt to the center of the mid-height hinge (or the mid point between hinges, when the door is hung with two hinges).

20.2 Attach an impact buffer, as described in Section 17, to the face of the door, centered on the impact point, and position the pendulum so that it just touches the surface of the buffer when at rest. Pull back the pendulum weight to the height necessary to produce the required impact, and release it. Subject the door to two impacts at each required impact level,



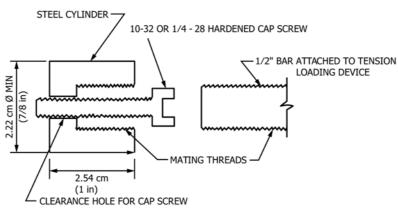


FIG. 13 Cylinder-Pulling Adapter (Cylinder Tapped for Cap Screw)

attaching a new buffer for each impact. After each impact, try to open the door or test panel by turning the knob, and test the dead bolt or dead latch for end pressure resistance (11.2).

20.3 A jamb/strike component failure consists of a pull-out or fracture of the strike attachment screws or any splitting, bending, or fracture of the door jamb at the strike that permits the door to be opened. A door component failure consists of any splitting or fracture of the door that allows it to be opened.

A lock component failure consists of any damage to the lock mechanisms or bolt that allows the door to be opened.

21. Precision and Bias

21.1 These test methods do not generate numerical values. They establish a pass/fail condition which cannot generate numerical values for precision and bias.

APPENDIXES

(Nonmandatory Information)

X1. APPARATUS

X1.1 Torque Applicator

X1.1.1 The torque applicator consists of a commercial torque wrench. To achieve adequate accuracy of the measured torque, it was necessary to bond strain gauges to the spring shaft of the torque wrench. These were connected to standard strain gauge read-out instrumentation. The system was calibrated to measure torque to 163 N·m (120 lbf·ft). This equipment is shown in Fig. X1.1.

X1.1.2 Two load adapters are also required to apply the torque to door knobs and lock cylinders. Fig. X1.2 shows a sketch of the adapter used for door knobs. It is essentially a cylinder slightly larger than the diameter of the knob, with four set screws that are tightened against the side of the knob. The end of the cylinder away from the knob has a square shank that is gripped with a standard socket attached to the torque wrench.

X1.1.3 The load adapter used to apply torque to lock cylinders is shown in Fig. X1.3. It is essentially a steel disk with a spot face to accommodate the cylinder core, and a square shank on the opposite side, and three 3-mm (½-in.) holes drilled on a 9-mm (¾-in.) radius from the center of the disk, spaced 120° apart. In use, the holes in the disk are used as a drill pattern to drill 3-mm diameter holes 6 mm (¼ in) deep into the face of the lock cylinder. A 3-mm drill rod is inserted in each hole, extending through the disk into the holes

in the cylinder. The torque wrench is connected to the adapter with a standard socket.

X1.2 Tensile-Loading Device

X1.2.1 The tensile-loading device has a load and force measuring capacity of 17.8 kN (4000 lbf). A double-acting hydraulic ram connected directly to a load cell was used for this equipment. The ram was an ordinary auto-body jack with permanently connected hoses and pump. The ram had a capacity of 17.8 kN in tension and 35.6 kN (8000 lbf) in compression. The load was measured with a universal, strain gauge type load cell with a capacity of 22 kN (5000 lbf) in tension and compression. Fig. X1.4 is a picture of this equipment together with a conventional strain-gauge readout instrument. In use, the load is applied to the cylinder core or body using an adapter such as that shown in Fig. 12.

X1.3 Jamb-Spreading Device

X1.3.1 The jamb-spreading device is a compressive-loading and force-measuring device with a capacity of 22 kN (5000 lbf). This is the same equipment used for the cylinder puller. The tensile loading rings are removed, and the force is applied to the jamb through two load distributing pressure plates made of 3-mm (½-in.) steel, 40 by 120 mm (1.5 by 5 in.) in size. The use of this equipment in the spreading of a door jamb is

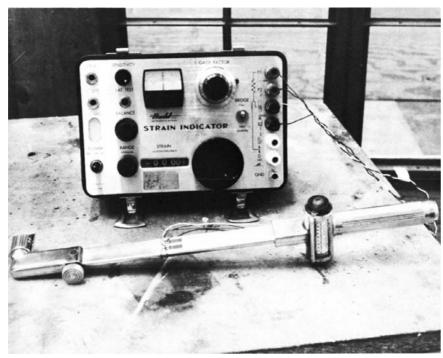


FIG. X1.1 Torque Applicator System

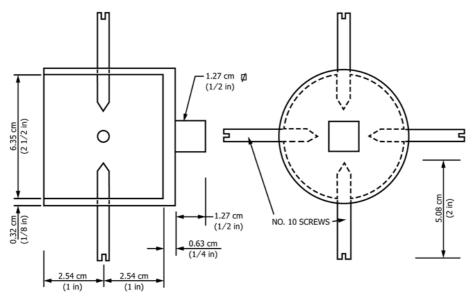


FIG. X1.2 Knob-Torque Adapter

illustrated in Fig. X1.5. The load is being indicated on the y axis of an x-y plotter while the movement of the jamb/strike is indicated on the x axis. The movement of the jamb/strike was measured by means of a linear variable differential transformer attached to the door.

X1.4 Compression-Loading Device

X1.4.1 The compression-loading device has a load- and force-measuring capacity of 900 N (200 lbf). A universal

testing machine was used for this equipment; however, the equipment described in X1.3.1 could be used for this purpose. The use of the double-acting hydraulic ram would require the construction of a rigid frame to hold the ram in a vertical position above a fixed base. This base must be perpendicular to the axis of the ram, and there must be sufficient clearance between the base and the pressure face of the ram to allow the static bolt load fixture, with the lock installed in it, to be positioned directly under the ram pressure face.



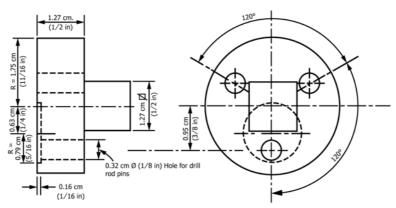


FIG. X1.3 Cylinder-Torque Adapter

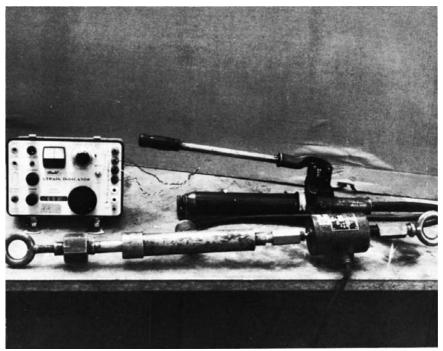


FIG. X1.4 Hydraulic Ram and Load Cell

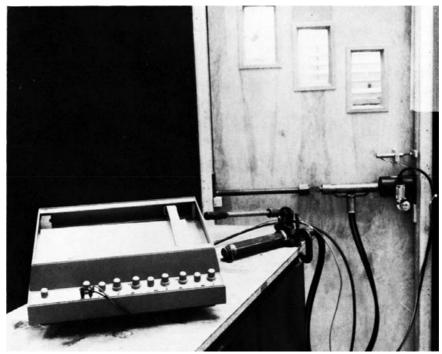


FIG. X1.5 Jamb Spreading Device

X2. RECOMMENDED ACCEPTANCE CRITERIA AND CLASSIFICATION

X2.1 Summary

- X2.1.1 Test Methods F476 *does not* establish acceptance criteria.
- X2.1.2 The NILECJ (National Institute of Law Enforcement and Criminal Justice) Standard and the CTRF Report, both, relate certain levels of force as generated by man (and tools); and the point of failure of certain assemblies as tested.
- X2.1.3 CTRF concludes: "The structural evaluation of standard exterior single door systems, under static and dynamic loads, demonstrated they will not withstand man's capability for forced entry without additional local reinforcement on both the door and the door jamb at the latch."
- X2.1.4 As a guide in the selection of an acceptable performance level which can be used in connection with Test Methods F476, the levels of acceptance proposed by the NILECJ document are included in X2.2.

X2.2 General Criteria

- X2.2.1 Table X2.1 lists proposed minimum requirements for four grades of door assemblies.
- X2.2.2 As general requirements, an item shall fail a test if, at any time during the test, an individual can open the door from the outside by the following methods: pushing or pulling on it; turning the knob; manipulating an exposed lock mechanism; reaching through damaged portions of the door and unlocking it from the inside; entering through damaged portions of the door even though it might not be possible to open the door; or depressing the dead latch or dead bolt using static load applied by hand.

- X2.2.3 *Disassembly*—Door assemblies and components shall incorporate no screw, bolt, nail, staple, or other mechanical fastener that is accessible from the outside, and whose removal would permit entry by disassembly.
- X2.2.4 *Lock Type*—Door assemblies and locks tested as components shall meet the requirements of the knob impact test, unless it is determined by inspection that the locks are of Type B.
- X2.2.5 *Grades*—A door assembly meets the requirements for a specific security grade if none of the sample assemblies fail any of the required tests for that grade. This grade holds only when the wall construction and the door assembly installation are identical in the use and the test situation, or are demonstrated to be equivalent.
- X2.2.5.1 A component meets the requirements for a specific security grade if none of the sample assemblies fail any of the required tests for that grade.
- X2.2.5.2 Door assemblies constructed from components tested and graded in accordance with these test methods shall be considered to provide a security grade equal to that of the component having the lowest grade level, providing that the wall construction and jamb and strike and hinge installations are identical in the use and the test situation, or are demonstrated to be equivalent.
- X2.2.6 Bolt Projection and Strike Hole Size—When Type A and B locks, as components, are tested, the dead bolt or dead latch projection shall be a minimum of 14.3 mm (%16 in.) for Grades 10 and 20, and 17.5 mm (11/16 in.) for Grades 30 and 40.

TABLE X2.1 Door Assembly Minimum Requirements

Test	Measured Parameters	Grade 10	Grade 20	Grade 30	Grade 40
Static bolt load ^A	resistance	670 N (150 lbf)	670 N (150 lbf)	670 N (150 lbf)	670 N (150 lbf)
in	force to spread	6000 N (1350 lbf)	8000 N (1800 lbf)	16 000 N (3600 lbf)	22 000 N (4950 lbf)
	increase in lock-front to strike space	9.5 mm (0.375 in.)	9.5 mm (0.375 in.)	13 mm (0.5 in.)	13 mm (0.5 in.)
Knob impact ^{A, C}	resistance: 100-J (74- ft·lbf) impacts	one blow	two blows	five blows	ten blows
Cylinder core load ^A	resistance	1300 N (290 lbf)	4800 N (1080 lbf)	11 000 N (2495 lbf)	11 000 N (2495 lbf)
Cylinder body load ^{A, D}	resistance				16 000 N (3600 lbf)
Knob Torque ^{A, C}	resistance	25 N·m (18.5 lbf·ft)	50 N·m (37 lbf·ft)	110 N·m (81 lbf·ft)	160 N·m (118 lbf·ft)
Cylinder torque ^{A, D}	resistance			110 N·m (81 lbf·ft)	160 N·m (118 lbf·ft)
Cylinder impact ^{A, D}	resistance: 100-J (74 ft·lbf) impacts			five blows	ten blows
Door impact ir	impact resistance at center and panel	two blows of 80 J (59 ft-lbf)	Grade 10 requirements plus two blows of 120 J (89 ft-lbf)	Grade 20 requirements plus two blows of 160 J (118 ft-lbf)	Grade 20 requirements plus two blows of 200 J (148 ft-lbf)
	impact resistance of glazing: 100 J (74 ft·lbf)	one blow ^{E, F}	two blows	five blows	ten blows
	impact resistance at	two blows of 80 J (59	Grade 10 requirements	Grade 20 requirements	Grade 20 requirements
	hinge	ft-lbf)	plus two blows of 120 J (89 ft·lbf)	plus two blows of 150 J (118 ft·lbf)	plus two blows of 200 J (148 ft-lbf)
Hinge pin tensile load ^G	resistance	225 N (50 lbf)	225 N (50 lbf)	900 N (200 lbf)	900 N (200 lbf)
Bolt impact	impact resistance at bolt	two blows of 80 J (59 ft-lbf)	Grade 10 requirements plus two blows of 120 J (89 ft-lbf)	Grade 20 requirements plus two blows of 160 J (118 ft·lbf)	Grade 30 requirements plus two blows of 200 J (148 ft-lbf)

^ADead latch plunger must project at least 7.9 mm (0.313 in.). use 7.9-mm (0.313-in.) spacer, where required.

X2.2.6.1 For locks incorporating dead latches, the size of the latch-retaining hole in the strike shall be such that it will not be possible for both the dead latch and dead latch plunger to enter the hole together when the latch is fully extended.

X2.2.7 Bolt Pressure Resistance—When Type A and B locks, as components, and locks that are components of door assemblies are tested, the force required to depress the dead latch or dead bolt, or both, from the locked and projected position shall be a minimum of 670 N (150 lbf).

X2.2.8 *Jamb Stiffness*—When jamb, as components, and door assemblies are tested, the force required to increase the lock front-to-strike spacing by an additional 9.5 mm (3/8 in.) for Grades 10 and 20 and 13 mm (1/2 in.) for Grades 30 and 40 shall be a minimum of 6000 N (1350 lbf) for Grade 10; 8000 N (1800 lbf) for Grade 20; 16 000 N (3600 lbf) for Grade 30; and 22 000 N (4950 lbf) for Grade 40.

X2.2.9 *Knob Impact Resistance*—When Type A locks, as components, and door assemblies using Type A locks are tested, it shall not be possible to open the door after the outside knob has been subjected to one blow of 100 J (74 ft·lbf) for Grade 10; two blows of 100 J (74 ft·lbf) for Grade 20; five blows of 100 J (74 ft·lbf) for Grade 30; and ten blows of 100 J (74 ft·lbf) for Grade 40.

X2.2.10 Cylinder Core Tension Resistance—When Type A and B locks, as components, and door assemblies are tested, it shall not be possible to open the door after the cylinder core of the lock has been subjected to a tensile force of 1300 N (290 lbf) for Grade 10; 4800 N (1080 lbf) for Grade 20; and 11 000 N (2450 lbf) for Grades 30 and 40.

X2.2.11 Cylinder Tension Resistance (Grade 40 Only)—When Type A and B locks, as components, and door assemblies are tested, it shall not be possible to open the door after the lock cylinder has been subjected to a tensile load of 16 000 N (3600 lbf).

X2.2.12 *Knob Torque Resistance*—When Type A locks, as components, and door assemblies using Type A locks are tested, it shall not be possible to open the door after the outside knob has been subjected to a torque of 25 N·m (18.5 lbf·ft) for Grade 10; 50 N·m (37 lbf·ft) for Grade 20; 110 N·m (81 lbf·ft) for Grade 30; and 160 N·m (118 lbf·ft) for Grade 40. This requirement does not apply to locks in which the outside knob is free to spin when locked.

X2.2.13 Cylinder Torque Resistance (Grades 30 and 40 Only)—When Type A and B locks, as components, and door assemblies are tested, it shall not be possible to open the door after the cylinder lock has been subject to a torque of 110 N·m (81 lbf·ft) for Grade 30 and 160 N·m (118 lbf·ft) for Grade 40. This requirement does not apply to key-in-knob locks, or a lock which is not possible to apply a torque to the cylinder body by gripping its edge.

X2.2.14 Cylinder Impact Resistance (Grades 30 and 40 Only)—When Type A and B locks, as components, and door assemblies are tested, it shall not be possible to open the door after the cylinder core or body has been subjected to five blows of 100 J (74 ft·lbf) for Grade 30 and ten blows of 100 J (74 ft·lbf) for Grade 40. This requirement does not apply to key-in-knob locks.

^BBolt of latch must remain engaged in strike.

^CApplies to Type A locks only.

^DDoes not apply to key-in-knob locksets.

EDoes not apply when glazing starts at a distance of 750 mm (30 in.) or more from the lock.

Whether to use glazing impacts as described in Table X2.1 of the Appendixes under Grade 10, shall be determined by the authorities using this test procedure. Such authority may eliminate this portion of the test.

^GApplies to out-swinging doors only.

X2.2.15 *Door Impact Resistance*—When doors, as components, and door assemblies are tested, it shall not be possible to open the door following impacts at each required test location of two blows of 80 J (59 ft·lbf) for Grade 10; the Grade 10 requirement plus two blows of 120 J (89 ft·lbf) for Grade 20, the grade 20 requirement plus two blows of 160 J (118 ft·lbf) for Grade 30; and the Grade 30 requirement plus two blows of 200 J (148 ft·lbf) for Grade 40.

X2.2.15.1 When the door has one or more glazing panels with the smallest side larger than 100 mm (4 in.) or the door assembly has such a panel in the door or adjacent to the door (side light), it shall, in addition, not be possible to open the door after the glazing panel closest to the lock has been subjected to one blow of 100 J (74 ft·lbf) for Grade 10, two blows for Grade 20, five blows for Grade 30, and ten blows for Grade 40. This requirement does not apply to Grade 10 door components or door assemblies in which the glazing panel is located a distance of 750 mm (30 in.) or more from the lock.

X2.2.16 *Hinge Pin Removal Resistance*—When hinges having exposed pins, intended for use with out-swinging doors, and out-swinging door assemblies incorporating such hinges are tested, the hinge pins shall resist without removal a tensile load of 225 N (50 lbf) for Grades 10 and 20; 900 N (200 lbf) for Grades 30 and 40.

X2.2.16.1 If the hinges fail to meet the requirement in X2.2.16, but incorporate mechanical interlocks between the leaves of the hinges in the closed position, and meet the

requirements of the hinge-impact resistance test with the hinge pins removed during the test, they shall be considered to have met the requirements for hinge pin removal resistance.

X2.2.17 *Hinge Impact Resistance*—When hinges, doors, and jambs, as components, and door assemblies are tested, it shall not be possible to open the door following two blows of 80 J (59 ft·lbf) for Grade 10; the Grade 10 requirements plus two blows of 120 J (89 ft·lbf) for Grade 20; the Grade 20 requirement plus two blows of 160 J (118 ft·lbf) for Grade 30; and the Grade 30 requirement plus two blows of 200 J (148 ft·lbf) for Grade 40.

X2.2.18 *Bolt Impact Resistance*—When Type A and B locks, doors, and jamb/strike, as components, and door assemblies are tested, it shall not be possible to open the door following two blows of 80 J (59 ft·lbf) for Grade 10; the Grade 10 requirement plus two blows of 120 J (89 ft·lbf) for Grade 20; the Grade 20 requirement plus two blows of 160 J (118 ft·lbf) for Grade 30; and the Grade 30 requirement plus two blows of 200 J (148 ft·lbf) for Grade 40.

X2.3 Classification

X2.3.1 It is suggested that Table X2.1 be used with the understanding that four grades of security are established with Grade 40 being the highest and Grade 10 the lowest. Use of grade levels should be selected in accordance with the security objectives desired.

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