

**Designation: D 6776 – 02**

# **Standard Test Method for Determining Anaerobic Biodegradability of Radiolabeled Plastic Materials in a Laboratory-Scale Simulated Landfill Environment<sup>1</sup>**

This standard is issued under the fixed designation D 6776; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon  $(\epsilon)$  indicates an editorial change since the last revision or reapproval.

#### **1. Scope**

1.1 This test method is designed to measure the anaerobic biodegradability of a material under conditions that simulate accelerated decomposition in a municipal solid waste (MSW) landfill. The test method requires the use of a  $^{14}$ C-labeled material so that biodegradability can be determined by monitoring for methane  $({}^{14}CH_4)$  and gaseous and aqueous carbon dioxide  $({}^{14}CO_{2(g)}$  and  ${}^{14}CO_{2(gq)}$ ), which are the terminal endproducts of methanogenic decomposition. Methanogenic conditions typically control decomposition in landfills.

NOTE 1-A more complete description of this decomposition is found in Reference **(3)**. 2

1.2 This method could be applied to landfills that contain materials other than MSW.  $^{14}$ C-Radiolabeled material will be added to compost such that between 25 µci and 75 µci activity per 2 litres of test refuse results.

NOTE 2—Adding more radiolabel is desirable because, if the material biodegrades, there will be little residual radiolabel left at the end of the decomposition experiment, which is when the refuse is removed from a reactor and analyzed for residual radiolabel to perform a mass balance. In addition, if insufficient radiolabel is added, then  $CH_4$  and  $CO_{2(g)}$  production from the added refuse will dilute the <sup>14</sup>CH<sub>4</sub> and <sup>14</sup>CO<sub>2(g)</sub> from decomposition of the test material, and the labeled gases may not be detected in the reactor offgas.

1.3 This measure of anaerobic biodegradability in the laboratory represents what will ultimately occur in a landfill over a long period. The test conditions specified here are designed to accelerate refuse decomposition such that the entire decomposition cycle can be completed in six months.

NOTE 3—This cycle may require decades in a landfill depending upon the actual environmental conditions (moisture content, pH, temperature).

1.4 The measured biodegradability obtained here is compared to the biodegradability of both pure and lignified cellulose, which are chemically similar to office paper and newsprint, both of which are routinely buried in landfills.

NOTE 4—The degradability of the referenced compounds is described in References **(2)** and **(5)**.

At this time, there is no standard concerning the extent to which a compound must biodegrade under the test conditions described here to be considered biodegradable. Thus, this test is most appropriately used to measure biodegradability relative to pure and lignified cellulose.

1.5 *The safety problems associated with refuse and radioactivity are not addressed in this standard. It is the responsibility of the user of this standard to establish appropriate safety and health practices. It is also incumbent on the user to conform to all the regulatory requirements, specifically those that relate to the use of open radioactive sources.*

NOTE 5-There are no corresponding ISO standards.

# **2. Referenced Documents**

- D 883 Terminology Relating to Plastics<sup>3</sup>
- E 170 Terminology Relating to Radiation Measurements and Dosimetry<sup>4</sup>

# **3. Terminology**

3.1 Terminology used in this Standard are defined in Terminology D 883 or Terminology E 170.

3.2 *refuse*, *n*—waste material for anaerobic decomposition. May be municipal or agricultural in source but not meant to include sludge from water treatment or sewage treatment facilities.

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<sup>&</sup>lt;sup>2</sup> The boldface numbers in parentheses refer to the list of references at the end of this standard.

<sup>2.1</sup> *ASTM Standards:*

<sup>3</sup> *Annual Book of ASTM Standards*, Vol 08.01.

<sup>4</sup> *Annual Book of ASTM Standards*, Vol 12.02.

3.3 *seed*, *n*—refuse material from an active anaerobic decomposition producing methane; which is used for inoculum of refuse material to undergo anaerobic decomposition.

# **4. Summary of Test Method**

4.1  $A^{14}C$ -labeled material is added to a mixture of fresh and decomposed refuse in a laboratory reactor. The old refuse serves as a seed to rapidly initiate methanogenesis. The volume of gas produced and the concentrations of  $14CH_4$  and  $14CO_{2(g)}$ are monitored. In addition, the reactor leachate is monitored for<sup>14</sup>C-organics and <sup>14</sup>CO<sub>2(aq)</sub>. At the conclusion of the refuse decomposition cycle, which typically requires 6 to 9 months, the refuse is removed from the reactor, dried, ground to a fine powder and analyzed for residual  ${}^{14}C$  by combustion. A mass balance on the added  $^{14}$ C is then conducted.

# **5. Significance and Use**

5.1 This method can be used to assess the anaerobic biodegradability of polymeric components of MSW such as packaging materials and to compare their biodegradability to that of materials routinely buried in landfills such as office paper and newsprint. The procedure can be completed in 6 to 9 months. This timeframe makes it possible to consider waste management during product design. The data from this method makes it possible to characterize the behavior of consumer products at the end of their useful life when they enter the solid waste management system.

5.2 *Limitations*—Because decomposition in this test is accelerated, the results reflect the ultimate biodegradability of a material in a landfill. The actual rate of degradability in a full-scale landfill will be affected by landfill environmental conditions as well as the physical characteristics of the material when actually buried.

#### **6. Apparatus**

6.1 Tolerances of 5 % from specification are acceptable unless otherwise stated.

6.2 *Reactor*—A detailed description of the 2-L reactor that was used for this research is described in Annex A1. Alternate reactor designs and sizes are acceptable. The critical criteria for the reactor are the ability  $(I)$  to obtain a gas-tight seal so that biogas may be collected, (*2*) to maintain anaerobic conditions, (*3*) to sample and recirculate leachate and (*4*) to ensure that there are no interactions between the material to be tested and the reactor system. If a larger system is used, then additional radiolabel should be added so that radiolabeled endproducts are not diluted to below detection by the increased volume of gas produced as the refuse decomposes.

6.3 *Gas Bag*—The gas bag must contain  $CO<sub>2</sub>$  and  $CH<sub>4</sub>$ while not allowing oxygen entry via diffusion. If a material to be tested may result in the production of volatile intermediates or endproducts, then the gas bag material should not result in sorptive losses for these compounds.

6.4 *pH Meter*.

6.5 *Combustion Furnace*—This consists of a column packed with copper oxide catalyst and a furnace capable of achieving temperatures of 875°C for oxidation of  ${}^{14}CH_4$ to<sup>14</sup>CO<sub>2</sub>.

6.6 *Tube Furnace*, capable of achieving temperatures of 875 °C. This consists of a steel column (121.9 cm [48 in.] long by 3.8 cm [1.5 in.] inside diameter) packed with copper oxide for oxidation of refuse samples.

6.7 *Ether-based Polyurethane Tubing*.

6.8 *Liquid Scintillation Counter*, with background correction capabilities.

6.9 *Gas Chromatograph (GC)*, equipped with a thermal conductivity detector; a column capable of separating  $CH<sub>4</sub>$ ,  $CO<sub>2</sub>$ , oxygen  $(O<sub>2</sub>)$ , and nitrogen  $(N<sub>2</sub>)$ ; and an integrator.

6.10 *Centrifuge*, equipped with a bucket that can hold 10-mL centrifuge tubes and capable of 3500 rpm.

6.11 *Syringe Pump*.

6.12 *Pressure Gage*.

6.13 *Vacuum Pump*.

6.14 *Wiley Cutting Mill*.

6.15 *Fiberglass Mesh*, standard construction grade.

#### **7. Reagents and Materials**

7.1 *Purity of Reagents*—Reagent grade chemicals shall be used in all tests. Unless otherwise indicated, it is intended that all reagents conform to the specifications of the Committee on Analytical Reagents of the American Chemical Society where such specifications are available **(1)**. Other grades may be used, provided it is first ascertained that the reagent is of sufficiently high purity to permit its use without lessening the accuracy of the determination.

7.2 *Purity of Water*—Unless otherwise stated, references to water shall be understood to mean deionized water with a resistance of greater than 10 megohms.

7.3 *Scintillation Cocktail*, capable of dissolving 1 mL of 2N sodium hydroxide (NaOH) without separation into layers or color production, or both.

NOTE 6-Packard Instruments' ULTIMA GOLD® meets this criteria. No other Scintillation reagent tested did.

7.4 2 *N* NaOH.

7.5 0.5  $M$  sulfuric acid (H<sub>2</sub>SO<sub>4</sub>).

### **8. Hazards**

8.1 This practice involves the use of microorganisms and hazardous chemicals that could produce a variety of diseases. Avoid contact with these materials by wearing gloves and other appropriate protective equipment. Use good personal hygiene to minimize exposure, and follow the instructions given in material safety data sheets.

8.2 The simulated-solid-waste mixture could contain sharp objects. Extreme care should be taken when handling this mixture to avoid injury.

#### **9. Procedure**

NOTE 7—**Precaution:** Adequate laboratory facilities, such as fume hoods and controlled ventilation, along with safe techniques, must be used throughout this work.

9.1 *Overview*:

9.1.1 Initially, reactors are filled with the  $^{14}$ C-labeled polymer and fresh and decomposed refuse. Monitor reactors for gas volume and composition  $(CH_4, {}^{14}CH_4, CO_2, {}^{14}CO_2)$  as well as the presence of radiolabel in the leachate  $({}^{14}C$ -organics,  ${}^{14}CO_2$ ).

Also monitor the leachate pH and chemical oxygen demand. Analyze the gas collected in gas bags every two to four weeks, and analyze the leachate at the same frequency. A more frequent monitoring frequency will likely be necessary early in the experiment when gas production is high and leachate composition is less stable. Initially, gas production may be so high as to require weekly or even more frequent gas analysis.

9.1.2 At the completion of the refuse decomposition cycle, dismantle the reactors and remove the refuse solids so they can be analyzed for residual radiolabel. Dry the solids, grind them in a wiley mill to pass through a 0.5-mm screen and then analyze them for  ${}^{14}$ C. This analysis is done by combustion of a solid sample and then trapping the evolved carbon as  ${}^{14}CO_2$ . Once data on the amount of residual radiolabel is available, calculate the fractions of the added radiolabel converted to<sup>14</sup>CH<sub>4</sub> and <sup>14</sup>CO<sub>2</sub>, solubilized, and remaining with the refuse solids. The material remaining with the refuse solids may be either undegraded material, cell mass or some other transformation product. Detailed protocols for each aspect of reactor loading, monitoring, takedown and final analysis are presented in 9.2-9.10.

9.1.3 Operate reactors to accelerate refuse decomposition (*1*) by the addition of a seed of well-decomposed refuse to eliminate the lag period or acid phase of decomposition, (*2*) by the neutralization and recirculation of leachate through the reactors and (*3*) by the incubation of the reactors at 37°C, the optimal temperature for mesophilic refuse decomposition. These steps make it possible to simulate complete refuse stabilization, as evidenced by little or no measurable methane production, in six months. Seeding the reactors and operating them at high moisture content and neutral pH without leachate recirculation is expected to lead to similar results.

#### 9.2 *Reactor Loading*:

9.2.1 Place a layer of fiberglass mesh on the bottom of the reactor to prevent large solids from plugging the reactor outlet.

9.2.2 Mix seed and fresh shredded refuse in a desired ratio of 30/70 by volume, which may be approximately 50/50 by dry weight. One thousand grams of total mixture should prove sufficient to fill a 2-L reactor. The effectiveness of the seed in initiating methane production from refuse should be verified in preliminary work. Add sufficient water so that the refuse may be compacted.

9.2.3 Add the refuse mixture to the reactor in approximately 75-mm lifts and compact the mixture after each addition.

9.2.4 After the reactor is half full, add radiolabeled material to the center of the reactor. Continue filling the reactor with the rest of the refuse.

9.2.5 Add a layer of cheesecloth and 454 g of 3-mm glass beads over the refuse. The cheesecloth and glass beads will distribute leachate recycled to the top of the reactor.

9.2.6 Close the reactor and connect a gas bag to the reactor outlet.

9.2.7 Leak-test all reactor joints to ensure that the system is gas tight by drawing a vacuum on one section of the reactor at a time and verifying that it holds a vacuum.

9.2.8 Add water to the leachate vessel and pump it over the refuse. Drain the leachate from the refuse and check the

volume remaining. Adjust, if necessary, to achieve a final leachate volume of at least 500 mL (based on a 2-L reactor).

9.3 *Leachate Recycle and Neutralization*:

9.3.1 Check the pH of the leachate daily and adjust with 2 *M* NaOH/HCL to achieve the desired pH of  $7.0 \pm 0.3$ . Once the leachate exhibits this pH consistently without acid or base addition, change to a weekly monitoring of pH.

9.3.2 Recycle leachate five to six times a week.

9.4 *Gas Composition*—Methane and carbon dioxide are typically measured by using a gas chromatograph (GC) equipped with a thermal conductivity detector. Concentrations of 1 to 50 % by volume can be expected. Helium is typically used as the carrier gas. Calibrate the GC by using a series of external standards with differing concentrations of  $CH<sub>4</sub>$  and  $CO<sub>2</sub>$ .

9.5 *Gas Trapping for Measurement of*  $^{14}CH_4$  *and*  $^{14}CO_2$ :

9.5.1 Assemble the gas trapping system using four 20-mL serum bottles filled with 15 mL of 2  $M$  NaOH to act as  $CO<sub>2</sub>$ traps. Place two traps before the combustion furnace and two after the furnace (Fig. 1). When inserting needles in the traps, be certain that the incoming needle extends to the bottom of the trap and the exhaust needle is in the headspace of the trap.

9.5.2 Inject a total of 400 mL of sample through the traps in 50-mL increments. Feed the gas into the gas trapping system at 20 mL/min by using a syringe pump. Use  $O_2$  as the carrier gas at 30 mL/min. Supply  $O_2$  in excess of the stoichiometric amount required to oxidize the  $CH<sub>4</sub>$  in the sample.

9.5.3 After the injections are complete, cover the injection port with any tape that fits tightly over the port and let the carrier gas continue to flow through the system for at least 30 min. Then add 1 mL from each trap to scintillation cocktail. Before scintillation counting, incubate samples in a refrigerator for at least 12 h to reduce chemiluminescence.

9.6 *Gas Volume Determination*:

9.6.1 With reference to Fig. 2, evacuate the stainless steel cylinder with a vacuum pump to 100 to 200 mbars while keeping the valve between the cylinder and gas sample closed. Vent the pump outlet to a fume hood. Record the initial pressure.

9.6.2 Connect the gas bag to the luer fitting and open valve 2. Allow gas to flow from the gas bag until the pressure reaches a value greater than 950 mbars. Close valve 2 and record the pressure. Repeat this procedure until the gas bag is evacuated. If the bag is evacuated before reaching 950 mbars, then close valve 2 and record the pressure.

9.6.3 After all the gas has been evacuated from a bag, open both valves and let the cylinder achieve room pressure. Record this pressure as atmospheric pressure.

9.6.4 Calculate the gas bag volume as follows:

$$
V_s = \frac{V_c \times \Sigma (Pf - Pi)}{Pa} \tag{1}
$$

where:

 $Vs =$  volume of sample, mL,

 $Vc =$  volume of the cylinder, mL,

 $Pf = \text{final pressure of cylinder, mmHg,}$ 

 $\overrightarrow{Pi}$  = initial pressure of cylinder, mmHg, and

*Pa* = atmospheric pressure.

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**FIG. 2 System for Determination of Gas Volume**

9.6.5 Correct the volume of gas to standard temperature and pressure (STP) as follows:

$$
V_{S-STP} = V_S \times \frac{Pa - P_W}{760} \times \frac{273.15}{T + 273.15}
$$
 (2)

where:

- $V_{S_{\text{STP}}}$  = volume of sample, mL, at STP and mean sea level,
- *Pa* = atmospheric pressure plus adjustment for elevation, mmHg,
- $T =$  room temperature,  ${}^{\circ}C$ , and<br>*Pw* = vapor pressure at room tem

$$
Pw =
$$
 vapor pressure at room temperature, mm Hg.

9.7 *Leachate Collection and Analysis*:

9.7.1 Allow leachate to drain from the reactor to the leachate collection vessel for 2 to 4 h as needed to drain >95 % leachate. Mix the leachate by turning on the magnetic stirrer

under the leachate collection vessel. Then collect 15 mL of leachate and adjust its pH to  $12 \pm 0.2$  using 50 % (w/w) NaOH.

9.7.2 Vortex the leachate to homogenize it and pour 8 mL into a centrifuge tube. Centrifuge the leachate for 15 min at 3500 rpm.

9.7.3 Transfer the supernatant to a scintillation vial and filter 2.2 mL through a 25-mm, 0.2-um polysulfone filter. Add two 0.5-mL specimens of filtered leachate to scintillation cocktail, refrigerate overnight and analyze by scintillation counting.

9.7.4 Place 2 mL of centrifuged leachate into a centrifuge tube containing 4 mL of 0.2  $M$  cadmium sulfate (CdSO<sub>4</sub>). Vortex until thoroughly mixed and refrigerate overnight.

9.7.5 Centrifuge the cold sample at 3500 rpm for 15 min and filter the supernatant through a 13-mm, 0.2-µm polysulfone filter. Add two 0.5-mL specimens of cadmium-treated leachate to scintillation cocktail and analyze.

9.8 *Calculation of Leachate Radiolabel Presence*:

9.8.1 Calculate the amount of dissolved  $^{14}$ C-organic as follows:

$$
{}^{14}C(\text{organics}) = 3 \times \frac{\text{Cdt}}{0.5 \text{ mL}} \tag{3}
$$

where:

*14C*(organics) = activity of dissolved organic matter in leachate (dpm/mL), and

Cdt = activity of cadmium-treated leachate specimen (dpm in a 0.5-mL sample).

9.8.2 Calculate the dissolved  ${}^{14}CO_2$  as follows:

$$
{}^{14}CO_2 = \text{Total} - {}^{14}C \text{ (organics)}
$$
 (4)  
Total =  $\frac{\text{Filt}}{0.5 \text{ mL}}$ 

where:

 $^{14}CO$  = dissolved CO<sub>2</sub> in leachate (dpm/mL),

Total  $=$  activity of the filtered leachate sample (dpm/mL),

Filt  $=$  measured activity in 0.5-mL sample (dpm).

9.9 *Reactor Dismantling and Refuse Grinding*:

9.9.1 Perform final samplings for gas volume and composition and leachate composition.

9.9.2 Open the reactor and remove the glass beads and cheesecloth. Next, empty all of the refuse into a series of tared baking pans and dry to constant weight at 65°C in a drying oven that is in a fume hood.

9.9.3 Once dry, sort the refuse and remove rocks and big pieces of glass that will be abrasive to the wiley mill blades. Weigh the mass of material removed before grinding.

9.9.4 Grind the refuse to pass through a 3-mm screen in a wiley mill. Finally, regrind the refuse to pass through a 0.5-mm screen.

9.9.5 Place the refuse in a jar that is covered with a piece of foil with holes punched in it. Redry the refuse at 65°C for 24 h and then seal the jar until it is time for the combustion analysis.

9.10 *Combustion Analysis*:

9.10.1 *Overview*—A small specimen of ground refuse is burned at high temperature in the primary tube furnace (designated F-1) to convert the organic matter to  ${}^{14}CO_2$ . The gas is then routed to a second combustion furnace (F-2) to ensure complete oxidation. From F-2, the gas is trapped in a series of three  $CO<sub>2</sub>$  traps, and the traps are analyzed by scintillation counting to determine the amount of  $^{14}C$  solid organic matter in the original sample. The trap exhaust must be located in a fume hood.

9.10.2 *Preparation of Primary Combustion Tube Prior to Initial Use*:

9.10.2.1 Pack the combustion tube 3⁄4 full with copper scouring pads or copper filings.

9.10.2.2 Screw end caps onto tube and attach  $O_2$  tank. Set the  $O_2$  flow rate to 60 mL/min with a flowmeter.

9.10.2.3 Heat the tube to 1000°C and allow it to oxidize for 3 h. Turn off furnace and let the column cool to room temperature. To accelerate cooling, pump air through the tube.

9.10.3 *Sample Combustion*:

9.10.3.1 Two furnaces are used for specimen combustion and they are designated as F-1 and F-2. As described in 9.10.1, the offgas from F-1 is routed to F-2 to ensure complete oxidation of the organics.

9.10.3.2 Connect the F-1 outlet to the F-2 inlet with cleaned ether-based polyurethane tubing  $(1.58 \text{ mm}$  [ $1/16$ -in.] inside diameter, 3.18 mm [1⁄8-in.] outside diameter). Also connect the outlet from F-2 to the NaOH traps with the same type of tubing. After use, clean the tubing by rinsing it with methanol and then water. The tubing should be checked regularly for damage or scorching.

9.10.3.3 Adjust the temperature on F-2 to 875°C.

9.10.3.4 After weighing, place the specimen to be combusted in the combustion boat and then the combustion boat in the combustion tube. Position the tube in F-1 so that approximately 25 cm (10 in.) of the tube protrude from the inlet end of the furnace and 15 cm (6 in.) protrude from the outlet end. Position the combustion boat 38 cm (15 in.) from the inlet end of the combustion tube.

9.10.3.5 After closing the inlet end, attach the F-1 outlet to the F-2 inlet with ether-based polyurethane tubing as described in 9.10.3.2.

9.10.3.6 Prepare three 20-mL serum bottles with 15 mL of 2 *M* NaOH to act as  ${}^{14}CO_2(g)$  traps and connect the traps in series as in 9.5. Connect the traps with the tubing described in 9.10.3.2.

9.10.3.7 Connect the  $O_2(g)$  tank to the F-1 inlet and turn on the gas. Check the system for leaks with a leak detection fluid.

9.10.3.8 Measure the exhaust gas flow rate and adjust it to 60  $\pm$  1 mL/min. Then allow oxygen to flow through the furnace for at least 5 min. This oxygen flowrate will flush the furnace three times in 90 min.

9.10.3.9 Turn on F-1 and wait for the temperature to stabilize at 875°C. Once stable, allow the furnace to remain at 875<sup>°</sup>C for 90 min to combust the specimen.

9.10.3.10 After combustion, disconnect the traps and tubing and analyze the traps by scintillation counting.

9.10.3.11 Verify that there is no carryover of radiolabel in the furnaces by running oxygen through the furnace and one fresh NaOH trap.

9.10.3.12 Once the carryover combustion check is complete, reset F-1 to 25°C and pump air through the furnace to accelerate the cooling process in preparation for the next

specimen. Disconnect the tube between F-1 and F-2 and attach it to the  $O_2$  tank. Continue the supply of  $O_2$  to F-2.

### **10. Detection Limits**

10.1 Add sufficient radiolabel to the reactors so that mineralization of at least 1 % of the radiolabel can be detected. However, for a polymer that is highly biodegradable, it may be quite difficult to detect the residual radiolabel in the refuse at the end of the experiment.

10.2 Detection limit calculations are presented in Annex A2-Annex A4.

#### **11. Precision and Bias**

11.1 *Precision*—The results provide a relative measure of anaerobic biodegradability of a test compound under optimal conditions in a MSW matrix. The principle result is the percent of the added compound that is converted to  ${}^{14}CO_2$  and  ${}^{14}CH_4$ . The procedure described here has been applied to four test materials. Each material was tested in triplicate reactors. The repeatability amongst the triplicate reactors for each of the test materials are given as the average followed by the standard deviation (sd): 55.5 (sd = 6.76), 2.5 (sd = 0.17), 25.7  $(sd = 3.04)$  and  $52.0$   $(sd = 1.17)$ . One additional material, a polyhydroxyalkonoate, was tested in later experiments and the average mineralization and standard deviation for this material were 45.2 % and 6.3, respectively. The reproducibility of the protocol, as determined by repeating the protocol in other laboratories, has not been determined. No additional information is available.

11.2 *Bias*—No information can be presented on the bias of this procedure for measuring the anaerobic biodegradability of radiolabeled test materials in a laboratory-scale simulated landfill because no information is available.

NOTE 8—The detection limit calculations presented in Annex A2 and Annex A3 are given for typical values of gas production in a 2-L reactor operated as described in the protocol. However, these calculations are best used as ranges because every reactor system will behave slightly differently.

#### **12. Keywords**

12.1 anaerobic biodegradation; biodegradability; landfills; methane production; radiolabeled method

#### **ANNEXES**

#### **(Mandatory Information)**

### **A1. FABRICATION OF A 2-L REACTOR SYSTEM**

A1.1 A 2-L reactor constructed from glass and TFEfluorocarbon must be fabricated. Reactor materials must be selected to minimize the potential for the test material and any intermediate or endproduct to interact with the reactor system. A detailed description of a reactor follows, and the reactor is illustrated in Fig. A1.1. Several steps require a glass blower.

A1.1.1 Fabricate reactor from two pieces (10.2-cm [4-in.] diameter) of flanged, medium thickness glass tube (flat o-ring joint with 38.1-cm [15-in.] glass below joint).

A1.1.2 Cut a portion from one of the two pieces of glass tube for fabrication of a leachate collection vessel with a working volume of 1 L.

A1.1.3 Seal shut one end of each piece of tube from step 1. The two ends of the reactor can now be connected to form a gas-tight seal with a viton o-ring and a u-shaped flange clamp.

A1.1.4 Construct reactor inlets and outlets from glass stopcock fittings fused into the reactor and leachate collection vessels.

A1.1.5 The leachate collection and reactor vessels should be connected with tubing that does not sorb organics or leak oxygen, by using leak tight, torque-free tube fittings.

NOTE A1.1—(Kynar tubing and Swagelok fittings [Crawford Fitting

Co., Solon, OH] have been used successfully. The connection between the bottom of the reactor and the leachate collection vessel inlet should be made with TFE-fluorocarbon-coated flexible tubing slipped over the stopcock fittings.

A1.1.6 A pump must be used to recycle leachate from the leachate collection vessel to the top of the reactor.

A1.1.7 Place a magnetic stir bar in the leachate collection vessel. The vessel then sits on a magnetic stirrer to mix the leachate after buffer addition.

A1.2 Gas should be collected in gas sampling bags that contain layers of polyester, polyvinylidene chloride, aluminum foil, polyamide and high-density polyethylene.

NOTE A1.2—Call-5-Bond gas sampling bags available from Calibrated Instruments, Hawthorne, NY. are examples. Gas bags should include a luer-fit valve for obtaining specimens for analysis of gas composition as well as a straight-through connector connected to the reactor outlet.

NOTE A1.3—Kynar tubing and two quick disconnect tube couplings (Part Nos. 5012K38, 5012K44, McMaster Carr, Atlanta, GA) have been found to be best suited to this application. The female quick disconnect valve is attached to the gas bag by a piece of flexible tubing attached to the straight-through connector on the bag (nickel-plated brass with swage ring). The male end is attached to the reactor with a piece of kynar tubing attached to a brass fitting.

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- $(A)$  Reactor
- $(B)$  Leachate collection vessel with magnetic stirrer
- (C) Gas collection bag
- (D) Kynar® tubing  $(9.5 mm)$  [3/8-in.] outside dia, 1.58-mm [1/16-in.] wall thickness
- $(E)$  Pump
- $(F)$  Food-grade flexible tubing (9.5-mm [3/8-in.] inside dia, 1.58-mm [1/16in.] wall thickness)
- $(H)$  6-mm stopcock with 7.6-cm (3-in.) gas extension
- TFE-flurocarbon-lined flexible tube  $\Omega$
- $(J)$  Valve in glass tube
- $(K)$  Union elbow
- $(L)$  Union tee
- $(M)$  Flange clamp
- $(N)$  Hose clamp

**FIG. A1.1 Reactor Used for Biodegradation Test**

#### **A2. CALCULATION OF DETECTION LIMIT FOR POLYMER IN GAS PHASE**

A2.1 Reactors are sampled every two to four weeks depending upon the volume of gas produced. The gas production rate will increase initially, reach a peak and then exhibit an asymptotic decrease **(2)**. This can be visualized in the size and shape of the gas collection bag. Data from a typical experiment are presented in Table A2.1 and are used to calculate the detection limit for polymer biodegradation. Each time that the scintillation counter is used, a lower limit of detection  $L<sub>D</sub>$  can be calculated as given in Eq A2.1 (4). If the counts exceed  $L<sub>D</sub>$ , then they are significant at the 99.5 % confidence interval; otherwise, they should be considered as zero.



$$
L_D = 2.71 + 4.65 \ (\mu_B)^{\frac{1}{2}}
$$
 (A2.1)

where:

 $L<sub>D</sub>$  = the detection limit (counts), and

 $\mu_B$  = the mean of blank (counts).

A2.2 At North Carolina State University at Raleigh NC, experimental data for seven measurement periods were found to have an average  $L<sub>D</sub>$  of 10 dpm. To calculate a typical detection limit, values of 10 dpm and 11 L were used for  $L_D$ and gas volume, respectively. Based on these assumptions and that 400 mL of gas were trapped per analysis, a detection limit was calculated as follows:

$$
\frac{10 \frac{\text{dpm}}{\text{mL}} \times 15 \text{ mL (liquid trap volume)} \times 11 \text{ L}}{0.4 \text{ L}} = 4125 \text{ dpm}
$$
\n(A2.2)\n
$$
100\% \times \frac{4125 \text{ dpm (not detected)} \times 2 \text{ (for } ^{14}\text{CH}_4 + ^{14}\text{CO}_2)}{2.22 \times 10^6 \frac{\text{dpm}}{\mu\text{ci}} \times 10.092 \mu\text{ci added}}
$$
\n(A2.3)

As shown in this calculation, the detection limit is a strong function of the amount of radiolabel added, 10.092 µci in this case.

#### **A3. CALCULATION OF DETECTION LIMIT FOR POLYMER IN LEACHATE**

A3.1 Under anaerobic conditions, materials are biodegraded to  $CO_2$  and  $CH_4$ , and some of the  $CO_2$  will dissolve in the leachate. In this annex, calculations are performed to estimate the detection limit for dissolved  $CO<sub>2</sub>$  as well as for dissolved organic radiolabel. In a recent experiment, a typical leachate volume in a 2-L reactor was 1650 mL.

A3.2 The leachate is analyzed in two fractions as described in 0:

A: 0.5 mL filtered and added to 18 mL of scintillation cocktail.

B: 2 mL was diluted with 4 mL of  $CdSO<sub>4</sub>$  solution, filtered and 0.5 mL was counted in scintillation cocktail.

Therefore, the quantity A-B represents  ${}^{14}CO_2$ , and B represents  $^{14}$ C-dissolved organics. Typical  $L_{D}$ s were 9.5 dpm for the

# blank and 11.6 dpm for a cadmium-treated blank. For purposes of calculation, an  $L<sub>D</sub>$  of 10.5 dpm was used. Since the cadmium-treated sample (B) is diluted, it will control the detection limit. The detection limit is the same for dissolved<sup>14</sup>CO<sub>2</sub> and organics since both are calculated from the same leachate sample. The detection limit is calculated as:

$$
\frac{10.5 \text{ dpm}}{0.5 \text{ mL}} \times 1650 \text{ mL} \times 3 \text{ (dilution factor)}
$$
  
2.22 × 10<sup>6</sup>  $\frac{\text{dpm}}{\mu \text{ci}} \times 10.092 \mu \text{ci}$  × 100 % = 0.46 % (A3.1)

As shown in this calculation, the detection limit is a strong function of the amount of radiolabel added, 10.092 µci in this case.

#### **A4. CALCULATION OF DETECTION LIMIT FOR RESIDUAL RADIOLABEL**

A4.1 The detection limit for residual radiolabel is calculated based on Eq A2.1; three NaOH traps are used. At the lower limit, detectable counts would be detected in the first trap only. Assuming an LD of 10 dpm/mL, combustion of a 0.05-g specimen and a total of 750 g of dry refuse removed from a reactor, the detection limit for residual radiolabel is 1.01 µci:

$$
\frac{10 \frac{\text{dpm}}{\text{mL}} \times 15 \text{ mL} \times 750 \text{ g}}{0.05 \text{ g sample} \times 2.22 \times 10^6 \frac{\text{dpm}}{\mu \text{ci}}} = 1.01 \,\mu \text{ci}
$$
 (A4.1)

A4.2 The amount of residual radiolabel at the end of a decomposition experiment is a function of the initial amount added; its extent of biodegradation; the relative amount of carbon converted to gaseous endproducts, cell mass and humic matter; and the actual chemical position of the radiolabel in the test material.

# **REFERENCES D 6776**

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