

Standard Test Method for Bearing Strength of Plastics¹

This standard is issued under the fixed designation D953; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon (ε) indicates an editorial change since the last revision or reapproval.

This standard has been approved for use by agencies of the U.S. Department of Defense.

1. Scope*

- 1.1 This test method covers the determination of the bearing strength of rigid plastics in either sheet form, molded form, or in thermoset pultruded form. Procedure A is applicable for tension loading and Procedure B for compression loading.
- 1.2 Test data obtained by this test method is relevant and appropriate for use in engineering design.
- 1.3 The values stated in SI units are to be regarded as the standard. The values given in parentheses are for information only.
- 1.4 This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use.

Note 1-There is no known ISO equivalent to this standard.

2. Referenced Documents

2.1 ASTM Standards:²

D618 Practice for Conditioning Plastics for Testing

D883 Terminology Relating to Plastics

D5947 Test Methods for Physical Dimensions of Solid Plastics Specimens

E4 Practices for Force Verification of Testing Machines

E6 Terminology Relating to Methods of Mechanical Testing

3. Terminology

- 3.1 *Definitions*—For definitions of technical terms pertaining to plastics used in this test method, see Terminology D883.
 - 3.2 Definitions of Terms Specific to This Standard:
- ¹ This test method is under the jurisdiction of ASTM Committee D20 on Plastics and is the direct responsibility of Subcommittee D20.10 on Mechanical Properties. Current edition approved April 1, 2010. Published June 2010. Originally approved in 1948. Last previous edition approved in 2009 as D953 09. DOI: 10.1520/D0953-10.

- 3.2.1 *bearing area*—the diameter of the hole multiplied by the thickness of the specimen.
- 3.2.2 *bearing strength*—the bearing stress at which the bearing hole is deformed 4 % of its diameter.
- 3.2.3 *bearing stress*—the applied load in newtons (or pounds-force) divided by the bearing area in mm² (or in²).
- 3.2.4 *edge distance ratio*—the distance from the center of the bearing hole to the edge of the specimen in the direction of the principal stress, divided by the diameter of the hole.
- 3.2.5 *maximum bearing stress*—the maximum load in newtons (or pounds-force) sustained by the specimen, divided by the bearing area.

4. Significance and Use

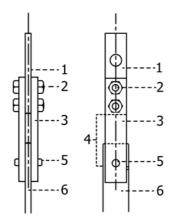
- 4.1 This bearing strength test for plastics is intended to apply in the specification of various thermoplastic or thermosetting products in sheet form where rivets, bolts, or similar fastenings are to be used in joining members or sections. It also is intended to apply wherever sheet materials of the classes indicated are required to sustain edgewise loads that are applied by means of pins or rods of circular cross section which pierce the sheet perpendicular to the surface.
- 4.2 The purpose of the test is to determine the bearing strength of the material and to show the bearing stress versus the deformation of the hole. The allowable deformation of the hole in the material should be such as to produce no looseness of joints.
- 4.3 While it is a known fact that higher strength materials will generally give higher bearing strengths, there is no satisfactory method by which bearing strength may be estimated from tensile or compressive properties of the material.
- 4.4 Before proceeding with this test method, reference should be made to the specification of the material being tested. Any test specimen preparation, conditioning, dimensions or testing parameters or combination thereof covered in the relevant ASTM materials specification shall take precedence over those in this test method. If there are no relevant ASTM material specifications then the default conditions apply.

² For referenced ASTM standards, visit the ASTM website, www.astm.org, or contact ASTM Customer Service at service@astm.org. For *Annual Book of ASTM Standards* volume information, refer to the standard's Document Summary page on the ASTM website.

³ Attention is also directed to Terminology E6.

5. Apparatus

- 5.1 Testing Machine—A properly calibrated universal testing machine that can be operated at a speed of 1.3 ± 0.3 mm $(0.05\pm0.01$ in.)/min, except that in cases of certain types of material it may be necessary to operate at a slower speed. The percentage of error of the testing machine shall be no more than ±1 % of the applied load as determined in accordance with Practices E4.
- 5.2 Tension Loading Fixture—A three-plate fixture of hardened steel similar to that shown in Fig. 1.
- 5.3 Extension Indicator—A suitable instrument reading in 0.0025 mm (0.0001 in.) for indicating the movement of the free end of the specimen with relation to the bearing pin in the tension loading fixture. A dial gauge fitted with accessories for this purpose is shown in Fig. 2.
- 5.4 Compression Loading Fixture—A type of support with a suitable bearing pin similar to Fig. 3.
- 5.5 Compression Indicator—A suitable instrument reading to 0.0025 mm (0.0001 in.) for indicating the movement of the free end of the specimen with relation to the bearing pin in the



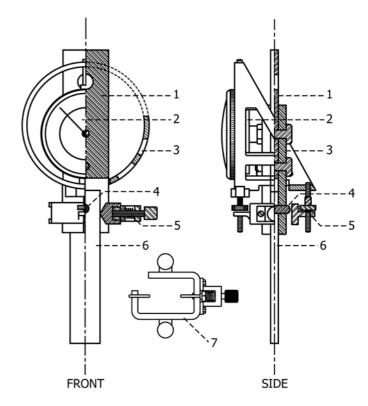
- 1—Hardened spacer plate.
- 2-6.3-mm (-in.) steel bolts in reamed holes.
- 3—Hardened side plate.
- 4—Extensometer span.
- 5-Hardened steel pin in reamed hole.
- 6—Test specimen.

Note 1—Critical dimensions are as follows:

Туре	Bearing Hole Diameter, mm (in.)	Bearing Pin Diameter, mm (in.)	Thickness of Spacer Plate, mm ^A (in.)
	3.175 + 0.025	3.150 + 0.000	3.2
	- 0.000	- 0.025	
	(0.125 + 0.0010)	(0.124 + 0.0000)	(1/8)
	- 0.0000)	- 0.0010)	
II	6.350 + 0.025	6.325 + 0.000	6.3
	- 0.000	- 0.025	
	(0.250 + 0.0010)	(0.249 + 0.0000)	(1/4)
	- 0.0000)	- 0.0010)	

 $^{^{}A}$ The spacer plate shall be shimmed to a thickness of 0.025 to 0.125 mm (0.001 to 0.005 in.) greater than the specimen under test.

FIG. 1 Steel Tension Loading Fixture



- 1—Spacer plate.
- 2—Dial gauge.
- 3—Double foot ring mounted on spindle of dial gauge.
- 4—Bearing pin.
- 5—Yoke mounted on specimen.
- 6-Test specimen.
- 7-Plan view of yoke.

FIG. 2 Tension Loading Assembly

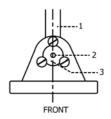
compression loading fixture. A suggested dial gauge assembly for this purpose is shown in Fig. 4.

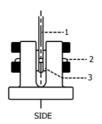
6. Test Specimens

6.1 The test specimens shall conform to the dimensions shown in Fig. 5. A size of test specimen shall be chosen that most nearly conforms to production requirements of the material and the type of loading under consideration. The thicker specimens with the larger bearing hole are likely to give the more precise results, although it is advantageous to use the thinner specimens with the smaller bearing hole in testing certain relatively brittle plastics because they are less likely to fail prematurely. The specimen may be machined from sheet or molded to finished size. The bearing hole shall be located as shown in Fig. 5. It shall be drilled undersized and reamed to size as indicated. The hole shall be clean and smooth with sharp edges but not polished. It is suggested that the reaming operation be done in the drill press by hand without the use of a jig.

7. Number of Test Specimens

7.1 At least five specimens shall be tested for each sample in the case of isotropic materials.





- 1—Test specimen.
- 2-Hardened steel pin.
- 3-Hardened thrust bushing.

Note 1—Critical dimensions are as follows:

Туре	Bearing Hole Diameter, mm (in.)	Bearing Pin Diameter, mm (in.)	Minimum Clear- ance Be- tween Bushings, mm (in.)
I	3.175 + 0.025	3.150 + 0.000	2.8
	- 0.000	- 0.025	
	(0.125 + 0.0010)	(0.124 + 0.0000)	(7/64)
	- 0.0000)	- 0.0010)	
II	6.350 + 0.025	6.325 + 0.000	6.0
	- 0.000	- 0.025	
	(0.250 + 0.0010)	(0.249 + 0.0000	(15/64)
	- 0.0000)	- 0.0010)	

FIG. 3 Steel Compression Loading Fixture

- 7.2 Ten specimens, five perpendicular to and five parallel with the principal axis of anisotropy, shall be tested for each sample in case of anisotropic materials.
- 7.3 Specimens that break at some obvious flaw shall be discarded and retests made, unless such flaws constitute a variable the effect of which is being studied.

8. Conditioning

- 8.1 Conditioning—Condition the test specimens in accordance with Procedure A of Practice D618, unless otherwise specified by contract or the relevant ASTM material specification. Conditioning time is specified as a minimum. Temperature and humidity tolerances shall be in accordance with Section 7 of Practice D618 unless specified differently by contract or material specification.
- 8.2 Test Conditions—Conduct tests at the same temperature and humidity used for conditioning with tolerances in accordance with Section 7 of Practice D618 unless otherwise specified by contract or the relevant ASTM material specification.

9. Measurement of Dimensions

9.1 Measure the width and thickness of the conditioned test specimen to the nearest 0.025 mm (0.001 in.) at the bearing hole. Also measure the diameter of the bearing hole and the distance from the center of the bearing hole to the edge of the specimen in the direction of the principal stress to the nearest 0.025 mm (0.001 in.). All measurements to be made using the applicable test methods in accordance with Test Method D5947.

10. Speed of Testing

10.1 The mean rate of crosshead travel in the testing of specimens shall not exceed 1.3 ± 0.3 mm (0.05 ± 0.01 in.)/min. In any case the crosshead movement shall be slow enough so that deflection gauge readings can be made accurately.

11. Procedure

- 11.1 The choice of either Procedure A for tension loading (11.2) or Procedure B for compression loading (11.3) is optional, but it should be recognized that Procedure B gives higher bearing strength values than Procedure A on the same material. Test specimens according to both Procedures A and B if a complete specification of bearing strength is required.
- 11.2 Procedure A for Tension Loading—Mount the specimen to be tested in the tension loading fixture and attach a deformation indicator. If a dial gauge (Fig. 2) is used, adjust the yoke so that contact is made with the specimen at the level indicated in Fig. 1. Exception is taken in the case of those thermoplastic materials which exhibit extended plastic flow. Such specimens tend to "neck down" in the region of the bearing hole, and it is necessary to mount the yoke 12.7 mm (½ in.) below the normal position indicated in A, Fig. 1, so that it will not slip during test.
- 11.3 Procedure B for Compression Loading—Mount the specimen to be tested in the compression loading fixture and load through a flat, hardened compression plate. Adjust the clearance between the thrust bushings of the loading fixture such that their contact with the specimen is sufficient to support it in a vertical position without binding. Clamp the hardwood cheek blocks in place and attach the deformation indicator (see Fig. 4).
- 11.4 Details Common to Procedures A and B—Take care in aligning the long axis of the specimen with the center line of the testing fixture. Load the specimen at the prescribed rate of crosshead travel and take deformation readings. In case autographic recording is not available, record the load sustained by the specimen for every 0.0127-mm (0.0005-in.) deformation up to a total deformation of 4 % of the bearing hole diameter. Continue the test until maximum load is sustained and the corresponding deformation of the bearing hole is recorded.

12. Calculation

- 12.1 Plot the load deflection curve for each specimen.
- 12.2 Use a template, as described in the Appendix, to determine the load at 4 % hole deformation.
 - 12.3 Calculate the bearing strength as follows:

$$S_b = P/(td) \tag{1}$$

where:

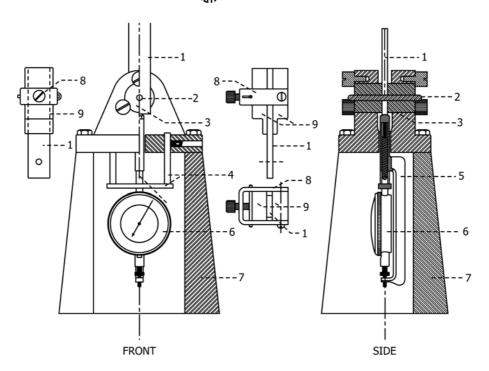
 S_h = bearing strength, MPa (or psi),

P = bearing load at 4 % hole deformation, N (or lbf),

d = bearing hole diameter, mm (or in.), and

t = specimen thickness, mm (or in.).

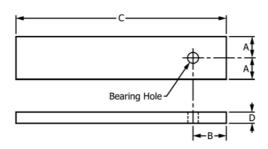
12.4 Calculate the arithmetic mean of the observations and report the result to three significant figures.



- 1—Test specimen.
- 2—Bearing pin.
- 3—Thrust bushings.
- 4—Hanger for dial gauge.
- 5—Spring-supported thrust member of transfer deformation of specimen to dial gauge foot.

- 6—Dial gauge.
- 7—Pedestal support.
- 8-Clamp for cheek blocks.
- 9—Hard maple cheek blocks to stabilize test specimen.

FIG. 4 Compression Loading Assembly



Type	Dimensions, mm ^A (in.)		Ream Hole		
	Α	В	С	D	to
1	11.913 ± 0 .127	19.050± 0 .127	120.6	3.2	3.200 ± 0 .025
	(0.469 ± 0.005)	(0.750 ± 0.005)	(43/4)	(1/8)	(0.126 ± 0.001)
II	11.913 ± 0 .127	19.050 ± 0 .127	120.6	6.4	6.375 ± 0 .025
	(0.469 ± 0.005)	(0.750 ± 0.005)	(43/4)	(1/4)	(0.251 ± 0.001)

All fractional dimensions shall be held to ± 0.40 mm ($\frac{1}{64}$ in.) tolerance.

Edge distance ratio = B/hole diameter

FIG. 5 Dimensions of Bearing Strength Test Specimens

12.5 Calculate the standard deviation of each set of observations and record to two significant figures.



13. Report

- 13.1 Report the following information:
- 13.1.1 Complete identification of the material tested, including type, source, manufacturer's code number, form, principal dimensions, and previous history,
 - 13.1.2 Direction of cutting and loading specimens,
- 13.1.3 Conditioning procedure and environmental conditions under which the tests were conducted,
- 13.1.4 Length, width, and thickness of specimen, in millimetres (or inches),
 - 13.1.5 Diameter of bearing hole, in millimetres (or inches),
 - 13.1.6 Edge distance ratio,
- 13.1.7 Mean rate of crosshead motion in millimetres (or inches) per minute,
- 13.1.8 Bearing strength in Megapascals (or pounds-force per square inch), stating whether Procedure A for tension loading or Procedure B for compression loading was used,
- 13.1.9 Maximum bearing stress in Megapascals (or poundsforce per square inch), stating whether Procedure A or Procedure B was used; thermoset pultruded shapes typically report only the maximum value, and

13.1.10 The test method number and published/revision date

14. Precision and Bias

- 14.1 Attempts to develop a comprehensive interlaboratory precision and bias statement for this test method have not been successful because of the small number of laboratories using this test method. However, limited precision data from one laboratory on one material utilizing a single operator, a single apparatus, on a single day and replicate runs of the material has been provided as follows: Determinations were made on two sets of ten individual specimens to provide two test results. The coefficient of variation of the two test results averaged 4.9 % with a difference of 0.3 % between results.
- 14.2 There are no recognized standards to estimate the bias of this test method. Anyone wishing to participate in the development of precision and bias data should contact the chairman, Subcommittee D20.10 (Section D20.10.01), ASTM International, 100 Barr Harbor Drive, West Conshohocken, PA 19428–2959.

15. Keywords

15.1 bearing strength; compression strength; plastics

APPENDIX

(Nonmandatory Information)

X1. DETERMINATION OF BEARING LOAD

- X1.1 Bearing strength has been defined as the bearing stress at which the bearing hole is deformed a given percentage (4 %) of the hole diameter, and is by definition, sensitive to zero load errors. The following procedure for determining bearing strength has been found to eliminate this ambiguity. It is insensitive to zero load errors, and as a result improves the precision of the bearing strength measurements.
- X1.2 The method is best illustrated by Fig. X1.1. Given the bearing load deflection curve, *ABC*, the tangent is determined at a point, *B*, such that when the tangent is projected through the point, *O*, on the zero load axis, the distance between *O* and *D* shall be equal to 4% of the bearing hole diameter.
- X1.3 A template to facilitate the determination of point Bon the curve is shown in Fig. X1.2. It is designed to fit the coordinate paper upon which the load-deformation curve is drawn in such a way that a" 4 % line" on the template is established at a distance from the origin, O, equal to 4 % of the bearing hole diameter. It consists of a thin rigid sheet of transparent plastic upon which the rectangular coordinates are ruled. A strip of transparent plastic is mounted on the sheet so as to rotate about point O. The strip is provided with a reference center line passing through the point of rotation.
- X1.4 In practice, the deformation axis of the template is superimposed on the zero load axis of the load-deformation curve. This can best be done with the aid of a drawing board

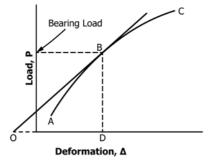


FIG. X1.1 Illustration of Method of Determining Bearing Strength from Bearing Load-Deformation Curve

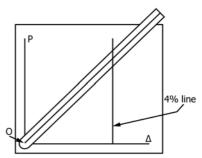


FIG. X1.2 Template for Determining Point Bon Bearing Load-Deformation Curve

and a parallel straightedge. The template is then slid to right or left while in superposition until the rotating arm can be made tangent to the load-deformation curve at its intersection with the 4 % line. The intersection is the point *B*on the curve in Fig. X1.1; *B*is projected horizontally to the load axis and the bearing load is read.

SUMMARY OF CHANGES

Committee D20 has identified the location of selected changes to this standard since the last issue (D953 - 09) that may impact the use of this standard. (April 1, 2010)

(1) Removed ASTM D4066 from 2.1.

(2) Revised Section 8.

Committee D20 has identified the location of selected changes to this standard since the last issue (D953 - 02) that may impact the use of this standard. (November 15, 2009)

- (1) Subsection 1.1 was adjusted to included thermoset pultruded shapes.
- (2) ASTM D4000 was eliminated from 2.1 and ASTM D5947 was added.
- (3) The humidity was adjusted in (8.1 and 8.2).
- (4) ASTM D5947 was added to 9.1.
- (5) Subsection 13.1.9 was adjusted stating the standard practice for thermoset pultruded shapes.

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