<span id="page-0-0"></span>

## **Standard Practice for Underground Installation of Thermoplastic Pipe for Sewers and Other Gravity-Flow Applications1**

This standard is issued under the fixed designation D2321; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon  $(\varepsilon)$  indicates an editorial change since the last revision or reapproval.

*This standard has been approved for use by agencies of the U.S. Department of Defense.*

 $\varepsilon$ <sup>1</sup> NOTE[—X2.4](#page-10-0) was editorially corrected in September 2014.

### **1. Scope\***

1.1 This practice provides recommendations for the installation of buried thermoplastic pipe used in sewers and other gravity-flow applications. These recommendations are intended to ensure a stable underground environment for thermoplastic pipe under a wide range of service conditions. However, because of the numerous flexible plastic pipe products available and the inherent variability of natural ground conditions, achieving satisfactory performance of any one product may require modification to provisions contained herein to meet specific project requirements.

1.2 The scope of this practice necessarily excludes product performance criteria such as minimum pipe stiffness, maximum service deflection, or long term strength. Thus, it is incumbent upon the product manufacturer, specifier, or project engineer to verify and assure that the pipe specified for an intended application, when installed according to procedures outlined in this practice, will provide a long term, satisfactory performance according to criteria established for that application. A commentary on factors important in achieving a satisfactory installation is included in [Appendix X1.](#page-7-0)

NOTE 1—Specific paragraphs in the appendix are referenced in the body of this practice for informational purposes.

NOTE 2—The following ASTM standards may be found useful in connection with this practice: Practice [D420,](#page-7-0) Test Method D1556, Method D2216, Specification D2235, Test Method D2412, Specification D2564, Practice [D2657,](#page-1-0) Practice [D2855,](#page-1-0) Test Methods [D2922,](#page-1-0) Test Method [D3017,](#page-1-0) Practice [F402,](#page-1-0) Specification [F477,](#page-1-0) Specification [F545,](#page-1-0) and Specification [F913.](#page-1-0)

NOTE 3—Most Plumbing Codes and some Building Codes have provisions for the installation of underground "building drains and building sewers." See them for plumbing piping applications.

1.3 *Units—*The values stated in inch-pound units are to be regarded as standard. The values given in parentheses are

<sup>1</sup> This practice is under the jurisdiction of ASTM Committee [F17](http://www.astm.org/COMMIT/COMMITTEE/F17.htm) on Plastic Piping Systems and is the direct responsibility of Subcommittee [F17.62](http://www.astm.org/COMMIT/SUBCOMMIT/F1762.htm) on Sewer.

mathematical conversions to SI units that are provided for information only and are not considered standard.

1.4 *This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use.*

## **2. Referenced Documents**

- 2.1 *ASTM Standards:*<sup>2</sup>
- [D8](#page-1-0) [Terminology Relating to Materials for Roads and Pave](http://dx.doi.org/10.1520/D0008)[ments](http://dx.doi.org/10.1520/D0008)
- D420 [Guide to Site Characterization for Engineering Design](http://dx.doi.org/10.1520/D0420) [and Construction Purposes](http://dx.doi.org/10.1520/D0420) (Withdrawn  $2011$ )<sup>3</sup>
- [D653](#page-1-0) [Terminology Relating to Soil, Rock, and Contained](http://dx.doi.org/10.1520/D0653) [Fluids](http://dx.doi.org/10.1520/D0653)
- [D698](#page-1-0) [Test Methods for Laboratory Compaction Character](http://dx.doi.org/10.1520/D0698)istics of Soil Using Standard Effort (12 400 ft-lbf/ft $3$  (600  $kN-m/m^3$ )
- D1556 [Test Method for Density and Unit Weight of Soil in](http://dx.doi.org/10.1520/D1556) [Place by Sand-Cone Method](http://dx.doi.org/10.1520/D1556)
- D2216 [Test Methods for Laboratory Determination of Water](http://dx.doi.org/10.1520/D2216) [\(Moisture\) Content of Soil and Rock by Mass](http://dx.doi.org/10.1520/D2216)
- D2235 [Specification for Solvent Cement for Acrylonitrile-](http://dx.doi.org/10.1520/D2235)[Butadiene-Styrene \(ABS\) Plastic Pipe and Fittings](http://dx.doi.org/10.1520/D2235)
- D2412 [Test Method for Determination of External Loading](http://dx.doi.org/10.1520/D2412) [Characteristics of Plastic Pipe by Parallel-Plate Loading](http://dx.doi.org/10.1520/D2412)
- [D2487](#page-3-0) [Practice for Classification of Soils for Engineering](http://dx.doi.org/10.1520/D2487) [Purposes \(Unified Soil Classification System\)](http://dx.doi.org/10.1520/D2487)
- [D2488](#page-2-0) [Practice for Description and Identification of Soils](http://dx.doi.org/10.1520/D2488) [\(Visual-Manual Procedure\)](http://dx.doi.org/10.1520/D2488)
- D2564 [Specification for Solvent Cements for Poly\(Vinyl](http://dx.doi.org/10.1520/D2564) [Chloride\) \(PVC\) Plastic Piping Systems](http://dx.doi.org/10.1520/D2564)

#### **\*A Summary of Changes section appears at the end of this standard**

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<sup>2</sup> For referenced ASTM standards, visit the ASTM website, www.astm.org, or contact ASTM Customer Service at service@astm.org. For *Annual Book of ASTM Standards* volume information, refer to the standard's Document Summary page on the ASTM website.

<sup>&</sup>lt;sup>3</sup> The last approved version of this historical standard is referenced on www.astm.org.

<span id="page-1-0"></span>[D2657](#page-0-0) [Practice for Heat Fusion Joining of Polyolefin Pipe](http://dx.doi.org/10.1520/D2657) [and Fittings](http://dx.doi.org/10.1520/D2657)

- [D2855](#page-0-0) [Practice for Making Solvent-Cemented Joints with](http://dx.doi.org/10.1520/D2855) [Poly\(Vinyl Chloride\) \(PVC\) Pipe and Fittings](http://dx.doi.org/10.1520/D2855)
- [D2922](#page-0-0) [Test Methods for Density of Soil and Soil-Aggregate](http://dx.doi.org/10.1520/D2922) [in Place by Nuclear Methods \(Shallow Depth\)](http://dx.doi.org/10.1520/D2922) (Withdrawn  $2007$ <sup>3</sup>
- [D3017](#page-0-0) [Test Method for Water Content of Soil and Rock in](http://dx.doi.org/10.1520/D3017) [Place by Nuclear Methods \(Shallow Depth\)](http://dx.doi.org/10.1520/D3017)
- D3839 [Guide for Underground Installation of "Fiberglass"](http://dx.doi.org/10.1520/D3839) [\(Glass-Fiber Reinforced Thermosetting-Resin\) Pipe](http://dx.doi.org/10.1520/D3839)
- [D4318](#page-3-0) [Test Methods for Liquid Limit, Plastic Limit, and](http://dx.doi.org/10.1520/D4318) [Plasticity Index of Soils](http://dx.doi.org/10.1520/D4318)
- [F402](#page-0-0) [Practice for Safe Handling of Solvent Cements,](http://dx.doi.org/10.1520/F0402) [Primers, and Cleaners Used for Joining Thermoplastic](http://dx.doi.org/10.1520/F0402) [Pipe and Fittings](http://dx.doi.org/10.1520/F0402)

F412 [Terminology Relating to Plastic Piping Systems](http://dx.doi.org/10.1520/F0412)

- [F477](#page-0-0) [Specification for Elastomeric Seals \(Gaskets\) for Join](http://dx.doi.org/10.1520/F0477)[ing Plastic Pipe](http://dx.doi.org/10.1520/F0477)
- [F545](#page-0-0) [Specification for PVC and ABS Injected Solvent Ce](http://dx.doi.org/10.1520/F0545)[mented Plastic Pipe Joints](http://dx.doi.org/10.1520/F0545) (Withdrawn  $2001$ )<sup>3</sup>
- [F913](#page-0-0) [Specification for Thermoplastic Elastomeric Seals](http://dx.doi.org/10.1520/F0913) [\(Gaskets\) for Joining Plastic Pipe](http://dx.doi.org/10.1520/F0913)
- [F1668](#page-10-0) [Guide for Construction Procedures for Buried Plastic](http://dx.doi.org/10.1520/F1668) [Pipe](http://dx.doi.org/10.1520/F1668)

2.2 *AASHTO Standard:*<sup>4</sup>

[AASHTO M145](#page-4-0) Classification of Soils and Soil Aggregate Mixtures

## **3. Terminology**

3.1 *General—*Definitions used in this practice are in accordance with Terminologies F412 and D8 and Terminology D653 unless otherwise indicated.

3.2 *Definitions:*

3.2.1 Terminology [D653](#page-0-0) definitions used in this standard:

3.2.2 *compaction curve (Proctor curve) (moisture-density curve)—*the curve showing the relationship between the dry unit weight (density) and the water content of a soil for a given compactive effort.

3.2.3 *maximum unit weight—*the dry unit weight defined by the peak of a compaction curve.

3.2.4 *optimum water content—*the water content at which a soil can be compacted to a maximum dry unit weight by a given compactive effort.

3.2.5 *percent compaction—*the ratio, expressed as a percentage, of: *(1)* dry unit weight of a soil, to *(2)* maximum unit weight obtained in a laboratory compaction test.

3.3 *Definitions of Terms Specific to This Standard:*

3.3.1 *aggregate—*a granular material of mineral composition such as sand, gravel, shell, slag or crushed stone (see Terminology [D8\)](#page-0-0).

3.3.2 *deflection—*any change in the inside diameter of the pipe resulting from installation and imposed loads. Deflection may be either vertical or horizontal and is usually reported as a percentage of the base (undeflected) inside pipe diameter.

3.3.3 *engineer—*the engineer in responsible charge of the work or his duly recognized or authorized representative.

3.3.4 *foundation, bedding, haunching, initial backfill, final backfill, pipe zone, excavated trench width—*See Fig. 1 for meaning and limits, and trench terminology.

3.3.5 *manufactured aggregates—*aggregates such as slag that are products or byproducts of a manufacturing process, or natural aggregates that are reduced to their final form by a manufacturing process such as crushing.

3.3.6 *modulus of soil reaction (E')—*an empirical value used in the Iowa deflection formula that defines the stiffness of the soil embedment around a buried pipe

3.3.7 *open-graded aggregate—*an aggregate that has a particle size distribution such that, when it is compacted, the voids between the aggregate particles, expressed as a percentage of the total space occupied by the material, are relatively large.

3.3.8 *processed aggregates—*aggregates that are screened, washed, mixed, or blended to produce a specific particle size distribution.

3.3.9 *secant constrained soil modulus (Ms)—*- a value for soil stiffness determined as the secant slope of the stress-strain curve of a one-dimensional compression test;  $M<sub>s</sub>$  can be used in place of *E'* in the Iowa deflection formula.

3.3.10 *standard proctor density—*the maximum dry unit weight of soil compacted at optimum moisture content, as obtained by laboratory test in accordance with Test Methods D<sub>698</sub>

### **4. Significance and Use**

4.1 This practice is for use by designers and specifiers, installation contractors, regulatory agencies, owners, and inspection organizations who are involved in the construction of sewers and other gravity-flow applications that utilize flexible



**FIG. 1 Trench Cross Section**

<sup>4</sup> Available from American Association of State Highway and Transportation Officials (AASHTO), 444 N. Capitol St., NW, Suite 249, Washington, DC 20001, http://www.transportation.org.

<span id="page-2-0"></span>thermoplastic pipe. As with any standard practice, modifications may be required for specific job conditions or for special local or regional conditions. Recommendations for inclusion of this practice in contract documents for a specific project are given in [Appendix X2.](#page-10-0)

## **5. Materials**

5.1 *Classification—*Soil types used or encountered in burying pipes include those classified in [Table 1](#page-3-0) and natural, manufactured, and processed aggregates. The soil classifications are grouped into soil classifications in [Table 2](#page-4-0) based on the typical soil stiffness when compacted. Class I indicates a soil that generally provides the highest soil stiffness at any given percent compaction, and provides a given soil stiffness with the least compactive effort. Each higher-number soil class provides successively less soil stiffness at a given percent compaction and requires greater compactive effort to provide a given level of soil stiffness

NOTE 4—See Practices [D2487](#page-9-0) and [D2488](#page-0-0) for laboratory and field visual-manual procedures for identification of soils.

NOTE 5—Processed materials produced for highway construction, including coarse aggregate, base, subbase, and surface coarse materials, when used for foundation, embedment, and backfill, should be categorized in accordance with this section and [Table 1](#page-3-0) in accordance with particle size and gradation.

5.2 *Installation and Use—*[Table 3](#page-5-0) provides recommendations on installation and use based on soil classification and location in the trench. Soil Classes I to IV should be used as recommended in [Table 3.](#page-5-0) Soil Class V, including clays and silts with liquid limits greater than 50, organic soils, and frozen soils, shall be excluded from the pipe-zone embedment.

5.2.1 *Class I—*Class I materials provide maximum stability and pipe support for a given percent compaction due to the low content of sand and fines. With minimum effort these materials can be installed at relatively high-soil stiffnesses over a wide range of moisture contents. In addition, the high permeability of Class I materials may aid in the control of water, and these materials are often desirable for embedment in rock cuts where water is frequently encountered. However, when ground-water flow is anticipated, consideration should be given to the potential for migration of fines from adjacent materials into the open-graded Class I materials. (See [X1.8.](#page-8-0))

5.2.2 *Class II—*Class II materials, when compacted, provide a relatively high level of pipe support; however, open-graded groups may allow migration and the sizes should be checked for compatibility with adjacent material. (See [X1.8.](#page-8-0))

5.2.3 *Class III—*Class III materials provide less support for a given percent compaction than Class I or Class II materials. Higher levels of compactive effort are required and moisture content must be near optimum to minimize compactive effort and achieve the required percent compaction. These materials provide reasonable levels of pipe support once proper percent compaction is achieved.

5.2.4 *Class IV—*Class IV materials require a geotechnical evaluation prior to use. Moisture content must be near optimum to minimize compactive effort and achieve the required percent compaction. Properly placed and compacted, Class IV materials can provide reasonable levels of pipe support; however, these materials may not be suitable under high fills, surface-applied wheel loads, or under high-energy-level vibratory compactors and tampers. Do not use where water conditions in the trench may prevent proper placement and compaction.

NOTE 6—The term "high energy level vibratory compactors and tampers" refers to compaction equipment that might deflect or distort the pipe more than permitted by the specifications or the manufacturer.

5.2.5 *Class V—*Class V materials should be excluded from pipe-zone embedment.

5.3 *Moisture Content of Embedment Materials—*The moisture content of embedment materials must be controlled to permit placement and compaction to required levels. For soils with low permeability (that is, Class III and Class IV and some borderline Class II soils), moisture content is normally controlled to  $\pm$  3 % of optimum (see Test Method [D698\)](#page-0-0). The practicality of obtaining and maintaining the required limits on moisture content is an important criterion for selecting materials, since failure to achieve required percent compaction, especially in the pipe zone embedment, may result in excessive deflection.

5.4 *Maximum Particle Size—*Maximum particle size for embedment is limited to material passing a  $1\frac{1}{2}$ -in. (37.5-mm) sieve (see [Table 2\)](#page-4-0). To enhance placement around small diameter pipe and to prevent damage to the pipe wall, a smaller maximum size may be required (see  $X1.9$ ). When final backfill contains rocks, cobbles, etc., the engineer may require greater initial backfill cover levels (see [Fig. 1\)](#page-1-0).

### **6. Trench Excavation**

6.1 *General—*Procedures for trench excavation that are especially important in flexible thermoplastic pipe installations are given herein.

6.1.1 *Excavation—*Excavate trenches to ensure that sides will be stable under all working conditions. Slope trench walls or provide supports in conformance with all local and national standards for safety. Open only as much trench as can be safely maintained by available equipment. Backfill all trenches as soon as practicable, but not later than the end of each working day.

6.2 *Water Control—*Do not lay or embed pipe in standing or running water. At all times prevent runoff and surface water from entering the trench.

6.2.1 *Ground Water—*When groundwater is present in the work area, dewater to maintain stability of in-situ and imported materials. Maintain water level below pipe bedding and foundation to provide a stable trench bottom. Use, as appropriate, sump pumps, well points, deep wells, geofabrics, perforated underdrains, or stone blankets of sufficient thickness to remove and control water in the trench. When excavating while depressing ground water, ensure the ground water is below the bottom of cut at all times to prevent washout from behind sheeting or sloughing of exposed trench walls. Maintain control of water in the trench before, during, and after pipe

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### **TABLE 1 Soil Classification Chart (see Classification [D2487\)](#page-4-0)**

<span id="page-3-0"></span>

SW-SM well-graded sand with silt

SW-SC well-graded sand with clay

SP-SM poorly graded sand with silt

SP-SC poorly graded sand with clay<br>
J If Atterberg limits plot in hatched area, soil is a CL-ML, silty clay (see Test Method D4318).

*K* If soil contains 15 to 29 % plus No. 200, add "with sand" or "with gravel," whichever is predominant.

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- *L* If soil contains ≥ 30 % plus No. 200, predominantly sand, add "sandy" to group name.<br>
<sup>M</sup> If soil contains ≥ 30 % plus No. 200, predominantly gravel, add "sandy" to group name.<br>
<sup>M</sup> If soil contains ≥ 30 % plus No. 2
- 

*<sup>Q</sup>*PI plots below "A" line.

installation, and until embedment is installed and sufficient backfill has been placed to prevent flotation of the pipe. To preclude loss of soil support, employ dewatering methods that minimize removal of fines and the creation of voids in in-situ materials.

6.2.2 *Running Water—*Control running water emanating from drainage of surface or ground water to preclude undermining of the trench bottom or walls, the foundation, or other zones of embedment. Provide dams, cutoffs or other barriers periodically along the installation to preclude transport of

## **f**Uy D2321 – 14<sup>ε1</sup>

### **TABLE 2 Soil Classes**

<span id="page-4-0"></span>

<sup>A</sup> See Classification [D2487,](#page-2-0) Standard Classification of Soils for Engineering Purposes (Unified Soil Classification System).<br><sup>B</sup> Limits may be imposed on the soil group to meet project or local requirements if the specifi a Class I material with minimal fines to address specific structural or hydraulic conditions and the specification may read "Use Class I soil with a maximum of 5% passing

the #200 sieve."<br>
CAASHTO M145, Classification of Soils and Soil Aggregate Mixtures.

 $P$  All particle faces shall be fractured.<br>  $F$  Materials such as broken coral, shells, and recycled concrete, with  $\le$  =12% passing a No. 200 sieve, are considered to be Class II materials. These materials should only be used when evaluated and approved by the Engineer

*<sup>F</sup>* Uniform fine sands (SP) with more than 50% passing a No. 100 sieve (0.006 in., 0.15 mm) are very sensitive to moisture and should not be used as backfill unless specifically allowed in the contract documents. If use of these materials is allowed, compaction and handling procedures should follow the guidelines for Class III materials.

water along the trench bottom. Backfill all trenches after the pipe is installed to prevent disturbance of pipe and embedment.

6.2.3 *Materials for Water Control—*Use suitably graded materials in foundation or bedding layers or as drainage blankets for transport of running water to sump pits or other drains. Use well graded materials, along with perforated underdrains, to enhance transport of running water, as required. Select the gradation of the drainage materials to minimize migration of fines from surrounding materials (see [X1.8\)](#page-8-0).

6.3 *Minimum Trench Width—*Where trench walls are stable or supported, provide a width sufficient, but no greater than necessary, to ensure working room to properly and safely place and compact haunching and other embedment materials. The space between the pipe and trench wall must be wider than the compaction equipment used in the pipe zone. Minimum width shall be not less than the greater of either the pipe outside diameter plus 16 in. (400 mm) or the pipe outside diameter times 1.25, plus 12 in. (300 mm). In addition to safety considerations, trench width in unsupported, unstable soils will depend on the size and stiffness of the pipe, stiffness of the embedment and in-situ soil, and depth of cover (see [X1.10\)](#page-9-0). Specially designed equipment may enable the satisfactory installation and embedment of pipe in trenches narrower than specified above. If it is determined that the use of such equipment provides an installation consistent with the requirements of this standard, minimum trench widths may be reduced, as approved by the engineer.

6.4 *Support of Trench Walls—*When supports such as trench sheeting, trench jacks, trench shields or boxes are used, ensure that support of the pipe and its embedment is maintained throughout installation. Ensure that sheeting is sufficiently tight to prevent washing out of the trench wall from behind the sheeting. Provide tight support of trench walls below viaducts, existing utilities, or other obstructions that restrict driving of sheeting.

6.4.1 *Supports Left in Place—*Unless otherwise directed by the engineer, sheeting driven into or below the pipe zone should be left in place to preclude loss of support of foundation and embedment materials. When top of sheeting is to be cut off, make cut 1.5 ft (0.5 m) or more above the crown of the pipe. Leave rangers, whalers, and braces in place as required to support cutoff sheeting and the trench wall in the vicinity of the pipe zone. Timber sheeting to be left in place is considered a permanent structural member and should be treated against biological degradation (for example, attack by insects or other biological forms) as necessary, and against decay if above ground water.

NOTE 7—Certain preservative and protective compounds may react adversely with some types of thermoplastics, and their use should be avoided in proximity of the pipe material.

6.4.2 *Movable Trench Wall Supports—*Do not disturb the installed pipe and its embedment when using movable trench boxes and shields. Movable supports should not be used below the top of the pipe zone unless approved methods are used for



**TABLE 3 Recommendations for Installation and Use of Soils and Aggregates for Foundation and Pipe-Zone Embedment**

<span id="page-5-0"></span>

*<sup>A</sup>* Class V materials are unsuitable as embedment. They may be used as final backfill as permitted by the engineer.

*B* Class I materials have higher stiffness than Class II materials, but data on specific soil stiffness values are not available at the current time. Until such data are available the soil stiffness of placed, uncompacted Class I materials can be taken equivalent to Class II materials compacted to 95% of maximum standard Proctor density (SPD95), and the soil stiffness of compacted Class I materials can be taken equivalent to Class II materials compacted to 100% of maximum standard Proctor density (SPD100). Even if placed uncompacted (that is, dumped), Class I materials should always be worked into the haunch zone to assure complete placement.

C Suitable compaction typically achieved by dumped placement (that is, uncompacted but worked into haunch zone to ensure complete placement).<br>  $\frac{D}{D}$  SPD is standard Proctor density as determined by Test Method [D698.](#page-2-0)<br>

maintaining the integrity of embedment material. Before moving supports, place and compact embedment to sufficient depths to ensure protection of the pipe. As supports are moved, finish placing and compacting embedment.

6.4.3 *Removal of Trench Wall Support—*If the engineer permits the use of sheeting or other trench wall supports below the pipe zone, ensure that pipe and foundation and embedment materials are not disturbed by support removal. Fill voids left on removal of supports and compact all material as required.

6.5 *Rock or Unyielding Materials in Trench Bottom—*If ledge rock, hard pan, shale, or other unyielding material, cobbles, rubble or debris, boulders, or stones larger than 1.5 in. (40 mm) are encountered in the trench bottom, excavate a minimum depth of 6 in. (150 mm) below the pipe bottom and replace with proper embedment material (see [7.2.1\)](#page-6-0).

## **7. Installation**

7.1 *General—*Recommendations for use of the various types of materials classified in Section 5 and [Table 2](#page-4-0) for foundation, bedding, haunching and backfills, are given in Table 3.

NOTE 8—Installation of pipe in areas where significant settlement may be anticipated, such as in backfill adjacent to building foundations, and in sanitary landfills, or in other highly unstable soils, require special <span id="page-6-0"></span>engineering and are outside the scope of this practice.

7.2 *Trench Bottom—*Install foundation and bedding as required by the engineer according to conditions in the trench bottom. Provide a firm, stable, and uniform bedding for the pipe barrel and any protruding features of its joint. Provide a minimum of 4 in. (100 mm) of bedding unless otherwise specified.

7.2.1 *Rock and Unyielding Materials—*When rock or unyielding material is present in the trench bottom, install a cushion of bedding, of 6 in. (150 mm) minimum thickness, below the bottom of the pipe.

7.2.2 *Unstable Trench Bottom—*Where the trench bottom is unstable or shows a "quick'' tendency, excavate to a depth as required by the engineer and replace with a foundation of Class I or Class II material. Use a suitably graded material where conditions may cause migration of fines and loss of pipe support (see  $X1.8$ ). Place and compact foundation material in accordance with [Table 3.](#page-5-0) For severe conditions, the engineer may require a special foundation such as piles or sheeting capped with a concrete mat. Control of quick and unstable trench bottom conditions may be accomplished with the use of appropriate geofabrics.

7.2.3 *Localized Loadings—*Minimize localized loadings and differential settlement wherever the pipe crosses other utilities or subsurface structures, or whenever there are special foundations such as concrete capped piles or sheeting. Provide a cushion of bedding between the pipe and any such point of localized loading.

7.2.4 *Over-Excavation—*If the trench bottom is overexcavated below intended grade, fill the over-excavation with compatible foundation or bedding material and compact as recommended in [Table 3.](#page-5-0)

7.2.5 *Sloughing—*If trench sidewalls slough off during any part of excavating or installing the pipe, remove all sloughed and loose material from the trench.

7.3 *Location and Alignment—*Place pipe and fittings in the trench with the invert conforming to the required elevations, slopes, and alignment. Provide bell holes in pipe bedding, no larger than necessary, in order to ensure uniform pipe support. Fill all voids under the bell by working in bedding material. In special cases where the pipe is to be installed to a curved alignment, maintain angular "joint deflection'' (axial alignment) or pipe bending radius, or both, within acceptable design limits.

7.4 *Jointing—*Comply with manufacturer's recommendations for assembly of joint components, lubrication, and making of joints. When pipe laying is interrupted, secure piping against movement and seal open ends to prevent the entrance of water, mud, or foreign material.

7.4.1 *Elastomeric Seal Joints—*Protect gaskets from harmful substances such as dust and grit, solvents, and petroleumbased greases and oils. Do not store gaskets close to electrical equipment that produces ozone. Some gaskets may need to be protected from sunlight (consult the manufacturer). Mark, or verify that pipe ends are marked, to indicate insertion stop position, and ensure that pipe is inserted into pipe or fitting bells to this mark. Push spigot into bell using methods recommended by the manufacturer, keeping pipe true to line and grade. Protect the end of the pipe while inserting the spigot into the bell and do not use excessive force that may result in over-assembled joints or dislodged gaskets. If full entry to the specified insertion depth is not achieved, disassemble and clean the joint and reassemble. Use only lubricant supplied or recommended for use by the pipe manufacturer. Do not exceed manufacturer's recommendations for angular "joint deflection'' (axial alignment).

7.4.2 *Solvent Cement Joints—*When making solvent cement joints, follow recommendations of both the pipe and solvent cement manufacturer. If full entry is not achieved, disassemble or remove and replace the joint. Allow freshly made joints to set for the recommended time before moving, burying, or otherwise disturbing the pipe.

7.4.3 *Heat Fusion Joints—*Make heat fusion joints in conformance with the recommendations of the pipe manufacturer. Pipe may be joined at ground surface and then lowered into position, provided it is supported and handled in a manner that precludes damage.

7.5 *Placing and Compacting Pipe Embedment—*Place embedment materials by methods that will not disturb or damage the pipe. Work in and tamp the haunching material in the area between the bedding and the underside of the pipe before placing and compacting the remainder of the embedment in the pipe zone. Follow recommendations for compaction given in [Table 2.](#page-4-0) Do not permit compaction equipment to contact and damage the pipe. Use compaction equipment and techniques that are compatible with materials used and location in the trench (see  $X1.7$ ). Before using heavy compaction or construction equipment directly over the pipe, place sufficient backfill to prevent damage, excessive deflections, or other disturbance of the pipe. See 7.6 for minimum cover.

7.5.1 *Percent Compaction of Embedment—* The Soil Class (from [Table 2\)](#page-4-0) and the required percent compaction of the embedment should be established by the engineer based on an evaluation of specific project conditions (see [X1.6.2\)](#page-8-0). The information in [Table 3](#page-5-0) will provide satisfactory embedment stiffness and is based on achieving an average modulus of soil reaction, *E'*, of 1000 psi (or an appropriate equivalent constrained modulus,  $M_s$ ).

7.5.2 *Consolidation by Watering—*Consolidation of cohesionless material by using water (jetting or puddling) should only be used under controlled conditions when approved by the engineer. At all times conform to the lift thicknesses and the compaction requirements given in [Table 3.](#page-5-0)

7.6 *Minimum Cover—*To preclude damage to the pipe and disturbance to pipe embedment, a minimum depth of backfill above the pipe should be maintained before allowing vehicles or heavy construction equipment to traverse the pipe trench. The minimum depth of cover should be established by the engineer based on an evaluation of specific project conditions. In the absence of an engineering evaluation, the following minimum cover requirements should be used. For embedment materials installed in accordance with [Table 3,](#page-5-0) provide cover (that is, depth of backfill above top of pipe) of at least 24 in. (0.6 m) or one pipe diameter (whichever is larger) for Class I embedment, and a cover of at least 36 in. (0.9 m) or one pipe

<span id="page-7-0"></span>diameter (whichever is larger) for Class II, III, and IV embedment, before allowing vehicles or construction equipment to traffic the trench surface, and at least 48 in. (1.2 m) of cover before using a hydrohammer for compaction. Do not use hydrohammer-type compactors unless approved by the engineer. Where construction loads may be excessive (for example, cranes, earth moving equipment, etc.), minimum cover shall be increased as determined by the engineer.

7.7 *Vertical Risers—*Provide support for vertical risers as commonly found at service connections, cleanouts, and drop manholes to preclude vertical or lateral movement. Prevent the direct transfer of thrust due to surface loads and settlement, and ensure adequate support at points of connection to main lines.

7.8 *Exposing Pipe for Making Service Line Connections—* When excavating for a service line connection, excavate material from above the top of the existing pipe before removing material from the sides of the pipe. Materials and percent compaction of service line embedment should conform to the specifications for the existing line, or with this practice, whichever is more stringent.

NOTE 9—Special construction techniques and considerations are required when more than one pipe is installed in the same or adjacent trenches, to ensure that the integrity of the embedment is maintained.

7.9 *Pipe Caps and Plugs—*Secure caps and plugs to the pipe to prevent movement and resulting leakage under test and service pressures.

7.10 *Manhole Connections—*Use flexible water stops, resilient connectors, or other flexible systems approved by the engineer to make watertight connections to manholes and other structures.

7.11 *Field Monitoring—*Compliance with contract documents with respect to pipe installation, including trench depth, grade, water conditions, foundation, embedment and backfill materials, joints, density of materials in place, and safety, should be monitored by the engineer at a frequency appropriate to project requirements. Leakage testing specifications, while not within the scope of this practice, should be made part of the specifications for plastic pipe installations, when applicable.

### **8. Inspection, Handling, and Storage**

8.1 *Inspection—*Upon receipt, inspect each shipment of pipe and fittings for conformance to product specifications and contract documents, and check for damage. Reject nonconforming or damaged pipe, and remove from the job. If not returned to supplier, dispose of legally.

8.2 *Handling and Storage—*Handle and store pipe and fittings in accordance with recommendations of the manufacturer.

## **9. Keywords**

9.1 backfill; bedding; compaction; embedment; haunching; migration; sewer pipe; soil stiffness; thermoplastic; underground installation

## **APPENDIXES**

### **(Nonmandatory Information)**

### **X1. COMMENTARY**

X1.1 Those concerned with the service performance of a buried flexible pipe should understand factors that can affect this performance. Accordingly, key considerations in the design and execution of a satisfactory installation of buried flexible thermoplastic pipe that provided a basis for the development of this practice are given in this Appendix.

X1.2 *General*—Sub-surface conditions should be adequately investigated prior to construction, in accordance with Practice [D420,](#page-0-0) as a basis for establishing requirements for foundation, embedment and backfill materials and construction methods. The type of pipe selected should be suited for the job conditions.

X1.3 *Load/Deflection Performance*—The thermoplastic pipes considered in this practice are classified as flexible conduits since in carrying load they deform (deflect) to develop support from the surrounding embedment. This interaction of pipe and soil provides a pipe-soil structure capable of supporting earth fills and surface live loads of considerable magnitude. The design, specification and construction of the buried flexible pipe system should recognize that embedment materials must be selected, placed and compacted so that pipe and soil act in concert to carry the applied loads without excessive strains from deflections or localized pipe wall distortions.

X1.4 *Pipe Deflection*—Pipe deflection is the diametral change in the pipe-soil system resulting from the process of installing the pipe (construction deflection), static and live loads applied to the pipe (load-induced deflection), and time dependent soil response (deflection lag). Construction and load induced deflections together constitute initial pipe deflection. Additional time dependent deflections are attributed primarily to changes in embedment and in-situ soils, and trench settlement. The sum of initial and time dependent deflections constitutes total deflection.

X1.4.1 *Construction Deflection—*Construction deflections are induced during the process of installing and embedding flexible pipe, even before significant earth and surface loads are applied. The magnitude of construction deflections depends on such factors as the method and extent of compaction of the embedment materials, type of embedment, water conditions in the trench, pipe stiffness, uniformity of embedment support,

<span id="page-8-0"></span>pipe out-of-roundness, and installation workmanship in general. These deflections may exceed the subsequent loadinduced deflections. Compaction of the side fill may result in negative vertical deflections (that is, increases in pipe vertical diameter and decreases in horizontal diameter).

X1.4.2 *Load-Induced Deflection—*Load-induced deflections result from backfill loads and other superimposed loads that are applied after the pipe is embedded. Traditionally, typical soil-structure interaction equations such as the "Iowa Formula'', attributed to Spangler, or other methods have been used to calculate deflections resulting from these loads.

X1.4.3 *Initial Deflection—*Initial deflection is the deflection in the installed and backfilled pipe. It is the total of construction deflections and load-induced deflections.

X1.4.4 *Time Dependent Factors—*Time dependent factors include changes in soil stiffness in the pipe embedment zone and native trench soils, as well as loading changes due to trench settlement over time. These changes typically add to initial deflections; the time involved varies from a few days to several years depending on soil types, their placement, and initial compaction. Time dependent factors are traditionally accounted for by adjusting load-induced deflections by a deflection lag factor. Selection of a deflection lag factor is considered in design guides for buried flexible pipe.

X1.4.5 *Final Deflection—*Final deflection is the total long term deflection of the pipe. It consists of initial deflection adjusted for time dependent factors.

X1.5 *Deflection Criteria*—Deflection criteria are often set as limits for the design and acceptance of buried flexible pipe installation. Deflection limits for specific pipe systems may be derived from both structural and practical considerations. Structural considerations include pipe cracking, yielding, strength, strain, and local distortion. Practical considerations include such factors as flow requirements, clearance for inspection and cleaning, and maintenance of joint seals. Initial and final deflection limits should be based on available structural properties with suitable factors of safety applied.

NOTE X1.1—Some ASTM standard specifications for thermoplastic pipe, such as Specifications D3034, F679, F714, and F949, provide recommended limits for installed deflections.

NOTE X1.2—Deflections may not be indicative of strain levels arising from local distortions caused by non-uniform embedment stiffness or localized loadings. When local distortions may be significant, the engineer needs to establish methods for controlling and monitoring distortion levels.

X1.6 *Deflection Control*—Embedment materials should be selected, placed, and compacted so as to minimize total deflections and, in any event, to maintain installed deflections within specific limits. Methods of placement, compaction, and moisture control should be selected based on soil types given in [Table 1](#page-3-0) and [Table 2](#page-4-0) and on recommendations given in [Table](#page-5-0) [3.](#page-5-0) The amount of load-induced deflection is primarily a function of the stiffness of the pipe and soil embedment system. Other factors that are important in obtaining deflection control are outlined below.

X1.6.1 *Embedment at Pipe Haunches—*Lack of adequate compaction of embedment material in the haunch zone can result in excessive deflection, since it is this material that supports the vertical loads applied to the pipe. A key objective during installation of flexible thermoplastic pipe (or any pipe) is to work in and compact embedment material under pipe haunches, to ensure complete contact with the pipe bottom, and to fill voids below the pipe.

X1.6.2 *Embedment Compaction—*Embedment compaction requirements should be determined by the engineer based on deflection limits established for the pipe, pipe stiffness, and installation quality control, as well as the characteristics of the in-situ soil and compactibility characteristics of the embedment materials used. The compaction requirements given in [Table 3](#page-5-0) are based on attaining an average modulus of soil reaction (E') of  $1000 \text{ psi}^5$  (or an appropriate equivalent constrained modulus,  $M<sub>s</sub>$ ), which relates soil stiffness to soil type and degree of compaction. For particular installations, the project engineer should verify that the percent compaction specified meets performance requirements.

X1.7 *Compaction Methods*—Achieving desired compaction for specific types of materials depends on the methods used to impart compactive energy. Coarse-grained, clean materials such as crushed stone, gravels, and sand are more readily compacted using vibratory equipment, whereas fine materials with high plasticity require kneading and impact force along with controlled water content to achieve acceptable compaction (see [5.3\)](#page-2-0). In pipe trenches, small, hand-held or walk-behind compactors are required, not only to preclude damage to the pipe, but to ensure thorough compaction in the confined areas around the pipe and along the trench wall. As examples, vibratory plate tampers work well for coarse grained materials of Class I and Class II, whereas hand tampers or air driven hand-held impact rammers are suitable for the finegrained, plastic groups of Class III and IV. Gas or diesel powered jumping jacks or small, walk-behind vibratory rollers impart both vibratory and kneading or impact force, and hence are suitable for most classes of embedment and backfill material.

X1.8 *Migration*—When coarse and open-graded material is placed adjacent to a finer material, fines may migrate into the coarser material under the action of hydraulic gradient from ground water flow. Significant hydraulic gradients may arise in the pipeline trench during construction when water levels are being controlled by various pumping or well-pointing methods, or after construction when permeable underdrain or embedment materials act as a "french'' drain under high ground water levels. Field experience shows that migration can result in significant loss of pipe support and continuing deflections that may exceed design limits. The gradation and relative size of the embedment and adjacent materials must be compatible in order to minimize migration (see  $X1.8.1$  below). In general, where significant ground water flow is anticipated, avoid placing coarse, open-graded Class I materials above, below, or adjacent to finer materials, unless methods are employed to impede

<sup>5</sup> Howard, Amster, "Modulus of Soil Reaction Values for Buried Flexible Pipe," *Journal of Geotechnical Engineering*, ASCE, Vol. 103, No. GT1, 1977.

<span id="page-9-0"></span>migration such as the use of an appropriate stone filter or filter fabric along the boundary of the incompatible materials. To guard against loss of pipe support from lateral migration of fines from the trench wall into open-graded embedment materials, it is sufficient to follow the minimum embedment width guidelines in X1.10.

X1.8.1 The following filter gradation criteria may be used to restrict migration of fines into the voids of coarser material under a hydraulic gradient:

X1.8.1.1  $D_{15}$  /  $d_{85}$  < 5 where  $D_{15}$  is the sieve opening size passing 15 % by weight of the coarser material and  $d_{85}$  is the sieve opening size passing 85 % by weight of the finer material, and

X1.8.1.2 *D*  $_{50}/d_{50}$  < 25 where  $D_{50}$  is the sieve opening size passing 50 % by weight of the coarser material and  $d_{50}$  is the sieve opening size passing 50 % by weight of the finer material. This criterion need not apply if the coarser material is well-graded (see Test Method [D2487\)](#page-0-0).

X1.8.1.3 If the finer material is a fine-grained soil (CL, CH, ML, or MH), then the following criterion may be used in lieu of X1.8.1.1:  $D_{15}$  < 0.02 in. (0.5 mm) where  $D_{15}$  is the sieve opening size passing 15 % by weight of the coarser material.

NOTE X1.3—Materials selected for use based on filter gradation criteria, such as in X1.8.1, should be handled and placed in a manner that will minimize segregation.

X1.9 *Maximum Particle Size*—Limiting particle size to 3⁄4 in. (20 mm) or less enhances placement of embedment material for nominal pipe sizes 8 in. (200 mm) through 15 in. (380 mm). For smaller pipe, a particle size of about 10 % of the nominal pipe diameter is recommended.

X1.10 *Embedment Width for Adequate Support*—In certain conditions, a minimum width of embedment material is required to ensure that adequate embedment stiffness is developed to support the pipe. These conditions arise where in-situ lateral soil resistance is negligible, such as in very poor native soils or along highway embankments. Examples of poor native soils include poorly compacted soils with blow counts of five or less, peat, muck, or highly expansive soils. Under these conditions, if the native soil is able to sustain a vertical cut, the minimum embedment width shall be 0.5 pipe diameters on either side of the pipe as shown in Fig. X1.1. Under these conditions, if the native soil cannot sustain a vertical cut or if it is an embankment situation, the minimum embedment width shall be one pipe diameter on either side of the pipe as shown in [Fig. X1.2.](#page-10-0) In either case, the embedment material shall be a Class II granular material or a Class I crushed rock as specified in Section [5](#page-2-0) of this standard. If other embedment materials are used, the engineer should establish the minimum embedment width based on an evaluation of parameters such as pipe stiffness, embedment stiffness, nature of in-situ soil, and magnitude of construction and service loads. Regardless of the trench width required for adequate support, the trench must be of sufficient width to allow the proper placement of embedment in accordance with [6.3.](#page-4-0)

NOTE X1.4—Installation in very poor soil conditions may require additional treatment, for example, soil stabilization or permanent sheeting. NOTE X1.5—The embedment over the top of the pipe shown in Fig.



**FIG. X1.1 Minimum Embedment Width When Trench and Native Soil Can Sustain a Vertical Cut**

X1.1 and [Fig. X1.2](#page-10-0) represent minimum cover for impact protection, not for pipe support. Regardless of the minimum cover shown, the requirements of [7.6](#page-6-0) must be met.

NOTE [X1.6](#page-8-0)—Refer to X1.6 for backfill material and compaction requirements to control deflection.

X1.11 *Lumps, Clods and Boulders*—Backfill materials should be free of lumps, clods, boulders, frozen matter, and debris. The presence of such material in the embedment may preclude uniform compaction and result in excessive localized deflections.

X1.12 *Other Design and Construction Criteria*—The design and construction of the pipe system should recognize conditions that may induce excessive shear, longitudinal bending, or compression loading in the pipe. Live loads applied by construction and service traffic may result in large, cumulative pipe deflections if the pipe is installed with a low density embedment and shallow cover. Other sources of loads on buried pipes are: freezing and thawing of the ground in the vicinity of the pipe, rising and falling of the ground water table, hydrostatic pressure due to ground water, and localized differential settlement loads occurring next to structures such as manholes and foundations. Where external loads are deemed to be excessive, the pipe should be installed in casing pipe or other load limiting structures.

X1.13 *Deflection Testing*—To ensure specified deflection limits are not exceeded, the engineer may require deflection testing of the pipe using specified measuring devices. To allow for stabilization of the pipe soil system, deflection tests should be performed at least 30 days after installation. However, as a quality control measure, periodic checks of deflection may be made during installation.

X1.13.1 Optional devices for deflection testing include electronic deflectometers, calibrated television or video

<span id="page-10-0"></span>

**FIG. X1.2 Minimum Embedment Width When Native Soil Can Not Sustain a Vertical Cut or When Installed in the Embankment Condition**

cameras, or a properly sized "go, no-go'' mandrel. Deflection measurements can be made directly with extension rulers or tape measures in lines that permit safe entry. To ensure accurate measurements, clean the lines before testing.

X1.14 *Additional Installation Information–*Supplemental information useful for buried pipe installation can be found in Practice [F1668.](#page-1-0)

### **X2. RECOMMENDATIONS FOR INCORPORATION IN CONTRACT DOCUMENTS**

X2.1 This practice may be incorporated, by referral, into contract documents for a specific project to cover requirements for installation of flexible thermoplastic pipe in sewers and other gravity-flow applications. Application to a particular project should be made by means of a list of supplemental requirements. Suggested modifications to specific sections are listed below (the list is keyed to applicable section numbers of this practice):

X2.2 *Sections [5.1,](#page-2-0) [5.2,](#page-2-0) and* [Table 3—](#page-5-0)Further restrictions on use of Classes of embedment and backfill materials.

X2.3 *Section [5](#page-2-0)*—Specific gradations of embedment materials for resistance to migration.

X2.4 *Section [5.4](#page-2-0)*—Maximum particle size, if different from [Table 2.](#page-4-0)

X2.5 *Section [6.2](#page-2-0)*—Restrictions on mode of dewatering; design of underdrains.

X2.6 *Section [6.3](#page-4-0)*—Requirements on minimum trench width.

X2.7 *Section [6.4](#page-4-0)*—Restrictions or details for support of trench walls.

X2.8 *Section [7.5](#page-6-0)*—Specific restrictions on methods of compaction.

X2.9 *Section [7.5.1](#page-6-0) and* [Table 3—](#page-5-0)Minimum embedment percent compaction if different from these recommendations; specific compaction requirements for backfill (for example, for pavement subgrade).

X2.10 *Section [7.6](#page-6-0)*—Minimum cover requirements if different from this paragraph.

X2.11 *Section [7.7](#page-7-0)*—Detailed requirements for support of vertical risers, standpipes, and stacks to accommodate anticipated relative movements between pipe and such appurtenances. Detailing to accommodate thermal movements, particularly at risers.

X2.12 *Section [7.10](#page-7-0)*—Detailed requirements for manhole connections.

X2.13 *Section [7.11](#page-7-0)*—Requirements on methods of testing compaction and leakage.

X2.14 *Section [X1.13](#page-9-0)*—Requirements on deflection and deflection measurements, including method and time of testing.



## **SUMMARY OF CHANGES**

Committee F17 has identified the location of selected changes to this standard since the last issue (D2321–11) that may impact the use of this standard. (Approved August 1, 2014.)

*(1)* [Table 3](#page-5-0) was revised.

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