



# Standard Test Method for Repassivation Potential of Aluminum and Its Alloys by Galvanostatic Measurement<sup>1</sup>

This standard is issued under the fixed designation D6208; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon ( $\epsilon$ ) indicates an editorial change since the last revision or reapproval.

## 1. Scope

1.1 A procedure to determine the repassivation potential of aluminum alloy 3003-H14 (UNS A93003) (**1**)<sup>2</sup> as a measure of relative susceptibility to pitting corrosion by conducting a galvanostatic polarization is described. A procedure that can be used to check experimental technique and instrumentation is described, as well.

1.2 The test method serves as a guide for similar measurement on other aluminum alloys and metals (**2-5**).

1.3 The values stated in SI units are to be regarded as the standard. Values given in parentheses are for information only.

1.4 *This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use.*

## 2. Referenced Documents

2.1 *ASTM Standards*:<sup>3</sup>

**D1193** Specification for Reagent Water

**D3585** Specification for ASTM Reference Fluid for Coolant Tests

**G3** Practice for Conventions Applicable to Electrochemical Measurements in Corrosion Testing

**G15** Terminology Relating to Corrosion and Corrosion Testing (Withdrawn 2010)<sup>4</sup>

**G46** Guide for Examination and Evaluation of Pitting Corrosion

**G107** Guide for Formats for Collection and Compilation of Corrosion Data for Metals for Computerized Database Input

## 3. Terminology

3.1 *Definitions*: Terms used in this test method can be found in Practice **G3** and Terminology **G15**.

3.2 *Symbols*:

3.2.1  $E_B$ —break potential, potential at which the passive aluminum oxide layer breaks down.

3.2.2  $E_G$ —protection potential as measured in this galvanostatic method, potential at which oxide layer repassivates.

3.2.3  $J$ —current density, in  $A/m^2$

## 4. Summary of Test Method

4.1 The test method described is an adaptation of the method described in FORD Motor Company standards (**6**).

4.2 An aluminum alloy specimen is polarized at fixed current density for 20 min. in a solution of coolant and corrosive water containing chloride. The potential as a function of time is recorded.

4.3 The maximum potential,  $E_B$  reached upon polarization is determined, as is the minimum potential following the maximum potential,  $E_G$ .

4.4 Visual examination of the specimen may be made using Guide **G46** as a guide after disassembly and rinsing.

## 5. Significance and Use

5.1 This test method is designed to measure the relative effectiveness of inhibitors to mitigate pitting corrosion of aluminum and its alloys, in particular AA3003-H14, rapidly and reproducibly. The measurements are not intended to correlate quantitatively with other test method values or with susceptibility to localized corrosion of aluminum observed in service. Qualitative correlation of the measurements and susceptibility in service has been established (**1**).

5.2 The maximum potential reached upon initial polarization,  $E_B$ , is a measure of the resistance to breakdown of the aluminum oxide film. Lower susceptibility to initiation of pitting corrosion is indicated by a more noble potential (See

<sup>1</sup> This test method is under the jurisdiction of ASTM Committee D15 on Engine Coolants and Related Fluids and is the direct responsibility of Subcommittee D15.06 on Glassware Performance Tests.

Current edition approved Feb. 1, 2014. Published March 2014. Originally approved in 1997. Last previous edition approved in 2007 as D6208 - 07. DOI: 10.1520/D6208-07R14.

<sup>2</sup> The boldface numbers in parentheses refer to the list of references at the end of this standard.

<sup>3</sup> For referenced ASTM standards, visit the ASTM website, www.astm.org, or contact ASTM Customer Service at service@astm.org. For *Annual Book of ASTM Standards* volume information, refer to the standard's Document Summary page on the ASTM website.

<sup>4</sup> The last approved version of this historical standard is referenced on www.astm.org.

Practice G3 and Terminology G15.) This potential, as measured in this test method, is not very sensitive to the inhibitors present.

5.3 The minimum potential,  $E_G$ , following the maximum potential is a measure of the protection against continued pitting corrosion by the inhibitors. Again, a more noble potential indicates better protection. This potential is sensitive to the inhibitors present.

5.4 Visual examination of the specimens can provide information about subtleties of the pitting and inhibition mechanisms. Number of pits, pit depth, amount of deposit, and surface discoloration are some examples of recordable observations, which can assist evaluation of inhibitor effectiveness.

5.5 The presence of chloride in the test solution is critical to observation of pitting corrosion. Also, a coolant/corrosive water solution in which gas bubbles evolve spontaneously on the aluminum (indicating general corrosion) is unlikely to have a significant amount of observable pitting corrosion.

## 6. Apparatus

6.1 *General Description*—The apparatus for the electrochemical test consists of a cell, current supply, recorder, and three electrodes. Fig. 1 is a generalized schematic of the arrangement. More specific requirements for each component are given below.

6.2 *Cell*—The cell consists of a No.25 O-ring borosilicate glass joint held vertically using standard laboratory clamps and ring stand. The working electrode will be clamped to the bottom using the matching O-ring clamp and viton or silicone rubber gasket.

6.3 *Current Supply and Recorder*—A constant current supply capable of generating 872  $\mu$ A continuously is required. The recorder must have a high input impedance ( $> 10^{12}$  Ohms), be capable of recording potentials of  $\pm 2$  V with mV accuracy, and have a low gain. These capabilities are typical of commercial potentiostat/galvanostat instruments connected to either a strip chart recorder or computer, for experimental control and data acquisition. The schematic in Fig. 1 shows connections using a

current supply and mV strip chart recorder, and Fig. X2.1 shows a schematic for using a computer and potentiostat/galvanostat.

### 6.4 Electrodes:

6.4.1 *Working Electrode (WE)*—The working electrode, aluminum test coupon, is cut as 51  $\times$  51 mm (2 in.  $\times$  2 in.) squares from aluminum sheet 2 to 6 mm (1/16 in. to 1/4 in.) thick. The standard material is AA3003-H14 (UNS A93003), used to develop the precision and bias statements. The coupon is rinsed thoroughly (both sides) with methanol and placed in a low temperature drying oven. No additional surface preparation is desirable. Prior to testing, a coupon is allowed to cool to room temperature. Then it is clamped to the bottom of the O-ring joint using the matching O-ring (viton or silicone rubber) and clamp. The clamping screw may be tightened to finger tightness, if desired. Excessive tightening must be avoided. This gives an area of 8.72 cm<sup>2</sup> aluminum exposed to the solution.

6.4.2 *Auxiliary Electrode (AE)*—Ultrafine grade graphite rod, 6-8 mm (1/4 in.) in diameter and at least 20 cm (8 in.) long. Avoid coarse grades as they can adsorb inhibitors.

6.4.3 *Reference Electrode (RE)*—The reference electrode can be of any convenient type, for example saturated calomel (Hg/HgCl) or silver chloride (Ag/AgCl). The electrode must be in good working order and stable in the solution to be measured. The reference electrode is placed in Luggin probe to avoid solution impedance bias. Appendix X2 contains two suggestions for easily constructed Luggin probes.

6.5 *Timer*—Timer with 1 s resolution out to 30 min.

## 7. Preparation of Apparatus

7.1 *Assembly*—Prior to running tests, assemble the cell and electrodes, using an unprepared Al specimen as the “working” electrode using appropriate clamping. The auxiliary electrode is positioned so that the tip is from 5 to 10 mm from the working electrode surface. The Luggin probe is positioned so that the tip is from 1 to 3 mm from the working electrode surface. It is most convenient if the clamping arrangement is such that this electrode configuration is maintained easily. The cell is then removed and Al specimen unclamped.

## 8. Procedure

8.1 A corrosive water containing chloride, sulfate, and bicarbonate is prepared by dissolving the following amounts of anhydrous salts in distilled or deionized water, ASTM Type II (see Specification D1193):

Sodium sulfate	592 mg
Sodium chloride	660 mg
Sodium bicarbonate	552 mg

The solution is made up to a total weight of 1 kg with distilled or deionized water at 20°C. A 4-kg batch size is convenient if many tests are to be run, multiply amounts above by four. This will give a solution, which is 400 ppm in chloride, sulfate, and bicarbonate.

8.2 Rinse cell, O-ring, Luggin probe (inside and out), auxiliary electrode, and reference electrode thoroughly with Type II water.

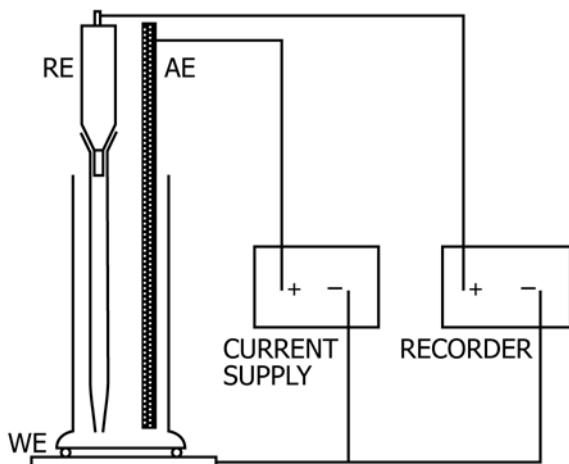


FIG. 1 Generalized Experimental Set-up

8.3 Prepare the aluminum specimen as the working electrode (see 5.4.2). Clamp to cell, using O-ring, and set to one side.

8.4 Prepare the test solution as 25 vol % of the coolant to be tested, 25 vol % of the corrosive water from 6.1, and the remainder deionized or distilled water. The amount to be made depends on one's exact cell configuration. Sufficient test solution is required to fill the cell (about 50 mLs) and the Luggin probe assembly. For the configurations of Luggin probe given in Appendix X2, 160 mLs is more than sufficient.

8.5 Fill the Luggin probe with test solution sufficient to cover the tip of reference electrode when inserted. Insert reference electrode. Gently tap Luggin to remove any bubbles between the tip and reference electrode. If a vertical Luggin is used, as in Fig. X2.2, then bubbles can be removed by allowing solution to drain slowly into a waste container.

8.6 Set up current generator to output 872  $\mu\text{A}$  ( $J = 100 \mu\text{A}/\text{cm}^2$ ) continuously, set recorder to a range of  $\pm 2 \text{ V}$  (other settings may be used if found to be necessary to achieve accurate and representative potentials, chart speed as desired (5 mm/min is reasonable). If acquiring data by computer, set data acquisition rate to 1 point/s. Do not turn either generator or recorder on at this time.

8.7 Fill cell with approximately 50 mL of test solution, about 25 mm from the top of the cell. Start timer. Do not start generator at this time. Recorder may be turned on at this time. Assemble cell over Luggin probe and auxiliary electrode. Attach wires to reference electrode, auxiliary electrode, and working electrode. Check for bubbles in Luggin, tap gently to remove.

8.8 At 5 min on the timer, turn on current generator, and recorder, if not already on. Record potential versus time response for 20 min. Turn off current generator and recorder (see Note 1).

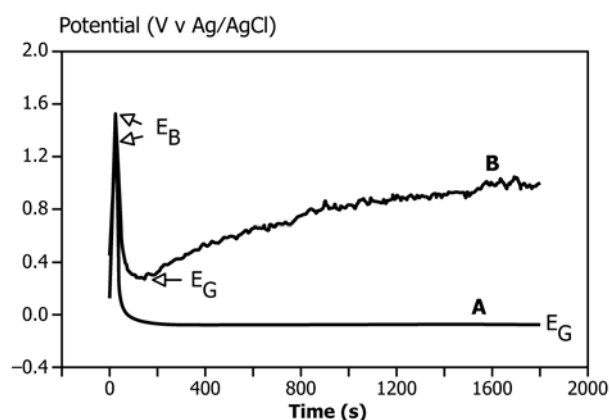
NOTE 1—A computer controlled system can be used in place of a current generator and recorder. In this case the current generator consists of a potentiostat/galvanostat operated in galvanostatic mode. The recorder is the computer. Software is used to control all aspects of the test protocol, including controlling the galvanostat, acquiring the data, plotting, and analysis.

8.9 Run the test in duplicate, steps 8.2 – 8.8

## 9. Interpretation of Results

9.1 *Break Potential,  $E_B$* —The graph in Fig. 2 illustrates two of the three possible forms of curve obtained in the experiment. In Fig. 2 there is an initial rapid rise in potential followed by a decrease. Record the maximum potential reached in this period as  $E_B$ . The third possibility is that the potential rises continuously, though perhaps oscillating. Record the maximum potential reached throughout the run. Express potential as  $V v SHE$  correcting for type of reference electrode used (see Appendix X1).

9.2 *Protection Potential  $E_G$* —For curves similar to curve A in Fig. 2, asymptotic decrease in potential after break, record the minimum potential reached, typically at the end of the run. For curves similar to curve B in Fig. 2, there is a decrease after the “break” followed by a series of rises and falls, record the



NOTE 1—Break potential,  $E_B$ , and protection potential,  $E_G$ , is indicated for each type of transient.

FIG. 2 Two Common Potential/Time Transient Profiles After Polarization

lowest potential reached on the first fall. Typically, subsequent rises and falls are small and appear as oscillations. For curves where the potential rises continuously,  $E_G$  will be equal to  $E_B$ . Express potential as  $V v SHE$ , correcting for type of reference electrode used (see Appendix X1).

9.3 *Curve Type*—Record whether curve is asymptotic (Type A), rising and falling (Type B), or rising only (Type C).

9.4 *Observations (optional)*—The following are optional observations that can be recorded as: evolution of gas bubbles during the test, description of surface after test, location of pits (for example, along scratch lines, etc. number of pits, depth of pits, area of pits, color of deposits, location of deposits in relation to pits, and other pitting evaluations as described in Guide G46).

## 10. Report

10.1 Report the following information:

10.1.1 Report aluminum alloy tested.

10.1.2 Report the average  $E_B$  and  $E_G$  of all experimental runs, at least two, for the formula.

10.1.3 Report type of curves obtained, A, B, or C. Report multiple types if obtained.

10.1.4 Report any visual observation made.

10.1.5 Many other relevant test parameters are given in Guide G107. These parameters should be recorded properly in laboratory notebooks for future reference.

## 11. Precision and Bias

11.1 *Precision*—The precision of this test method has not been determined. Round-robin testing will commence once final details of the method are determined. It is expected that the precision associated with the “break” potential will be less than the precision associated with the “protection” potential. It is also expected that precision will be constant over the range of measurement as opposite to being relative to the value of the measurement and insignificantly affected by the choice of aluminum alloy tested.

11.2 *Bias*:

11.2.1 *Statement on Bias*—This procedure has no bias because the values for the “break” and “protection” potentials are defined only in terms of this test method. An apparent bias will exist if the user does not correct the potentials for the

specific reference electrode used. Potential always must be expressed as relative to a standard hydrogen electrode (SHE) at the pH of use (see [Appendix X1](#)).

11.2.2 *Procedure to Determine Bias Due to Technique or Instrumentation*—The following procedure uses specific, published coolant specifications as controls to determine biases introduced due to one’s experimental technique or instrumentation. Results can be corrected for this bias. The two control formulas are Specification **D3585** with 0.2 wt % sodium nitrate and AL39, a coolant consisting of sodium sebacate and benzotriazole (see [Table 1](#)). Each formula is run at least five times. The mean and standard deviation are compared to the values determined in round robin testing (see [11.1](#)). The bias is calculated as the difference between the means.

**TABLE 1 Composition of Control Formulas**

Ingredient	Specification <b>D3585</b> (wt %)	AL39 (wt %)
Ethylene glycol	89.76	95.35
Diethylene glycol	5.00	
Sodium tetraborate, pentahydrate	3.06	
Trisodium phosphate, dodecahydrate	0.30	
Sodium mercaptobenzothiazole solution (50 wt % aqueous)	0.40	
Sodium nitrate (s)	0.20	
Pluronic L-61	0.02	
Water	1.36	
Sodium sebacate (s)		4.50
Benzotriazole (s)		0.15

## 12. Keywords

12.1 aluminum; corrosion; electrochemical measurement; galvanostatic; localized corrosion; polarization

## ANNEX

### (Mandatory Information)

#### A1. CORRECTING REFERENCE ELECTRODE READINGS TO STANDARD HYDROGEN ELECTRODE REFERENCE

##### A1.1 Temperature Compensation

A1.1.1 *Correction*—The experiment is run at room temperature, usually between 15° and 25°C. Temperature correction is applied to bring the reported potential up to the equivalent at 25°C. Add  $(25-T_r) \times E_T$ , where  $T_r$  is the room temperature and  $E_T$  is the temperature coefficient for the reference electrode used, [Table A1.1](#). For the common Ag/

AgCl and Hg/Hg<sub>2</sub>Cl<sub>2</sub> electrodes, then, the temperature correction is from 1 to 3 mV. This correction is insignificant when compared to the potential measurements made.

A1.1.2 *Example*—Measured potential is –0.345 mV against a saturated Cu/CuSO<sub>4</sub> reference electrode, room temperature is 18°C. Correction factor is  $(25-18) \times 0.90$  or +6.3 mV. Temperature corrected potential, then, is  $-0.345 + 0.0063$  equals  $-0.339$  V v Cu/CuSO<sub>4</sub> (at 25°C).

**TABLE A1.1 Reference Potentials and Conversion Factors (ref)**

Electrode	Potential (at 25°C) (V)	Temperature Coefficient (mV/°C)	To SHE Scale (V)
(Pt)/H <sub>2</sub> (a=1)/H <sup>+</sup> (a=1) (SHE)	0.000	+0.87	0.000
Ag/AgCl/sat KCl	+0.197		+0.197
Ag/AgCl/1M KCl	+0.235	+0.25	+0.235
Ag/AgCl/0.6 M Cl (seawater)	+0.250	...	+0.250
Hg/Hg <sub>2</sub> Cl <sub>2</sub> /sat KCl (SCE)	+0.241	+0.22	+0.241
Hg/Hg <sub>2</sub> Cl <sub>2</sub> /1 M KCl	+0.280	+0.59	+0.280
Cu/CuSO <sub>4</sub> sat	+0.300	+0.90	+0.300
Hg/Hg <sub>2</sub> SO <sub>4</sub> /H <sub>2</sub> SO <sub>4</sub>	+0.616	...	+0.616

##### A1.2 Correction to Standard Hydrogen Electrode

A1.2.1 *Correction*—Add the correction factor from the column “To SHE Scale” in [Table A1.1](#) for the reference electrode used to the measured potentials corrected for temperature. Express potential as x.xx v SHE (at 25°C).

A1.2.2 *Example*—The potential of  $-0.339$  V v Cu/CuSO<sub>4</sub> would be  $(-0.339+0.300)$  equals  $-0.039$  V v SHE (at 25°C). the potential of 0.850 V v sat Ag/AgCl would be  $(0.850 + 0.197)$  equals + 1.047 V v SHE (at 25°C).

APPENDIXES

(Nonmandatory Information)

X1. Schematic for Computer Controlled Galvanostat

X1.1 *Use of the Computer*—Computer control of the galvanostatic experiment is very convenient. The computer acts to control the galvanostat to produce the desired current density after a set (5 % min) delay, as well as, the recorder by acquiring the potential versus time data. Graphing of the data and data analysis also is common.

X1.2 *Potentiostat/Galvanostat* —This specialized piece of equipment is used for electrochemical experimentation. Several benefits accrue to use of this instrumentation, including stable polarization through use of feedback circuitry, unbiased

current measurement using a zero resistance ammeter, unbiased potential measurements using an infinite impedance voltmeter, and reduction in biases due to ground loop interferences.

X1.3 *Current Supply/Voltmeter*—This piece of equipment can be used with a computer, as well. In this case the current supply is computer controlled, or not, to provide the desired current. A computer interfaced voltmeter is used to digitize the potential signal to be read and stored by the computer.

X2. Luggin Probe Configurations

X2.1 *Integrated Luggin/Reference Electrode*—As shown in Fig. X2.1, this equipment consists of a 6-mm (1/4 in.) diameter glass tube with a fitting for the reference electrode at the upper end and a tip to narrow the bottom opening. The Luggin must be filled with test solution.

X2.1.1 *Fitting for the Reference Electrode*—This fitting must provide an air tight seal between the reference electrode and the Luggin to prevent solution in the Luggin from running out. Ground glass joints or O-ring seal joints work equally well. The choice depends on the manufacture of the reference electrode.

X2.1.2 *Tip to Narrow Opening*—This opening is conveniently constructed from a plastic disposal pipette. The flexibility of the plastic saves the tip from chipping as would be the case for the glass tube drawn out to a fine tip. A length of pipette is cut off and forced over the end of the glass tube to provide an air tight seal. Generally, this procedure requires some care as the fit must be very tight.

X2.2 *Salt Bridge and Reference Electrode*—This piece of equipment consists of three components including a salt bridge of high grade glass, which tapers to membrane seals at either end; a beaker containing a salt solution; and, the reference electrode, Fig. X2.2.

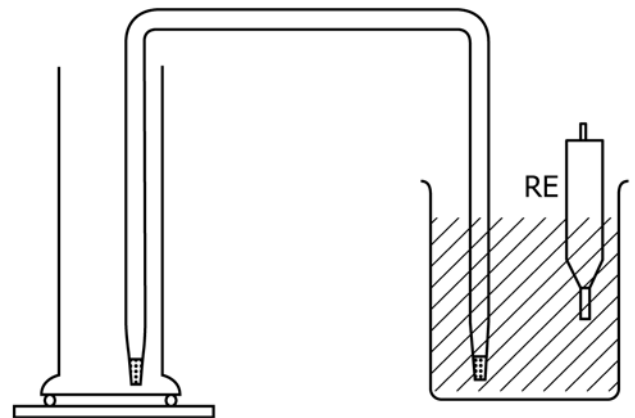


FIG. X2.2 Luggin Probe in the Form of a Salt Bridge

X2.2.1 *Salt Bridge*—This component is filled permanently with a highly conductive salt solution, terminating at both ends in a membrane such as porous high-silica. The bridge is constructed for the apparatus of interest, is this case providing a vertical shaft to get the tip close to the test specimen.

X2.2.2 *Beaker*—This component is filed with the salt solution used in the salt bridge. It is used to provide the electrical contact between the salt bridge and reference electrode.

X2.2.3 *Reference Electrode*—This component is any convenient type, which can be inserted into the beaker. This provides for a wider variety of electrodes, including a standard hydrogen electrode, to be used than might otherwise be possible.

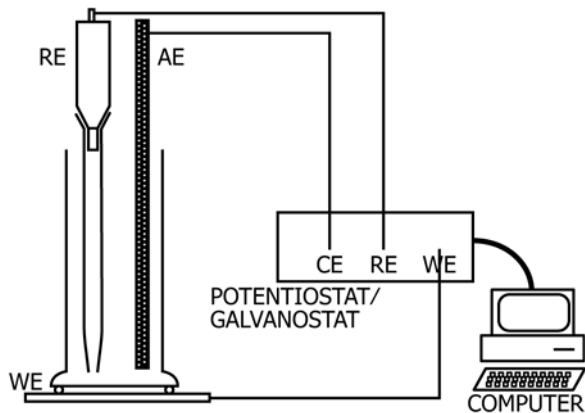


FIG. X2.1 Experimental Setup Using Computer Controlled Galvanostat

**REFERENCES**

- (1) Wiggle, R.R., “A. Rapid Method to Predict the Effectiveness of Inhibited Coolants in Aluminum Heat Exchangers”, SAE Paper No. 800800.
- (2) Sridhar, A. and Cragolino, G.A., “ Applicability of Repassivation Potential for Long Term Prediction of Localized Corrosion of Alloy 825 and Type 316L Stainless Steel”, Corrosion, November 1993, p. 885.
- (3) Truhan, J.J. and Hudgens, R.D., “ Effect of Nitrate Concentration on Passivation of Aluminum Alloys in Commercial Coolants for Heavy Duty Diesel Engines, SAE Paper No. 900436.
- (4) Hirozawa, S.T., “Galvanostaircase Polarization: A Powerful Technique for the Investigation of Localized Corrosion”, Paper No. 48 at the Electrochemical Society Meeting, October 1982.
- (5) Chyou, S.D. and Shih, H.C., “The Effect of Nitrogen on the Corrosion of Plasma-Nitrided 4140 Steel”, Corrosion, 47(1), 1991, p. 31.
- (6) Ford Laboratory Test Method BL 5-1, “A Rapid Method to Predict the Effectiveness of Inhibited Coolants in Aluminum Heat Exchangers.”

*ASTM International takes no position respecting the validity of any patent rights asserted in connection with any item mentioned in this standard. Users of this standard are expressly advised that determination of the validity of any such patent rights, and the risk of infringement of such rights, are entirely their own responsibility.*

*This standard is subject to revision at any time by the responsible technical committee and must be reviewed every five years and if not revised, either reapproved or withdrawn. Your comments are invited either for revision of this standard or for additional standards and should be addressed to ASTM International Headquarters. Your comments will receive careful consideration at a meeting of the responsible technical committee, which you may attend. If you feel that your comments have not received a fair hearing you should make your views known to the ASTM Committee on Standards, at the address shown below.*

*This standard is copyrighted by ASTM International, 100 Barr Harbor Drive, PO Box C700, West Conshohocken, PA 19428-2959, United States. Individual reprints (single or multiple copies) of this standard may be obtained by contacting ASTM at the above address or at 610-832-9585 (phone), 610-832-9555 (fax), or service@astm.org (e-mail); or through the ASTM website (www.astm.org). Permission rights to photocopy the standard may also be secured from the Copyright Clearance Center, 222 Rosewood Drive, Danvers, MA 01923, Tel: (978) 646-2600; <http://www.copyright.com/>*