

**Designation: D7649 − 10 (Reapproved 2017)**

# **Standard Test Method for Determination of Trace Carbon Dioxide, Argon, Nitrogen, Oxygen and Water in Hydrogen Fuel by Jet Pulse Injection and Gas Chromatography/Mass Spectrometer Analysis<sup>1</sup>**

This standard is issued under the fixed designation D7649; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon  $(\varepsilon)$  indicates an editorial change since the last revision or reapproval.

## **1. Scope**

1.1 This test method describes a procedure primarily for the determination of carbon dioxide, argon, nitrogen, oxygen and water in high pressure fuel cell grade hydrogen by gas chromatograph/mass spectrometer (GC/MS) with injection of sample at the same pressure as sample without pressure reduction, which is called "Jet Pulse Injection". The procedures described in this method were designed to measure carbon dioxide at 0.5micromole per mole (ppmv), Argon 1 ppmv, nitrogen 5 ppmv and oxygen 2 ppmv and water 4 ppmv.

1.2 The values stated in SI units are standard. The values stated in inch-pound units are for information only.

1.3 The mention of trade names in standard does not constitute endorsement or recommendation for use. Other manufacturers of equipment or equipment models can be used.

1.4 *This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use.*

1.5 *This international standard was developed in accordance with internationally recognized principles on standardization established in the Decision on Principles for the Development of International Standards, Guides and Recommendations issued by the World Trade Organization Technical Barriers to Trade (TBT) Committee.*

## **2. Referenced Documents**

2.1 *Other Standards:*

SAE TIR J2719 Information Report on the Development of a Hydrogen Quality Guideline for Fuel Cell Vehicles April 2008<sup>2</sup>

### **3. Terminology**

3.1 *Definitions of Terms Specific to This Standard:*

3.1.1 *absolute pressure—*pressure measured with reference to absolute zero pressure, usually expressed as kPa, mm Hg, bar or psi. All the pressures mentioned in this method are absolute pressure.

3.1.2 *constituent—*A component (or compound) found within a hydrogen fuel mixture.

3.1.3 *contaminant—*impurity that adversely affects the components within the fuel cell system or the hydrogen storage system by reacting with its components. An adverse effect can be reversible or irreversible.

3.1.4 *dynamic calibration—*calibration of an analytical system using calibration gas standard generated by diluting known concentration compressed gas standards with hydrogen, as used in this method for carbon dioxide, argon, nitrogen and oxygen [\(7.3](#page-4-0) and [7.4\)](#page-4-0).

3.1.5 *extracted ion chromatogram (EIC)—*a GC/MS chromatogram where a selected ion is plotted to determine the compound(s) of interest.

3.1.6 *fuel cell grade hydrogen—*hydrogen satisfying the specifications in SAE TIR J2719.

3.1.7 *hydrogen fuel—*hydrogen to be tested without compositional change due to sample introduction, etc.

3.1.8 *jet pulse injection—*high pressure hydrogen fuel sample is introduced instantaneously at the same pressure into GC/MS.

3.1.9 *relative humidity—*ratio of actual pressure of existing water vapor to maximum possible pressure of water vapor in the atmosphere at the same temperature, expressed as a percentage.

3.1.10 *response factor (RF)*—-the amount in volume ( $\mu$ L) of an analyte divided by the EIC area of the analyte.

3.1.11 *static calibration—*calibration of an analytical system using standards in a matrix, state or manner different than the samples to be analyzed, as used in this method for water concentration in hydrogen.

3.2 *Acronyms:*

<sup>&</sup>lt;sup>1</sup> This test method is under the jurisdiction of ASTM Committee [D03](http://www.astm.org/COMMIT/COMMITTEE/D03.htm) on Gaseous Fuels and is the direct responsibility of Subcommittee [D03.14](http://www.astm.org/COMMIT/SUBCOMMIT/D0314.htm) on Hydrogen and Fuel Cells.

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<sup>2</sup> Available from SAE International (SAE), 400 Commonwealth Dr., Warrendale, PA 15096-0001, http://aerospace.sae.org.

<span id="page-1-0"></span>3.2.1 *FCV—*fuel cell vehicle.

3.2.2 *PEMFC—*proton exchange membrane fuel cell.

## **4. Summary of Test Method**

4.1 The simultaneous analysis of carbon dioxide, argon, nitrogen, oxygen and water at 0.5 – 5 ppmv (micromole per mole) in hydrogen fuel samples from fueling stations is challenging due to high hydrogen fuel sample pressure and possible contaminations from ambient air.

4.2 In this method, a small stainless steel loop is initially pressurized with high pressure hydrogen standard or sample without any pressure regulation or restriction ("Sample Loop Pressurization", Fig. 1). The hydrogen in the loop is then released entirely as a "jet pulse" into a T-union which splits sample into a 0.25  $\mu$ m ID 30 m long capillary column and an electronic flow controller (EFC) used to vent excess hydrogen to the atmosphere ("Jet Pulse Injection", [Fig. 2\)](#page-2-0). Less than 1% of hydrogen enters the capillary column with the remaining sample venting to atmosphere through EFC. As demonstrated in [Appendix X1,](#page-6-0) the hydrogen volume "jet pulse injected" into the capillary column is a constant volume and independent of the sample loop pressure when the sample loop pressure is over 90 psi. Therefore, the constant hydrogen volume from standards or samples is GC/MS analyzed in regardless of standard or sample pressures.

4.3 Jet pulse injected volume into the capillary column is approximate 100  $\mu$ L (In [Appendix X1,](#page-6-0) this volume is calculated to be 115µL under the analytical conditions described in [Appendix X1\)](#page-6-0). When a 2-mL of sample loop is pressurized to 200 psi, the hydrogen in the loop is  $(200 \text{ psi}/14.7 \text{psi}) \times 2 \text{ mL}$ or 27 mL. Hence, 99.5% of the hydrogen sample vents to atmosphere. This type of "Jet Pulse Injection" has been found acceptable for the analysis of high pressure hydrogen fuel sample since the hydrogen volume injected is independent of the pressures of hydrogen standards or samples. Consequently it is unnecessary to regulate standards and hydrogen samples to the same pressure. In addition to possible trace leaks or air trapped inside, regulators are not recommended as moisture on the regulator surface can be released into the sample resulting in a high moisture determination.

4.4 A mass spectrometer provides sensitive and selective detection towards carbon dioxide, argon, nitrogen, oxygen and water.

### **5. Significance and Use**

5.1 Low operating temperature fuel cells such as proton exchange membrane fuel cells (PEMFCs) require high purity hydrogen for maximum performance. The following are the reported effects (SAE TIR J2719) of the compounds determined by this test method.

5.2 *Carbon Dioxide* ( $CO<sub>2</sub>$ ), acts largely as a diluent, however in the fuel cell environment  $CO<sub>2</sub>$  can be transformed into CO.

5.3 *Water*  $(H_2O)$ *,* is an inert impurity, as it does not affect the function of a fuel cell stack; however, it provides a transport mechanism for water-soluble contaminants, such as Na<sup>+</sup> or K<sup>+</sup>. In addition, it may form ice on valve internal surface at cold weather or react exothermally with metal hydride used as hydrogen fuel storage.

5.4 *Inert Gases (N<sub>2</sub> and Ar)*, do not normally react with a fuel cell components or fuel cell system and are considered diluents. Diluents can decrease fuel cell stack performance.

5.5  $Oxygen (O<sub>2</sub>)$ , in low concentrations is considered an inert impurity, as it does not adversely affect the function of a fuel cell stack; however, it is a safety concern for vehicle on board fuel storage as it can react violently with hydrogen to generate water and heat.



# **Figure 1 Sample Loop Pressurization**

**FIG. 1 Sample Loop Pressurization**

# **Figure 2 Jet Pulse Injection**

<span id="page-2-0"></span>

# **6. Apparatus**

6.1 *Mass Spectrometer (MS)—*The MS can perform mass calibration with a scanning range from m/e 15 to 650. The background peak intensities of water, nitrogen, argon, oxygen and carbon dioxide in the mass spectrum of FC-43 (perfluorotributylamine), used for mass calibration, should be less than 10% of m/e 69 to demonstrate a background acceptable for the determination of these analytes before beginning sample analysis. All analytes determined according to this method have a molecular mass less than 44 amu; therefore, the mass scanning range of m/e 15 to 50 is typically used.

6.2 *Data System—*A computer or other data recorder loaded with appropriate software for data acquisition, data reduction, and data reporting and possessing the following capabilities is required:

6.2.1 Graphic presentation of the total ion chromatogram (TIC) and extracted ion chromatogram (EIC).

6.2.2 Digital display of chromatographic peak areas.

6.2.3 Identification of peaks by retention time and mass spectra.

6.2.4 Calculation and use of response factors.

6.2.5 External standard calculation and data presentation.

6.3 *Gas chromatography (GC)—*Chromatographic system capable of obtaining retention time repeatability of 0.05 min (3 s) throughout the analysis.

6.3.1 *Interface with MS—*A heated interface connecting the GC column to the MS ion source.

6.3.2 *GC Column—*A 0.25mm ID 30m 0.25 µm film thickness DB-5 column has been successfully used to perform this analysis. Other capillary columns may be used provided chromatographic peaks do not significantly tail. One end of the GC column is connected to the Jet Pulse Split [\(6.4.5\)](#page-3-0) and the other end is connected to the ion source inlet of a mass spectrometer.

6.3.3 *Carrier Gas—*Ultra high purity hydrogen is used as carrier gas. Use of helium carrier gas results in unacceptable broadening of the water chromatographic peak. An example of water peaks is shown in [Fig. 3.](#page-3-0)

6.3.4 *GC Injector—*An injector port with a glass insert and a septum is connected through a  $\frac{1}{16}$  in. OD stainless steel tubing to a jet pulse split  $(6.4.5)$  in the inlet system  $(6.4)$ . The injector temperature is set to at 220°C to ensure that all water vapor in injected ambient air are not condensed in the injector. The GC column and total split flow rate are electronically set at 1.5 and 75 mL/min, respectively. The GC total split flow includes a GC septum purge flow of 3mL/min [\(Fig. 1](#page-1-0) and Fig. 2) and GC injector split flow of 72mL/min.

6.4 *Inlet System—*A system introduces high pressure samples or standards into GC/MS for analysis. The sample or standard enter the inlet system through "Sample Loop Pressurization" [\(Fig. 1\)](#page-1-0) and then leave the inlet system to GC/MS through "Jet Pulse Injection" (Fig. 2). While the inlet system is in "Sample Loop Pressurization", the sample loop [\(6.4.4\)](#page-3-0) is pressurized directly with hydrogen samples or calibration standards without pressure regulation or flow restriction. Afterwards, a six-port sample valve (6.4.1) switches the inlet system to "Jet Pulse Injection", in which pressurized hydrogen in the sample loop is released instantaneously onto the GC column (6.3.2) and jet pulse split [\(6.4.5\)](#page-3-0). Since the sample pressure is high, all parts of the inlet system must be capable of working at pressures of 1500 psi or higher.

6.4.1 *Six Ports Valve—*This valve is used to switch from "Sample Loop Pressurization" [\(Fig. 1\)](#page-1-0) to "Jet Pulse Injection" (Fig. 2).

6.4.2 *Samples and Calibration Standards—*All calibration standards and samples are prepared or collected in 1800 psi pressure rated containers with a DOT 3A1800 label (United Stated Department of Transportation mandated label) affixed to the outside surface. All calibration standards and samples are

<span id="page-3-0"></span>

**FIG. 3 m/e18 Extracted Ion Chromatogram of Sample Analysis with Co-Injection of Ambient Air**

connected to the inlet system before beginning an analytic sequence to minimize the potential for air or moisture contamination due to addition or replacement of standard or sample containers.

6.4.3 *Vacuum Pump—*an oil vacuum pump that can pump down to 50 mtorr or less.

6.4.4 *Sample Loop—*stainless steel tubing with1⁄16 in. OD and 2 mL inside volume. Both ends of the sample loop are connected to a six port valve [\(6.4.1\)](#page-2-0).

6.4.5 *Jet Pulse Split—*a T-union connects the following three portions.

6.4.5.1 Six port valve [\(6.4.1\)](#page-2-0)

6.4.5.2 Inlet of GC column [\(6.4.2\)](#page-2-0)

6.4.5.3 Inlet of an electronic flow controller (EFC) with its outlet to ambient air. The flow rate of this EFC is always electronically set at 150mL/min to vent most of the GC injector split flow (72mL/min) during "Sample Loop Pressurization" [\(Fig. 1\)](#page-1-0) and released hydrogen from pressurized sample loop in "Jet Pulse Injection" [\(Fig. 2\)](#page-2-0).

6.4.6 *Digital Vacuum Gauge—*capable of measuring absolute pressure at vacuum range 0 to 12,000 milli-torr (mtorr or  $10^{-3}$  torr). For the vacuum range from 0 to 1000 mtorr, the accuracy is  $\pm 10\%$  or $\pm 10$  mtorr, whichever is larger.

6.4.7 *Digital Pressure Gauges—*Two types of digital pressure gauges are required. A pressure gauge 0 to 1000 psig is used to measure sample and standard final pressure. Another digital pressure gauge in the low and narrow pressure range, such as 0 to 2000 torr, is used to measure the pressure of pure gases in initial standard preparation.

6.4.8 *Pressure Regulator—*A 10,000 psi pressure regulator is used to reduce UHP hydrogen pressure to approximate 400 psi for calibration standard preparation. It is also used to pressurize the inlet system during method blank analysis, and during inlet system flushing.

#### **7. Reference Standards**

7.1 Typical reference standards are listed in [Fig. 1.](#page-1-0) Two standards prepared in helium containing 100 ppmv  $O_2$  and 100 <span id="page-4-0"></span>ppmv  $N_2$ , are commercial available. Remaining standards listed in [Fig. 1](#page-1-0) are prepared as per below.

7.2 0.5% CO<sub>2</sub>, Ar, N<sub>2</sub> and O<sub>2</sub> in hydrogen—An evacuated 1-L cylinder is connected to four pressure-regulated compressed gas cylinders containing reagent or UHP grade  $CO<sub>2</sub>$ , Ar,  $N_2$  and  $O_2$ . The system is evacuated to less than 500 mtorr with all the regulators opened and the main cylinder valves closed. With the system isolated from vacuum pump, the 1-L cylinder valve is opened and 100 torr of each target compound from the compressed gas cylinders is expanded into the system and 1-L cylinder. The 1-L cylinder is then pressured using UHP hydrogen to 390 psi, or 390/14.7  $\times$  760 = 2.02  $\times$  10<sup>4</sup> torr. The concentration of each target compound is 100 torr/ $(2.02 \times 10^4$ torr) =  $0.5$  %. This standard can be used as a co-injection standard (9.3.3) and further diluted to prepare a 5 ppmv standard (7.3). The UHP hydrogen used for preparation of both  $0.5\%$  (7.2) and 5 ppmv standards (7.3) are free from CO<sub>2</sub>, Ar,  $N_2$  and  $O_2$  by this test method.

7.3 *5ppmv CO2, Ar, N2 and O2 in hydrogen:*

7.3.1 Close all the valves in [Fig. 1](#page-1-0) except leave Valves 2, 4 and both valves of the cylinder labeled with "5 ppmv  $CO<sub>2</sub>$ , Ar, N2& O2 Standard in H2" open. Evacuate the "Standard Section" in [Fig. 1](#page-1-0) to less than 100 mtorr.

7.3.2 Close Valve 2 and pressurize the "Standard Section" in [Fig. 1](#page-1-0) to above 100 psi by UHP hydrogen.

7.3.3 Open Valve 2 and pump the "Standard Section" in [Fig.](#page-1-0) [1](#page-1-0) to less than 100 mtorr and then close it.

7.3.4 Close the valve of the standard cylinder close to the 0.5% standard and open the valve of the cylinder containing the  $0.5\%$  CO<sub>2</sub>, Ar, N<sub>2</sub> and O<sub>2</sub> in hydrogen for about 10 s and then close it.

7.3.5 Open the valve of the standard cylinder close to the 0.5% standard for 5 s and close it. Measure the pressure by the digital pressure gauge in [Fig. 1.](#page-1-0)

7.3.6 Pressurize the "Standard Section" in [Fig. 1](#page-1-0) to less than 400 psi with UHP  $H<sub>2</sub>$  with 10,000 psi pressure regulator and close the other valve of the standard cylinder.

7.3.7 The concentration of the standard is calculated as following. If the pressure in 7.3.5 is 20 torr and final pressure 385 psi (7.3.6), the concentration is (20 torr × (0.50/100)/(385/  $14.7 \times 760$ ) = 5.0 ppmv.

7.3.8 Low concentration standards other than 5 ppmv can be prepared and used as calibration standards.

7.4 *Detection Limit Standards of Oxygen and Nitrogen—* ~2 ppmv  $O_2$  and  $\sim$ 5 ppmv  $N_2$  in hydrogen. The preparation of these two standards from commercially available 100 ppmv  $O_2$ and  $N<sub>2</sub>$  in helium, respectively, is in the same as that for 5ppmv  $CO<sub>2</sub>$ , Ar, N<sub>2</sub> and  $O<sub>2</sub>$  in hydrogen (7.3). The detection limit standards are analyzed in each analytical sequence to validate acceptable detection of oxygen and nitrogen at the detection limit.

# **8. Preparation of Apparatus**

8.1 *GC/MS—*Place in service in accordance to the manufacturer's instructions. Perform daily mass calibration using FC-43. As stated in [6.1,](#page-2-0) each of the peak intensities of m/e 18, 28, 29, and 32 should be less than 10% of m/e 69 in the mass spectrum of FC-43 used for mass calibration. In order to achieve this condition, the GC column flow rate of GC/MS system should be set at a high flow rate, such as, 2mL/min, while the system is in standby mode to remove any air in the carrier gas line. In addition, when any air may be introduced into the carrier gas system, such as when changing the hydrogen carrier gas tank, the GC total split flow rate is set at 100mL/min for an hour to rapidly remove air in the carrier gas line.

# **9. Procedure**

9.1 The detailed procedures used to perform jet pulse injection followed by GC/MS analysis are listed below. The procedures are split into two sections – sample loop pressurization [\(Fig. 1\)](#page-1-0) and jet pulse injection/GC/MS analysis [\(Fig. 2\)](#page-2-0).

9.2 *Sample Loop Pressurization (*[Fig. 1](#page-1-0)*):*

9.2.1 With all the valves closed in [Fig. 1,](#page-1-0) Valves 2, 3 and 4 are opened and pumped down including both standard and sample sections to less than 100 mtorr. If this pressure cannot be lowered to at least 100 mtorr, perform a leak check.

9.2.2 Open Valves 1 and 5 and close Valves 2 and 4, followed with pressurization of the sample loop with UHP hydrogen to  $300 - 400$  psi.

9.2.3 Open Valve 4 only to pump down the entire system to less than 10 torr and then open Valve 2 to less than 1 torr. Simultaneously, measure the flow rate from EFC of the jet pulse split [\(6.4.5\)](#page-3-0); this should be close to 72 mL/min.

9.2.4 Close both Valves 2 and 4 and pressurize the entire system with standard or sample and measure the loop pressure using a digital high pressure gauge as depicted in [Fig. 1.](#page-1-0) For safety reason, it is recommended that the loop pressure not be over 500 psi. For the method blank analysis using UHP hydrogen, the loop should be pressurized to approximate 400 psi.

9.3 *Jet Pulse Injection/GC/MS Analysis (*[Fig. 2](#page-2-0)*):*

9.3.1 Switch the six port valve to "Jet Pulse Injection" [\(Fig.](#page-2-0) [2\)](#page-2-0) and simultaneously start GC/MS acquisition.

9.3.2 Measure the GC injector split flow rate, which should be 0 mL/min since most injector split flow vents out from the jet pulse split [\(6.4.5\)](#page-3-0). Measure the GC septum purge flow, which should be approximate 3 mL/min.

9.3.3 After 1.5 minutes from the start of GC/MS acquisition, the  $0.5\%$  CO<sub>2</sub>, Ar, N<sub>2</sub> and O2 in hydrogen [\(6.2\)](#page-2-0),  $1\%$  CO<sub>2</sub> in nitrogen or ambient air is co-injected three times and 18 seconds apart. The volume and time interval of co-injections can be varied, for example, those in [Table X1.1](#page-7-0) of [Appendix X1.](#page-6-0) The reasons for co-injection are listed under "Co-Injection" of [Appendix X1.](#page-6-0) Each GC/MS analysis is completed in less than 5 minutes.

9.3.4 A typical analytic sequence is shown in [Table 1.](#page-5-0) As shown in this table, except for the method blank, each standard or sample is analyzed consecutively three times. The three analyses of each standard or sample should generate the same extracted ion chromatogram (EIC) areas of target compounds within analytical error, as described in [Appendix X1;](#page-6-0) this demonstrates that the jet pulse injected the same volume of each hydrogen standard or sample. The EIC of target compounds are m/e44 for  $CO_2$ , 40 Ar, 29 N<sub>2</sub>, 32 O<sub>2</sub> and 18 H<sub>2</sub>O.

**TABLE 1 Analytical Sequence***<sup>A</sup>*

<span id="page-5-0"></span>

 $^A$  Percentage relative humidity and atmospheric pressure are measured during each analysis for water concentration calculation by [Eq](#page-6-0) and Eq. The co-injection starts after 1.5 minutes from the beginning of GC/MS acquisit volumes and numbers of co-injections at different time intervals can be used, such as the example in [Table X1.1](#page-7-0) in [Appendix X1.](#page-6-0)

**TABLE 2 Example of GC/MS Operating Parameters**



In general, the variation of EIC areas of 5 ppmv  $CO<sub>2</sub>$ , Ar, N<sub>2</sub> and  $O_2$  in hydrogen [\(7.3\)](#page-4-0) in three consecutive analyses in the analytical sequence (Table 1) are less than  $10\%$  RSD for  $CO<sub>2</sub>$ and Ar. For  $N_2$  and  $O_2$ , the %RSD should be less than 30% due to the baseline noise of GC/MS analysis.

#### **10. Calculation**

10.1 The concentrations of carbon dioxide, argon, nitrogen and oxygen in hydrogen sample can be calculated from the EIC areas of carbon dioxide at m/e44, argon m/e40, nitrogen m/e29, and oxygen m/e32 using [Eq](#page-6-0) . See [Fig. 4.](#page-6-0)

10.2 The jet pulse injected volume described in [9.3.4](#page-4-0) can be calculated from the RF of co-injection [\(Eq](#page-6-0) ) and the EIC area of jet pulse injected 5 ppmv standard [\(7.2\)](#page-4-0), as shown in [Eq](#page-6-0) . The split ratio is the ratio of sum of the flow rates of the jet pulse split, GC injector split and injector septum purge over the column flow rate. In general, it is close to 50. Since air contains 0.934% of argon, the RF of argon can be also calculated from ambient air co-injection.

10.3 The concentration of water in hydrogen cannot be calculated from [Eq](#page-6-0) since a water standard at low ppmv in hydrogen cannot be prepared or purchased commercially. However, the relative humidity of ambient air can be precisely measured by humidity meter; therefore, a known amount of water in co-injected ambient air of a known volume can be used as a calibration standard for water. The percentage of water in ambient air is relative humidity times the saturated water vapor pressure in mm Hg divided by atmospheric pressure in mm Hg. At 25°C, the atmosphere is saturated with water vapor when the partial pressure of water is 23.756 torr. The RF of water at 25C is calculated in [Eq](#page-6-0) and water concentration in a hydrogen sample according to [Eq](#page-6-0) . Examples for all calculations, except [Eq](#page-6-0) , in Section 10 are contained in [Appendix X1.](#page-6-0) The 2µL ambient air injection is

<span id="page-6-0"></span>Average EIC Area of Jet Pulse Injected Sample Average EIC Area of Jet Pulse Injected Sample<br>Average EIC Area of Jet Pulse Injected Standard × Standard Concentration … (1) Sample Concentration =

Response Factor (RF) =  $\frac{\text{Volume}(\mu\text{L})$  of Co Injected Standard × Concentration of Standard ... (2) Split Ratio × Peak Area of EIC Area

*Jet Pulse Injected Volume* ( $\mu$ L) =  $\frac{\text{EIC Area of Jet Pulse Injected 5 ppmv Standard (7.3) × RF}}{1,000,000}$  (Concentration of 5 ppmv Standard)

*RF of H*<sub>2</sub>O =  $\frac{23.756 \text{ torr}}{5 \text{plit Ratio} \times \text{Area of } \frac{m}{e} 18 \text{ of } H_2O}$  in coinjected air 23.756 torr

Average 
$$
\frac{m}{6}
$$
 18 Area of Jet Pulse Injected H<sub>2</sub> Sample × *RF of H<sub>2</sub>*(

Jet Pulse Injected Hydrogen Volume in  $\mu$  as calculated in (3)  $\times$  1,000,000 ... (5)

Detection Limit of water = 
$$
\frac{2 \mu L \times 0.25 \times 23.756 \text{ torr}}{50 \times 100 \mu L \times 760 \text{ torr}} \times 1,000,000 = 3.1 \text{ ppm} \cdot \cdot \cdot (6)
$$

\nFIG. 4 Equations

used to determine the detection limit of water. The jet injected volume is in general 100µL under the conditions in [Fig. 1.](#page-1-0) If the relative humidity is 25%, atmospheric pressure 760 torr and split ratio [\(10.2\)](#page-5-0) 50, the detection limit of water is 3.1ppmv, as shown in Eq .

 $H<sub>2</sub>O$  Conc. (ppmv) in sample = -

# **11. Precision and Bias**

11.1 *Precision—*The estimate of the repeatability for impurities present in  $H<sub>2</sub>$  fuel gas, is based upon the standard deviation of 14 successive test results multiplied by a factor of 2.77 which represent that difference between two such single and independent results as would be exceeded in the long run in only 1 case in 20 in the normal and correct operation of the test method result in the following:



11.2 The bias for each component analyzed will be determined by experimental results within five years of the release of this standard.

### **12. Keywords**

12.1 jet pulse injection; high pressure hydrogen; gas chromtography/mass spectrometer detection

### **APPENDIX**

#### **(Nonmandatory Information)**

#### **X1. JET PULSE INJECTION**

## **X1.1 Summary**

X1.1.1 To demonstrate that "Jet Pulse Injection" as depicted in [Fig. 2](#page-2-0) injects a constant volume of hydrogen into a GC/MS independent of hydrogen pressure, an experiment is performed to analyze a diluted calibration standard in hydrogen repetitively by jet pulse injection/GC/MS. The hydrogen pressure of the diluted calibration drops gradually during the entire experiment. The EIC areas of the target compounds are measured for each analysis. The results indicate that the EIC areas remain constant within the analytic error independent of hydrogen pressure drop. This leads to the conclusion that the hydrogen volume injected by jet pulse injection is constant independent of hydrogen pressure of this diluted calibration standard.

### **X1.2 Experimental**

X1.2.1 A diluted calibration standard, Standard-J in [Table](#page-7-0) [X1.1,](#page-7-0) in a one liter steel containerwas analyzed consecutively by jet pulse injection/GC/MS from the Standard-J initial pressure 210 to 78 psi, as listed in [Table X1.1.](#page-7-0) As shown in this table, the analytical sequence of 1st to 4th Analysis of Standard J was repeated a total of 6 times with total 24 analyses. Before this sequence of analyses of Standard-J, UHP hydrogen was

**TABLE X1.1 Analysis of Standard-J by Jet Pulse Injection/GC/MS**

<span id="page-7-0"></span>

Standard-J contains 7.7 ppmv CO $_2$  , 7.7 ppmvAr, 7.7 ppmv O2 and 31.8 ppmv N $_2$  in H $_2$ ; Standard-J is prepared from the dilution through pressurization of the 0.5%  $CO<sub>2</sub>$ , Ar,  $O<sub>2</sub>$  and 2.0% N<sub>2</sub> in H<sub>2</sub> listed above as co-injection standard.

analyzed by the jet pulse injection/GC/MS to demonstrate no target compounds were detected above detection limits.

#### **X1.3 Co-Injection**

X1.3.1 As shown in Table X1.1, each analysis is coinjected, after 1.3 minutes from the beginning of jet pulse injection, with a series of volumes of concentrated calibration standards or ambient air at approximate 12 seconds apart through the GC injector in Fig. X1.1. However, every four analysis in the sequence does not have a co-injection. The reasons for co-injection are listed below.

X1.3.1.1 Instrumentation sensitivity variation through the entire analytical sequence can be monitored through the response factor (RF, [Eq](#page-6-0) ) variation of the target compounds in the co-injection.

X1.3.1.2 The volume of hydrogen from Standard-J injected through jet pulse injection is unknown; however, the volume injected through jet pulse injection can be measured by comparison of the extracted ion chromatogram (EIC) areas of each target compound from jet pulse injection and its response factor (RF) from the co-injection, as shown in [\(Eq](#page-6-0) ).

X1.3.1.3 The RF of water can be calculated from coinjected ambient air, as shown in [Eq](#page-6-0) [\(Fig. 4\)](#page-6-0). The water concentration in the jet pulse injected hydrogen sample can be calculated [\(Eq](#page-6-0) ) from the RF of water and the jet pulse injected volume [\(Eq](#page-6-0) ). For each analysis, the extracted ion chromatogram (EIC) areas of carbon dioxide at m/e44, argon m/e40, nitrogen m/e29, oxygen m/e32 and water m/e18 are obtained for Standard-J and seven co-injections. We use  $[M+1]^+$  m/e29

for quantitation of nitrogen, instead of its molecular ion m/e28, since m/e29 is the base peak while hydrogen is used as carrier gas. The ion m/e29 is  $N_2H^+$  and formed in the following ion-molecule or chemical ionization reaction. See [Fig. X1.2.](#page-8-0)

Carbon dioxide and argon, but not oxygen, also have similar ion-molecular reaction as nitrogen. However, unlike nitrogen, their molecular ions are base peaks. Carbon dioxide has both m/e 44 and 45 in the ratio of 2:1, argon m/e 40 and 41 1:0.8, however, nitrogen m/e 28 and 29 0.7:1.

X1.3.1.4 In this entire analytical process, Standard-J is repetitively jet pulse injected into the GC/MS, which leads to a Standard-J pressure decrease consecutively from 210 to 78 psi. If the jet pulse injection method injects the same volume of the Standard-J into GC/MS each time in spite of pressure drop, the EIC areas of the target compounds should be the same within instrumentation variation.

X1.3.1.5 The instrumentation variation is measured as the percent relative standard deviation of the co-injections response factor (RF), which is the ratio of the volume of the target compound co-injected onto GC column over the EIC area of the target compound. Since the co-injection into the GC injector is split, the volume of the target compound injected is (volume injected through GC injector × Concentration of the target compound/split ratio). The split ratio is the ratio of the sum of the flow rates of the jet pulse split, GC injector split and injector septum purge over the column flow rate, which is 75/1.5 or 50 for the case in Fig. X1.1. An example to calculate RF of  $CO_2$  using [Eq](#page-6-0) [\(10.2\)](#page-5-0) is shown below for 10 $\mu$ L coinjection of 0.49%  $CO<sub>2</sub>$ , Ar, N<sub>2</sub>, and O<sub>2</sub> in H<sub>2</sub>.



**FIG. X1.1 Co-Injection**

<span id="page-8-0"></span>
$$
(\mathbf{L})
$$
 D7649 – 10 (2017)  
\ne<sup>-</sup> (energy: 70ev)  
\n
$$
\begin{array}{ccc}\n\downarrow & & \\
\downarrow & & \\
\downarrow & & \\
\downarrow & & \\
\downarrow & & \\
2 e^- & & \\
\end{array}
$$
 D7649 – 10 (2017)  
\n
$$
\begin{array}{ccc}\n\downarrow & & \\
\downarrow & & \\
\end{array}
$$
 D7649 – 10 (2017)

$$
RF = \frac{10\mu L \times \frac{0.49}{100} (concentration)}{50 (Split Ratio) \times \frac{m}{e} 44 Area}
$$

X1.3.1.6 The EIC areas of carbon dioxide, argon, nitrogen and oxygen in Standard-J analyzed by jet pulse injection in the entire analytical process are summarized for in Table X1.2. The %RSD of EIC areas for carbon dioxide of Standard-J are 6.8 %, which are practically identical to the corresponding %RSD of co-injection RFs, 7.3 %, within experimental errors. This means that the volumes of carbon dioxide of Standard-J jet pulse injected into GC/MS throughout the entire analytical process are identical. The same argument can apply to argon, since %RSD of argon from jet pulse injected Standard-J, 7.1%, is almost identical to that of co-injection, 8.7%. The only way to get constant jet pulse injected volume of both carbon dioxide and argon in Standard-J is through constant hydrogen volume of Standard-J injected by jet pulse injection throughout the entire analytical process. The nitrogen and oxygen have higher %RSD for both Standard-J and co-injection, probably due to nitrogen and oxygen always present in the GC/MS background.

X1.3.1.7 However, the same argument can be applied to nitrogen and oxygen. From these experimental results, one can conclude that the hydrogen volumes injected by jet pulse injection is constant and independent of the hydrogen pressure for hydrogen pressure over 90 psi. However, Standard-J does not contain water or moisture since moisture is easily absorbed onto surfaces, including the internal surface of the standard container. For the same reason, commercial moisture standards are not available in ppmv concentrations. However, the relative humidity of ambient air can be precisely measured by humidity meter; therefore, ambient air can be used as a calibration standard for moisture. The percentage of water in ambient air is the percentage of humidity measured times the saturated water vapor pressure in mm Hg divided by atmospheric pressure in mm Hg. At 25°C, the atmosphere is saturated with water vapor when the partial pressure of water is 23.756 torr. The RF of water is calculated in [Eq](#page-6-0) and water concentration in hydrogen sample [Eq](#page-6-0) .

X1.3.1.8 As shown in [Eq](#page-6-0) , the jet pulse injected hydrogen volume must be calculated  $(Eq)$  $(Eq)$  to obtain the water concentration in samples. An example of calculation of the jet pulse injected volume by [Eq](#page-6-0) is given for the analytical data in Table X1.2. The average area of m/e 44 of jet pulse injected standard J and average RF of co-injected CO<sub>2</sub> are 15803 and  $5.6 \times 10^{-8}$ , respectively, as shown in Table X1.2. For standard J containing 7.7 ppmv  $CO<sub>2</sub>$ , the jet pulse injected volume is calculated based on  $CO<sub>2</sub>$  as below.

*Jet Pulsed Injected Volume=*  
\n
$$
\frac{15803 \text{ area unit} \times 5.6 \times 10^{-3} \frac{\mu L}{\text{area unit}}}{7.7} = 115 \mu L
$$
\n
$$
\frac{7.7}{1,000,000} = 115 \mu L
$$

X1.3.1.9 As the same token, the jet pulse injected volume calculated using m/e40 of Ar is  $(5640 \times 1.7 \times 10^{-7})/(7.7)$  $1000000 = 124$  µL. The difference between both jet pulse injected volumes is 7.5%. However, the jet pulse injected volumes calculated based on nitrogen and oxygen are 102 and 88 µL, respectively. Since its large %RSD for both average areas through jet pulse injection, these two jet pulse injected volumes are only for reference. In general, we use the jet pulse injected volume calculated using  $CO<sub>2</sub>$  since its EIC noise is smallest.

Pressure	Carbon Dioxide,			Argon,			Nitrogen,			Oxygen,			Water
range	7.7 ppmv			7.7 ppmv			$31.8$ ppmv $\times$			7.7 ppmv×			
	Average	%RSD	Average	Average	%RSD of	Average	Average	$%$ RSD	Average	Average	%RSD	Average	Average
	m/e	of $m/e$ 44	and	$m/e$ 40	$m/e$ 40	and	m/e 29	of m/e	and	m/e	of m/e	and	and
	44 Area	Area of	$%$ RSD	Area	Area	%RSD	Area	29	$%$ RSD	32	32 Area	%RSD	%RSD
	of	Standard-J	of RFs	οf	0f	of RFs	of	Area	of	Area	of	οt	of RFs
	Standard-J		of $CO2$ in $\blacksquare$	Standard-J	Standard-J	of Ar	Standard-J	of	<b>RFs</b>	οf	Standard-J	<b>RFs</b>	ot
			Co-			in.		Standard-J	of $N_{2}$	Standard-J		of $O2$	H <sub>2</sub> O
			Injection			Co-			in.			<i>in</i>	in.
						Injection			Co-Injection			$Co-$	$Co-$
												Injection	Injection
			$5.6 \times 10^{-8}$			$1.7 \times 10^{-7}$			$1.9 \times 10^{-7}$			$2.7 \times 10^{-7}$	$1.5 \times 10^{-8}$
$210 \rightarrow$	15803	6.8%	7.3%	5640	7.1%	8.7%	17145	12%	20%	2504	28 %	22%	12%
78 psi													

**TABLE X1.2 Extracted Ion Chromatogram (EIC) Areas of Standard-J**

# **ADDITIONAL READING**

#### *ASTM Standards:*<sup>3</sup>

- **(1)** D1945 Test Method for Analysis of Natural Gas by gas Chromatography
- **(2)** D1946 Practice for Analysis of Reformed Gas by Gas Chromatography
- **(3)** D4150 Terminology Relating to Gaseous Fuels
- **(4)** D4626 Test Method for Analysis of Natural Gas by Gas Chromatography
- **(5)** D4626 Test Method for Analysis of Natural Gas by Gas Chromatography
- **(6)** F307 Practice for Sampling Pressurized Gas for Gas Analysis

### *Other Standards:*<sup>4</sup>

**(7)** California Code of Regulations, Title 4, Division 9, Chapter 6, Article 8 , Sections 4180 – 4181

# *ISO Standards:*<sup>5</sup>

- **(8)** ISO/TR 15916 : 2004 Basic consideration for safety of hydrogen systems
- **(9)** ISO 26142 Hydrogen detection apparatus
- **(10)** ISO TS 14687-2 Hydrogen fuel Product Specification Part 2: Proton exchange membrane fuel cell (PEMFC) applications for road vehicles

<sup>4</sup> Available from Standardization Documents Order Desk, DODSSP, Bldg. 4, Section D, 700 Robbins Ave., Philadelphia, PA 19111-5098, http:// dodssp.daps.dla.mil.

<sup>5</sup> Available from International Organization for Standardization (ISO), 1, ch. de la Voie-Creuse, Case postale 56, CH-1211, Geneva 20, Switzerland, http:// www.iso.ch.

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