

Standard Test Method for Dilute Solution Viscosity of Ethylene Polymers¹

This standard is issued under the fixed designation D1601; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon (ε) indicates an editorial change since the last revision or reapproval.

1. Scope*

- 1.1 This test method covers the determination of the dilute solution viscosity of ethylene polymers at 135°C. It is applicable to a reasonably wide spectrum of ethylene polymers having densities from 0.910 to 0.970 g/cm². Directions are given for the determination of relative viscosity (viscosity ratio), inherent viscosity (logarithmic viscosity number), and intrinsic viscosity (limiting viscosity number) (see Appendix X4).
- 1.2 The values as stated in SI units are to be regarded as the standard.
- 1.3 This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use.

Note 1—This test method is technically equivalent to ISO 1628-3.

Note 2—Appendix X1 – Appendix X3 contain material from the previous version of Test Method D1601 and are included for information only.

2. Referenced Documents

2.1 ASTM Standards:²

D86 Test Method for Distillation of Petroleum Products at Atmospheric Pressure

D445 Test Method for Kinematic Viscosity of Transparent and Opaque Liquids (and Calculation of Dynamic Viscosity)

D883 Terminology Relating to Plastics

D1600 Terminology for Abbreviated Terms Relating to Plas-

D4020 Specification for Ultra-High-Molecular-Weight Polyethylene Molding and Extrusion Materials

E1 Specification for ASTM Liquid-in-Glass Thermometers

IEEE/ASTM SI-10 Standard for Use of the International System of Units (SI): The Modern Metric System 2.2 *ISO Standards:*³

ISO 1628-3 Plastics—Determination of Viscosity Number and Limiting Viscosity Number—Part 3: Polyethylenes and Polypropylenes

3. Terminology

3.1 Units, symbols, and abbreviations used in this test method are those recommended in IEEE/ASTM SI-10 and Terminologies D883 and D1600 (see also Appendix X4).

4. Significance and Use

- 4.1 The knowledge of dilute solution viscosity serves as an additional tool in characterizing ethylene polymers. Viscosity data alone may be of limited value in predicting the processing behavior of the polymer. However, when used in conjunction with other flow and physical property values, the solution viscosity of ethylene polymers may contribute to their characterizations.
- 4.2 Satisfactory correlation between solution viscosity and certain other properties is possible from polymers of a single manufacturing process. The solution viscosity test is not sensitive to some molecular configurational patterns that may occur among polymers from different manufacturing processes. Hence, its correlation with other properties of polymers produced by different processes, by even one manufacturer, may be limited.
- 4.3 The viscosity of polymer solutions may be drastically affected by the presence of known or unknown additives in the sample. The use of solution viscosity may be of questionable value where ethylene polymers are known or suspected to contain colorants, carbon black, low molecular weight hydrocarbons, fillers, or other additives.
- 4.4 The measurement of dilute solution viscosity of ethylene polymers presents problems not ordinarily encountered in viscosimetry. Ethylene polymers are not soluble at room temperature in any known solvent. Some of the higher density materials are insoluble below 100°C. Extreme care must be exercised in transferring the solution to the viscometer for the

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² For referenced ASTM standards, visit the ASTM website, www.astm.org, or contact ASTM Customer Service at service@astm.org. For *Annual Book of ASTM Standards* volume information, refer to the standard's Document Summary page on the ASTM website.

 $^{^3}$ Available from American National Standards Institute (ANSI), 25 W. 43rd St., 4th Floor, New York, NY 10036.

test if the correct solution concentration is to be maintained. This test has no significance unless the sample is completely soluble.

4.5 The solution viscosity is a function of the root-mean-square size of the polymer molecules in solution. It is known that the solvent selected and the temperature of the determination have an effect on the root-mean-square size of the particles. Hence, where a viscometer, solvent, or temperature other than specified is used, data may not be comparable to that obtained by this procedure.

5. Apparatus

- 5.1 Volumetric Flasks, 100-mL, grade EXAX or better.4
- 5.2 Transfer Pipets, Grade EXAX or better.4
- 5.3 Constant Temperature Bath, capable of maintaining 135 \pm 10.1°C.
- 5.4 *Viscometer*, Ubbelohde No. 1, calibrated for kinetic energy correction constant.

Note 3—Other types of viscometers may be used provided they can be shown to agree with the type specified.

- 5.5 Oven, maintained at 140 ± 5 °C.
- 5.6 *Timer*, as specified in 4.5 of Test Method D445.
- 5.7 Thermometer—An ASTM High Softening Point Thermometer having a range from 30 to 200°C, and conforming to the requirements for Thermometer 16C in Specification E1. Thermometric devices such as resistance temperature detectors (RTDs), having accuracies equal to or better than Thermometer 16C in the specified temperature range are also appropriate for use.

6. Reagents and Materials

- 6.1 *Solvent—Decahydronaphthalene*, practical grade, purified and redistilled, as follows:
- 6.1.1 The solvent shall be purified by percolation through 100 to 200 mesh commercial grade silica gel. This treatment removes naphthalene, tetrahydronaphthalene, and oxy compounds, particularly peroxides.
- 6.1.2 The redistilled product shall conform to the following requirements when tested in accordance with Method D86:

	ASTM		
Standard Distillation	Method D86		
Initial boiling point	190°C min		
10 mL	191°C min		
20 mL	192°C min		
80 mL	194°C max		
90 mL	195°C max		
Dry point	196°C max		

Note 4—While use of other solvents, such as tetrahydronaphthalene or xylene, may sometimes be advantageous, they will generally yield different values for solution viscosities.

6.1.3 Immediately after redistillation of the decahydronaphthalene, add 0.2 % Tetrakis [methylene 3-(3',5'-

di-tert-butyl-4'-hydroxphenyl) propionate] methane to inhibit oxidation during the viscosity determination.

6.2 *Heat Transfer Medium*—Any liquid heat transfer medium that will not appreciably affect the accuracy of the test may be used. Care should be exercised in using fluids that discolor or smoke with prolonged heating.

Note 5—Silicone heat-transfer fluids are adequate for this use⁵.

7. Procedure

- 7.1 Decahydronaphthalene Preparation—Add 0.2 % weight/volume stabilizer (Irganox 1010 or equivalent), to the decahydronaphthalene, stir to dissolve, filter through fast filter paper, and store in a clean amber bottle.
- 7.2 Cleaning the Viscometer—Clean the viscometer thoroughly as follows: fill with cleaning solution, let stand overnight, empty and rinse several times with distilled water, then rinse with acetone and purge with dry nitrogen.
- 7.3 Solution Preparation—Weigh 20 to 30 mg of the UH-MWPE (see Note 6) into the Erlenmeyer flask. Add the decahydronaphthalene at room temperature, using a burette to measure in milliliters a volume equal to 4.5 times the UHM-WPE weight in milligrams (for example, 26 mg of UHMWPE and 117 ml of decahydronaphthalene). Heat the flask, with stirring, to $150^{\circ}\text{C} \pm 2^{\circ}\text{C}$. Continue stirring at $150^{\circ}\text{C} \pm 2^{\circ}\text{C}$ for 1 h, with the flask lightly stoppered. Examine the flask to see if undissolved UHMWPE remains. If so, heat an additional 15 min and reexamine. Heat for an additional 15 min, if necessary, but do not heat longer than 2 h total.
 - 7.4 Viscosity Measurement:
- 7.4.1 Place the clean viscometer into the constanttemperature bath. Fill the viscometer decahydronaphthalene, and allow it and the solvent to equilibrate at 135 \pm 0.1°C. Measure the flow time of the solvent, t_o , three times, and average the results. The viscometer may have to be cleaned if replicate measurements of flow time differ by more than 0.3 s (see 7.4.3). Remove the decahydronaphthalene from the viscometer with vacuum and thoroughly rinse the viscometer with xylene at 110 to 120°C or decahydronaphthalene at 135°C. Remove the xylene or decahydronaphthalene with vacuum and aspirate dry air or nitrogen to dry the viscometer (2 or 3 min). It is essential that the viscometer be completely dry.
- 7.4.2 Transfer the hot (150°C) polymer solution to the viscometer with sufficient quantity to fill to the mark (see Note 7), allow to equilibrate at 135°C \pm 0.1°C, and measure the flow time of the solution, t_s , in triplicate, and average the results.
- 7.4.3 Between uses, clean the viscometer by rinsing with hot xylene or decahydronaphthalene, drying with air or nitrogen, and storing filled with hot decahydronaphthalene. If solvent flow time changes by more than 0.3 s, or if difficulty is

⁴ Glassware used in this test method should be tested in accordance with the procedures described in the National Institute of Standards and Technology Circular No. C-434, "Testing of Glass Volumetric Apparatus," and should not exceed the limits of accuracy set forth in the circular.

⁵ The silicone fluids available from the Dow Corning Corp., Midland, MI, or from the Union Carbide Corp., Linde Silicones Div., New York, NY, have been found satisfactory for this purpose.

encountered in obtaining reproducible flow times with any solution or solvent, clean the viscometer with cleaning solution as described in 7.2.

Note 6—If the UHMWPE is suspected to contain moisture or other volatiles, it shall first be dried in a vacuum oven at 60° C for 2 h.

NOTE 7—Filling of the viscometer is made easier by the use of a glass funnel warmed with a heating mantle. This helps to prevent the UHMWPE solution from precipitating.

8. Calculation

8.1 Calculate the relative solution viscosity as follows:

$$\eta_r = (t_s - k/t_s)/(t_o - k/t_o) \tag{1}$$

where:

k = kinetic energy correction constant for the particular viscometer used,

 t_s = flow time of solution at 135°C (average of three measurements), and

 t_o = flow time of pure solvent at 135°C (average of three measurements).

9. Report

- 9.1 Report the following information:
- 9.1.1 Complete identification of the material tested including type, source, manufacturer's code numbers, and trade name.
 - 9.1.2 Conditioning procedure used, if any.
- 9.1.3 The relative viscosity (viscosity ratio) of one or more concentrations, depending on whether it is desired to obtain relative, inherent, or intrinsic viscosity (viscosity ratio, logarithmic viscosity number, or limiting viscosity number) (see Appendix X4).
- 9.1.4 The intrinsic viscosity (limiting viscosity number), when desired, to three significant figures (see Appendix X4).

10. Precision and Bias

10.1 Table 1 is based on a round robin conducted in 1997 in accordance with Practice E691, involving two materials tested by six laboratories. One laboratory distributed the two commercial UHMWPE samples chosen for the evaluation. Each laboratory obtained six test results for each material.

Note 8—Caution: The explanations of r and R (10.1.1 – 10.1.4) are only intended to present a meaningful way of considering the approximate precision of this test method. The data in Table 1 should not be applied to acceptance or rejection of materials, as these data apply only to the materials tested in the round robin and are unlikely to be representative of

TABLE 1 Relative Solution Viscosity

				-	
Material	Average	S_r^A	$S_R^{\ B}$	r^{C}	R^D
UHMWPE No. 1	1.454	0.015	0.049	0.042	0.136
UHMWPE No. 2	1.653	0.017	0.048	0.047	0.136

 ${}^{A}S_{r}$ = within-laboratory standard deviation for the indicated material. It is obtained by first pooling the within-laboratory standard deviations of the test results from all of the participating laboratories.

$$S_r = [\{(s_1)^2 + (s_2)^2 \dots + (s_R)^2\}/n]^{1/2}$$

 ${}^{B}S_{R}$ = between-laboratory reproducibility, expressed as standard deviation:

$$S_R = [Sr^2 + S_L^2]^{1/2}$$

where S_{I} = standard deviation of laboratory means.

 C_r = within-laboratory critical interval between two test results = 2.8 × S_r .

 ^{D}R = between laboratories critical interval between two test results = 2.8 × S_{R} .

other lots, formulations, conditions, materials, or laboratories. Users of this test method should apply the principles outlined in Practice E691 to generate data specific to their materials and laboratory (or between laboratories). The principles of 10.1.1-10.1.4 would then be valid for such data.

10.1.1 Concept of r and R in Table 1—If S_r and S_R have been calculated from a large enough body of data, and for test results from testing one sample for each test result, then the following applies:

10.1.2 Repeatability—r is the interval representing the critical difference between two test results for the same material, obtained by the same operator using the same equipment on the same day in the same laboratory. Two test results shall be judged not equivalent if they differ by more than the r value for the material.

10.1.3 Reproducibility—R is the interval representing the critical difference between two test results for the same material, obtained by different operators using different equipment in different laboratories, not necessarily on the same day. Two test results shall be judged not equivalent if they differ by more than the R value for that material.

10.1.4 Any judgement in accordance with 10.1.2 and 10.1.3 would have an approximate 95 % (0.95) probability of being correct.

10.2 *Bias*—There are no recognized standards by which to estimate bias of this method.

11. Keywords

11.1 dilute solution viscosity; ethylene polymers; inherent viscosity (logarithmic viscosity number); intrinsic viscosity (limiting viscosity number); reduced viscosity (viscosity number); relative viscosity; specific viscosity; viscosity ratio

APPENDIXES

(Nonmandatory Information)

X1. PROCEDURE FROM PREVIOUS VERSION (D1601 – 86 (1991)^{\$\vert^{\alpha}\$}) DATING BACK TO 1957

X1.1 If it is desired to determine only the relative viscosity (viscosity ratio) or the inherent viscosity (logarithmic viscosity number), weigh one specimen of 0.18 to 0.22 ± 0.0002 g and transfer it quantitatively to a 100-mL volumetric flask which has been purged with nitrogen.

Note X1.1—Usually the determination of relative or inherent viscosity (viscosity ratio or logarithmic viscosity number) may suffice.

X1.2 To determine the intrinsic viscosity (limiting viscosity number), weigh four specimens of the following approximate weights to \pm 0.0002 g:

Specimen 1	0.09 to 0.11 g
Specimen 2	0.18 to 0.22 g
Specimen 3	0.28 to 0.32 g
Specimen 4	0.38 to 0.42 g

Note X1.2—The intrinsic viscosity (limiting viscosity number) may also be measured using successive dilutions of only one, or duplicate, solutions. This has the advantage of requiring that only one polymer specimen be weighed. Dilutions to the solution of this specimen in the viscometer are a time-saving device. The technique is as follows: Weigh one, or a duplicate, specimen of 0.38 to 0.42 g to an accuracy of ± 0.0002 g and transfer it quantitatively to a 100-mL volumetric flask, which has been purged with nitrogen, using a funnel and washing the watch glass and funnel down with solvent. Place the specimen into solution and measure the relative viscosity (viscosity ratio).

Separate dilutions of the original solution to desired concentrations can be made by adding solvent at 135°C in precisely measured quantities to the original solution in the viscometer and the relative viscosity (viscosity ratio) at each dilution tested before the next dilution is made. For example, the following technique might be used.

First Dilution—Add exactly 5 mL of solvent at 135°C to the filter stick of the viscometer and calculate the solution concentration from the known weight of solute and total volume of solvent in the viscometer. (This concentration should be approximately 0.3 g/100 mL.) Mix the solution in the viscometer thoroughly by pulling it into the viscometer bulb and back again three times. Determine the relative viscosity (viscosity ratio) at this concentration.

Second Dilution—Add exactly 10 mL of solvent at 135°C and calculate the concentration, as above. (This concentration should be approximately 0.2 g/100 mL.) Determine the relative viscosity (viscosity ratio) at this concentration.

Volumetric limitations of the Ubbelohde viscometer require that approximately 15 mL of solution be added to the instrument for the first determination of relative viscosity (viscosity ratio). Also, the viscometer will not hold and properly mix liquid volumes very much in excess of 30 mL. Hence, use of the above procedure will provide only three values of relative viscosity (viscosity ratio) from which intrinsic viscosity (limiting viscosity number) can be determined. Other dilution techniques may be used to obtain four or more values of relative viscosity (viscosity ratio), but the range of solute concentrations is limited unless the reverse procedure is used—that of introducing a minimum volume of solvent into the viscometer to obtain solvent viscosity, then adding aliquots of a concentrated stock solution to the viscometer to obtain successive values of relative viscosity (viscosity ratio) at higher concentrations.

X1.3 Add approximately 50 mL of solvent to the specimen flasks, purge them again with nitrogen, stopper them loosely and place them in an oven or bath maintained at 140°C. Vent the flasks at the end of 10 min. Shake the flasks once every 10 min until the solution is complete.

Note X1.3—Most ethylene polymers will go into complete solution at the solute concentrations used in this method within 2 h. Some polymer samples may require up to 4 h. If the solute has not dissolved in 6 h, this procedure may not be applicable, due to possibly incomplete solution of the sample not detectable to the eye. If incomplete solution of the sample is suspected, the viscometer filter stick may be removed from the instrument after the sample solution has been transferred and the filter stick dried under vacuum. Any weight difference after drying should show evidence of undissolved residue. Even with the use of an antioxidant in the solvent, significant oxidation of the polymer sample may occur in unusually long dissolving period.

Note X1.4—Caution: When the solution is considered complete, examine visually to be certain that no undissolved particles, gels, or particles of foreign matter are present.

X2. PRINCIPLES OF SOLVENT VISCOSITY (FROM PREVIOUS VERSION (D1601 – 86 (1991)^{\$1}) DATING BACK TO 1957)

X2.1 Determine the efflux time of the solvent in the viscometer until three consecutive efflux times agree within 0.2 s. The average of these readings shall be used in calculating the relative viscosity of the solution, as described in Appendix X3.

Note X2.1—The solvent viscosity may be calculated from the efflux time in accordance with the following equation:

$$V = Ct - B/t \tag{X2.1}$$

where:

V = kinematic viscosity, cSt,

C = calibration constant for the viscometer,

t = efflux time, s, and

B = kinetic energy and end effect correction constant. (This constant is dependent on the design of the viscometer and may be determined experimentally, along with the constant C, by use of suitable calibrating fluids. In general, with viscometers designed so that B is relatively small, the correction B/t is negligible for relatively long efflux times.)

Note X2.2—Although the kinetic energy effect inherent in the design of the viscometer may be determined by Test Method D445, that method is believed to be tedious for liquids with viscosities in the range of decalin at 135°C. The following equations provide a more convenient and precise means of calculating the relative viscosity (viscosity ratio), η_r , corrected

for the kinetic energy contribution.

$$\eta_r = \frac{t_s + \Delta t_s}{t_o + \Delta t_o} = \frac{t_s - D/t_s}{t_s - D/t_o}$$
(X2.2)

where:

 t_s and t_o = flow times of the solution and solvent, respectively, Δt = kinetic energy correction term for a particular liquid, and

D = a constant for the viscometer.

D and Δt may be calculated as follows:

$$D/t = (-Vm\rho)/L\eta 8\pi = \Delta t \tag{X2.3}$$

where:

t = flow time of the liquid in the viscometer,

V = efflux volume of the liquid,

a = kinetic energy correction coefficient. (If the viscometer capillary has trumpet-shaped ends that break away rather sharply, and Δt is no larger than 3 % of t, it is probably safe to assume m equal to unity.)

= density of the liquid,

L = length of the capillary, and

 η = viscosity of the liquid.

Using this equation, the viscometer constant D, may be calculated after the following measurements are made:

- (1) Flow time of a liquid (water for example) of known viscosity and density in the viscometer,
 - (2) Capillary length, and
- (3) Volume of the viscometer bulb. This may be done by filling the bulb with water and measuring the volume of the water in a graduated cylinder. An accuracy of ± 3 % is adequate for all measurements, if Δt is no larger than 3% of t. This will provide a precision of better than 0.1%.

X3. CALCULATION FROM PREVIOUS VERSION (D1601 – 86 (1991)^{E1}) DATING BACK TO 1957

X3.1 Relative Viscosity (Viscosity Ratio)—Calculate the relative viscosity (viscosity ratio) for each concentration measured, from the average efflux times as follows:

$$\eta_r = t/t_o \tag{X3.1}$$

where:

 η_r = relative viscosity (viscosity ratio)

t = average efflux time of solution, and

 t_o = average efflux time of pure solvent.

X3.2 Inherent Viscosity (Logarithmic Viscosity Number)—Calculate the inherent viscosity (logarithmic viscosity number) for each concentration measured, as follows:

$$\eta_{inh} = \ln \eta_r / C \tag{X3.2}$$

where:

 η_{inh} = inherent viscosity (logarithmic viscosity number) at concentration C, and

 $ln\eta_r$ = natural logarithm of the relative viscosity (viscosity ratio), and

C = concentration in grams/100 mL of solution.

X3.3 Intrinsic Viscosity (Limiting Viscosity Number)⁶—Plot the four logarithmic viscosity numbers versus their respective concentrations on rectilinear graph paper. Draw the best straight line through the points and extrapolate it to zero concentration. The intrinsic viscosity (limiting viscosity number), $[\eta]$, is the intercept of the line at zero concentration.

Note X3.1—If desired, the specific viscosity (η_{sp}) and the reduced viscosity (viscosity number) (η_{red}) may be calculated as follows:

$$\eta_{sp} = \eta_r - 1 \tag{X3.3}$$

$$\eta_{red} = \eta_{sp}/C$$

Note X3.2—As a check on the plot of the intrinsic viscosity (limiting viscosity numbers) versus their concentrations, the specific viscosity ($\eta_s p$) divided by their concentrations for the four specimens may be plotted versus their concentrations on the same graph. The slopes of these two lines will not be the same, but they should converge to the same value at zero concentration. This additional line serves to more accurately position the zero concentration point.

X4. COMPENDIUM OF MACROMOLECULAR NOMENCLATURE (SELECTED TERMS)⁷

X4.1 Archibald's method—a sedimentation method based on the fact that at the meniscus and at the bottom of the centrifuge cell there is never a flux of the solute across a plane perpendicular to the radial direction and the equations characterizing the sedimentation equilibrium (see X4.11) always

from equilibrium.

X4.1.1 *Discussion*—The use of the term 'approach to sedi-

X4.1.1 *Discussion*—The use of the term 'approach to sedimentation equilibrium' for Archibald's method is discouraged, since it has a more general meaning.

apply there, even though the system as a whole may be far

X4.2 equilibrium sedimentation (method)—a method by which the distribution of the concentration of the solute or dispersed component in a dilute solution or dispersion along the centrifuge cell is measured at sedimentation equilibrium

⁶ Schulken, R. M., and Sparks, M. L., *Journal of Polymer Science*, JPSCA, Vol XXVI, 1957, p. 227.

⁷ Compendium of Macromolecular Nomenclature, International Union of Pure and Applied Chemistry, Macromolecular Division, Commission on Macromolecular Nomenclature, prepared for publication by W.V. Metanomski of the Chemical Abstracts Service, Columbus, OH, Blackwell Scientific Publications, Oxford.

(see X4.11), and the results are interpreted in terms of molar masses or their distribution, or both.

X4.3 equilibrium sedimentation in a density gradient—an equilibrium sedimentation technique (see X4.2) working with a multi-component solvent forming a density gradient in a centrifugal field.

X4.4 *Huggins equation*—the equation describing the dependence of the reduced viscosity (see X4.7), η_i/c , on the mass concentration of the polymer, c, for dilute polymer solutions of the form

$$\eta_i/c = [\eta] + k_H [\eta]^2 c \tag{X4.1}$$

X4.5 inherent viscosity, logarithmic viscosity number—recommended symbols: η_{inh} , η_{ln} , respectively; the ratio of the natural logarithm of the relative viscosity (see X4.9) to the mass concentration of the polymer, c, i.e.

$$\eta_{\rm inh} \equiv \eta_{\rm ln} = (\ln \eta_r)/c.$$
(X4.2)

X4.5.1 Discussion—See X4.7.1 and X4.7.2.

X4.6 intrinsic viscosity, limiting viscosity number—recommended symbol: [η]; the limiting value of the reduced viscosity (see X4.7) or the inherent viscosity (see X4.5) at infinite dilution of the polymer, i.e.

$$\left[\eta\right] = \lim_{c \to 0} \left(\eta_i / c\right) = \lim_{c \to 0} \eta_{inh} \tag{X4.3}$$

X4.6.1 *Discussion*—This term is also known in the literature as the Staudinger index.

X4.6.2 Discussion—See X4.7.1 and X4.7.2.

X4.7 reduced viscosity, viscosity number—the ratio of the relative viscosity increment (see X4.8) to the mass concentration of the polymer, c, i.e. η/c .

X4.7.1 *Discussion*—The unit must be specified; cm³/g is recommended.

X4.7.2 *Discussion*—This quantity and those in X4.5 and X4.6 are neither viscosities nor pure numbers. The terms are to be looked on as traditional names. Any replacement by consistent terminology would produce unnecessary confusion in the polymer literature.

X4.8 relative viscosity increment—recommended symbol: η_i ; the ratio of the difference between the viscosities of solution and solvent to the viscosity of the solvent, i.e. $\eta_i = (\eta - \eta_s)/\eta_s$. For explanation of symbols, see X4.9.

X4.8.1 *Discussion*—The use of the term 'specific viscosity' for this quantity is discouraged, since the relative viscosity increment does not have the attributes of a specific quantity.

X4.9 relative viscosity, viscosity ratio—recommended symbol: η_r ; the ratio of the viscosity of the solution, η_s , i.e. $\eta_r = \eta/\eta_s$.

X4.10 sedimentation coefficient—recommended symbol: s; a parameter characterizing the motion of a particle in a centrifugal field and defined as the velocity of motion u due to unit centrifugal acceleration, i.e. $s = ul(r \cdot \omega^2)$, where ω is the angular velocity and r the distance from the centre of rotation.

X4.10.1 *Discussion*—The unit 10^{-13} second is useful; this unit has been referred to as a 'svedberg' which, however, is not an SI unit.

X4.11 *sedimentation equilibrium*—the equilibrium established in a centrifugal field when there is no net flux of any component across any plane perpendicular to the centrifugal force.

X4.12 sedimentation velocity method—a method by which the velocity of motion of solute component(s) or dispersed particles is measured and the result is expressed in terms of its (their) sedimentation coefficient(s) (see X4.10).

SUMMARY OF CHANGES

Committee D20 has identified the location of selected changes to this standard since the last issue (D1601 - 99(2004)) that may impact the use of this standard. (August 1, 2012)

(1) Revised 5.7 as part of the five-year review.

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